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lainfall Analysis for rainage Design olume III. Itensity-Duration-Frequency urves

#### Technical Report Documentation Page

	Government Access	on No 3 R	ecipient s Corolog No	,
DWR Bulletin No. 195				
4 Title and Subtitle	-	5 R	eport Date	
Rainfall Analysis for Dr	ainage Des	ign Oct	ober 1976	
Volume III, Intensity-Du	ration-Fre		erforming Organizatio	n Code
Curves		-		
7 Author(s)		8 P.	erforming Organizatio	n Report No
J. D. Goodridge				
9 Performing Organisation Name and Address		10	York Unit No TRAIS	1
California Department of	Water Res	ources	Contract or Grant No	
P. O. Box 388		E-3		
Sacramento, CA 95802		13	ype of Repart and P	errod Covered
12 Sponsoring Agency Name and Address				
California Departments o	f Water Re	sources Fir	al	
and Transportation	I water ne			
Sacramento, CA 95814		114	ponsoring Agency Co	ode
15 Supplementory Notes				_
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Transportation, Federal	Highway Ad	ministration, a	ind 33 othe	r agencies.
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This report is an analys	is of dept	h-duration-free	mency of n	recipi-
tation in California and				
from about 30 rain gage				
analysis of each record	is availab	le, giving 12 r	eturn peri	ods
ranging from 2 to 10,000	years and	durations of 5	minutes t	o 60 days,
including the annual tot	al precipi	tation. Method	ls of inter	station
interpolation are given.	Hourly p	recipitation re	cords of t	he
National Weather Service		aluated to deve	lop 5-, 10	-, 15-,
and 30-minute extreme da	ta.			
This volume contains pre	cipitation	intensity-dura	tion-frequ	ency curves
from 500 recording rain		ed on maximum a	nnual rain	fal1
depths for 5 to 180 minu	tes.			
The information contains	d in this	report is inter	ded for us	e in
runoff computation using	procedure	s such as the r	ational me	thod or
the unit hydrograph meth	od.			
A cooperative computer d	ata bank h	as been develor	ed to stor	e data
on rainfall extremes and	to period	ically analyze	data, as w	ell as
to maintain a continuous	file for	future use by	cooperator	s.
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17. Key Words		18 Dietribution Statement		
Precipitation, Frequency		Nc restriction		
Rainfall, Duration, Cali	fornia	available to t		
		National Techr		
		Service, Sprin	igilela, VA	22101
19 Security Classif, (of this report)	20 Security Clas	sel, (of this page)	21. No. of Poges	22 Price
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Department of Water Resources

**Bulletin No. 195** 

# Rainfall Analysis for Drainage Design

Volume III. Intensity-Duration-Frequency Curves

October 1976

Claire T. Dedrick Secretary for Resources

The Resources Agency

Edmund G. Brown Jr. Governor

State of California

Ronald B. Robie
Director

Department of Water Resources

# OTHER VOLUMES OF BULLETIN NO. 195 (Bound separately)

- Volume I. Short-Duration Precipitation Frequency Data
- Volume II. Long-Duration Precipitation Frequency Data

#### Disclaimer Statement

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#### ACKNOWLEDGMENTS

Alameda County Flood Control and Water Conservation District Contra Costa County Flood Control and Water Conservation District

This report was prepared in cooperation with the State of California, Business and Transportation Agency, Department of Transportation; and the U. S. Department of Transportation, Federal Highway Administration.

### Data was supplied by:

Cummings-Tehachapi Water District East Bay Municipal Utility District Kern County, Department of Public Works and County Surveyor Kern County Water Agency Los Angeles County Flood Control District Marin County, Department of Public Works Marin Municipal Water District Monterey County Flood Control and Water Conservation District Orange County Environmental Management Agency Pacific Gas and Electric Company Riverside County Flood Control and Water Conservation District Sacramento County, Department of Public Works Sacramento Municipal Utility District San Bernardino County Flood Control District San Diego County, Department of Sanitation and Flood Control San Francisco, City of, Sanitary Engineering Department San Luis Obispo County, Engineering Department San Mateo County, Department of Public Works

Santa Barbara County Flood Control and Water Conservation District

Santa Clara Valley Water Conservation District Santa Cruz County, Departments of Public Works and Health Shasta County, Department of Water Resources

Southern California Edison Company

University of California

University of Nevada, Desert Research Institute

U. S. Army, Corps of Engineers

U. S. Army, Hunter-Leggett Meteorological Team

U. S. Bureau of Reclamation

U. S. Forest Service

U. S. Geological Survey

U. S. Marine Corps, Camp Pendleton

U. S. National Weather Service

Ventura County Flood Control District

and many private individuals



Typical modern tipping bucket rain gage

Photo by Weather Measure Corp.

#### INTRODUCTION

Bulletin No. 195, Rainfall Analysis for Drainage Design, is published as three separate volumes that complement one another but may be used independently, as well. Volume I contains short-duration precipitation data. Volume II contains long-duration precipitation data. This volume, Volume III, presents intensity-duration-frequency (IDF) curves for stations with data for precipitation periods of 5 minutes to 24 hours.

The IDF curves are arranged first by county, second by watersheds within each county, and then alphabetically by station name. The drainage basins are depicted on Plate 1. Individual station locations are plotted on Plate 2. Mean annual precipitation is shown on Plate 3.

The data in this volume consist of annual extremes of rainfall for durations of 5 to 180 minutes (reported in Volume I, along with the analysis on which the curves are based). This information is necessary to the design of culverts, spillways, and other drainage facilities. The sizes of such structures are determined by many factors, including the expected rainfall intensities associated with given return periods. These curves have been developed specifically for culvert designers of the California Department of Transportation who need data on rainfall intensity to estimate runoff at culvert sites. The curves are planned for use with simple runoff models, such as the rational formula:

$$Q = 1.008 \text{ CiA}$$
 (a)

where

Q = peak runoff in cubic feet per second

C = runoff coefficient, ranging from "0" for no runoff to "1" for runoff of all rainfall

i = rainfall intensity in inches per hour

A = area in acres

Rainfall intensities are inversely proportional to time; the shorter the period of time, the higher the intensity. Therefore short-duration rainfall is the most critical in culvert design. Short-duration rainfall extremes can be estimated by use of the following equation:

$$I = \overline{P}T^{n}$$
 (b)

where

I = design storm intensity, in inches per hour

 $\overline{P}$  = mean one-hour storm, as a fraction of MAP, in inches

T = time in hours

N = slope of the log-intensity/log-line plot

Design rainfall for various return periods can be developed from the following equation:

$$I_{j} = MAP \overline{P} (1 + K_{j}CV)$$
 (c)

where

j refers to return period

 $I_{i}$  = precipitation intensity for return period j

MAP = mean annual precipitation, in inches (see Plate 3)

 $\overline{P}$  = mean one-hour storm, as a fraction of MAP, in in inches (see Plate 4)

 $K_{\dot{\gamma}}$  = frequency factor (see Table 1)

CV = coefficient of variation (see Figure 1)

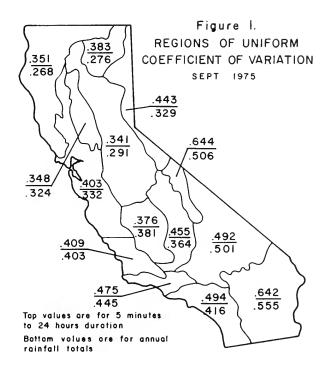
Combining equations (b) and (c) yields the equations of the IDF curves of Volume III:

$$K_{\dot{1}} = (MAP) (\overline{P}) (1 + K_{\dot{1}}CV)T^{-n}$$
 (d)

K<sub>j</sub> is the only value representing different return periods; therefore, the lines on the IDF curves are parallel. The distance between the lines are a function of CV and K<sub>j</sub> only. The slope of the IDF curves represents the ratio of short-duration design storms to storms of longer duration

The length of the time period used in a specific application depends on the "time to peak", or time of concentration, which is unique to each watershed. The broad ranges of time represented here are suitable for all but the smallest watersheds. Rooftop and bridge surfaces frequently need data for durations shorter than 5 minutes. No adequate data are available for storms of that duration at the present time; however, estimates of such durations can probably be made from a straight line extension of the IDF curves in this volume.

In some cases, there was no information on one or more of the seven durations of 5, 10, 15, 30, 60, 120, and 180 minutes. Where this has occurred, only those durations that were available were used in this analysis. The durations used are shown on the IDF curves by plotting the mean values just above the two-year return period values.



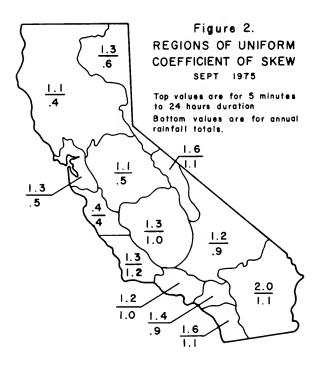
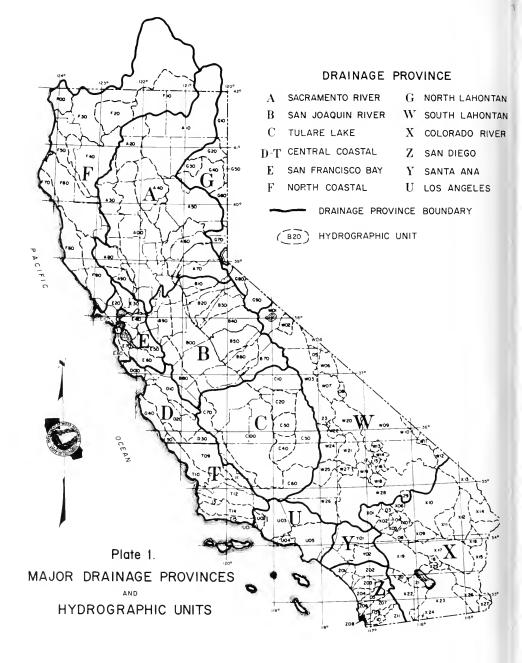


TABLE 1
FREQUENCY FACTORS FOR PEARSON'S TYPE III DISTRIBUTION

Return Period	Coefficient of Skew																
in Yeors	.4	.5	.6	.7	.8	.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0
2	07	08	10	12	13	15	16	18	20	21	23	24	25	27	28	29	31
5	.82	.81	.80	.79	.78	.77	.76	.75	.73	.72	.71	.69	.68	.66	.64	.63	.61
10	1.32	1.32	1.33	1.33	1.34	1.34	1.34	1.34	1.34	1.34	1.34	1.33	1-33	1.32	1-32	1.31	1.30
20	1.75	1.77	1.80	1.82	1.84	1.86	1.88	1.89	1.91	1.92	1.94	1.95	1.96	1.97	1.98	1.99	2.00
25	1.88	1.91	1.94	1.97	1.99	2.02	2.04	2.06	2.09	2.11	2.13	2.15	2.16	2.18	2.19	2.21	2.22
40	2.14	2.19	2.22	2.27	2.31	2.35	2.38	2.42	2.45	2.49	2.52	2.55	2.58	2.61	2.64	2.66	2.69
50	2.26	2.31	2.36	2.41	2.45	2.50	2.54	2.58	2.63	2.67	2.71	2.74	2.78	2.81	2.85	2.88	2.91
100	2.62	2.69	2.76	2.82	2.89	2.96	3.02	3.09	3.15	3.21	3.27	3.33	3.39	3.44	3.50	3.55	3.61
200	2.95	3.04	3.13	3.22	3.31	3.40	3.49	3.58	3.66	3.75	3.83	3.91	3.99	4.07	4.15	4.22	4.30
1,000	3.67	3.81	3.96	4.10	4.24	4.39	4.53	4.67	4.81	4.96	5.10	5.23	5.37	5.51	5.64	5.77	5.91
2,000	3.96	4.12	4.29	4.46	4.63	4.80	4.97	5.13	5.30	5.47	5.63	5.80	5.96	6.12	6.28	6.44	6.60
10,000	4.60	4.82	5.05	5.27	5.50	5.72	5.96	6.18	6.41	6.64	6.87	7.09	7.32	7.54	7.77	8.00	8.21



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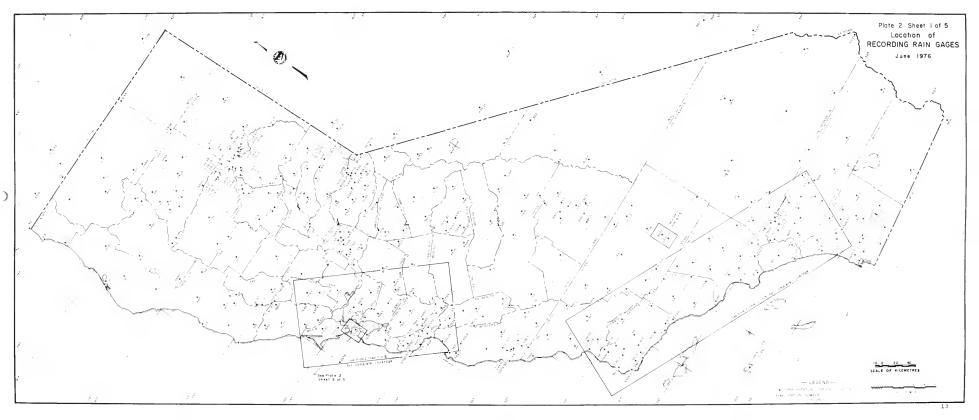
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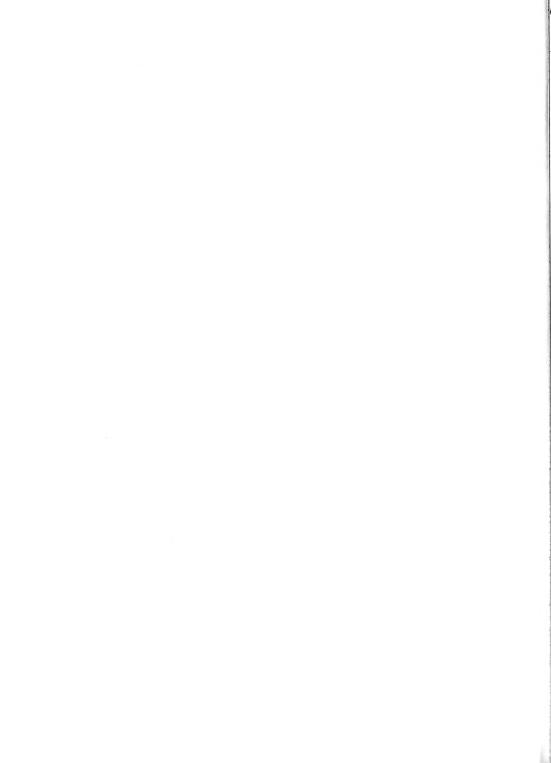
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Scarpers Peak	216	Tehachapi No 18	66
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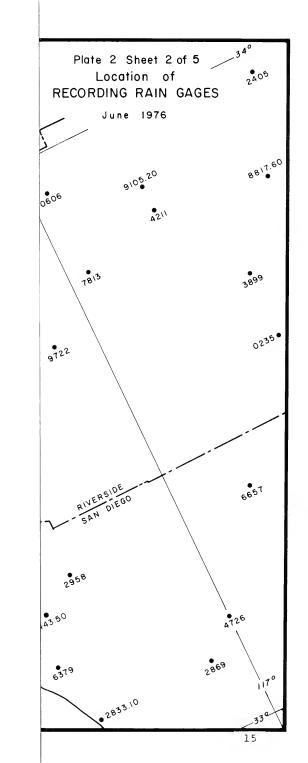
<u>Station</u>	Page	Station	Page
Tehachapi No 26	67	Villa Park Dam	145
Tehachapi No 28	68	•	199
Tehachapi No 30	68		251
Terminous Dam	269	Volta Power House	253
Termo	75	Walnut Creek 2 ENE RRNG	41
The Geysers	260	Walnut Creek 2 ENE	42
Thermal AP	154	Wasioja Forbes Rch	219
Three Rivers 6SE	270	Waterman Gd Sta	108
Three Rivers PH No 1	270	Wawona RS	113
Tiger Creek PH	33	Weaverville	267
Tonopah Nevada	312		42
Topanga Pat Sta	85		61
Trabuco Canyon	147		292
Tracy 2 SSE	205		145
Trinity Center	266	Westwood	75
Truckee R S	135	Wheatland 2NE	289
Tujunga Mill Creek	84		60
Tulelake	255		278
Tustin Automatic	144	Wheller Springs 7N	287
Twin Pines	155		252
United Technology C	242		114
Upland FC650B	191		38
Upper Franklin Res	107		116
Upper San Leandro Filters			162
Upper Toro Creek	210	Woodacre	81
Upper Tres Pinos	173		158
Upper Van Vlick SMUD	48		48
Valleton	130		138
Van Nuys	108	- <del>-</del>	117
Venado		Yosemite N P	113
Ventura County Apt 168		Yucaipa Water Co	192
Victorville	179	Yuma Arizona AP NWS	295

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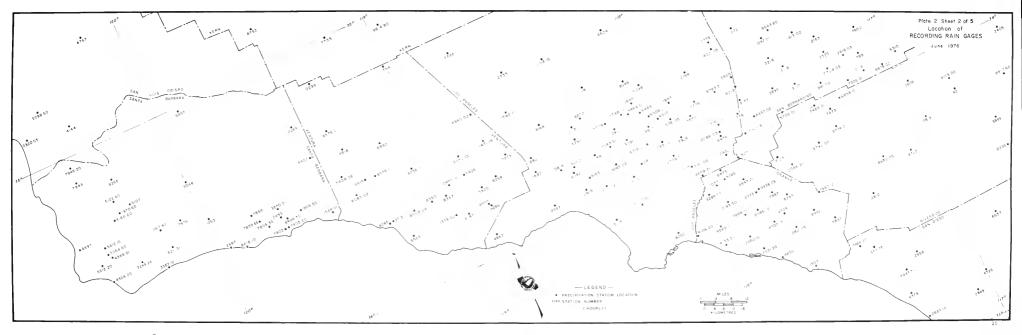
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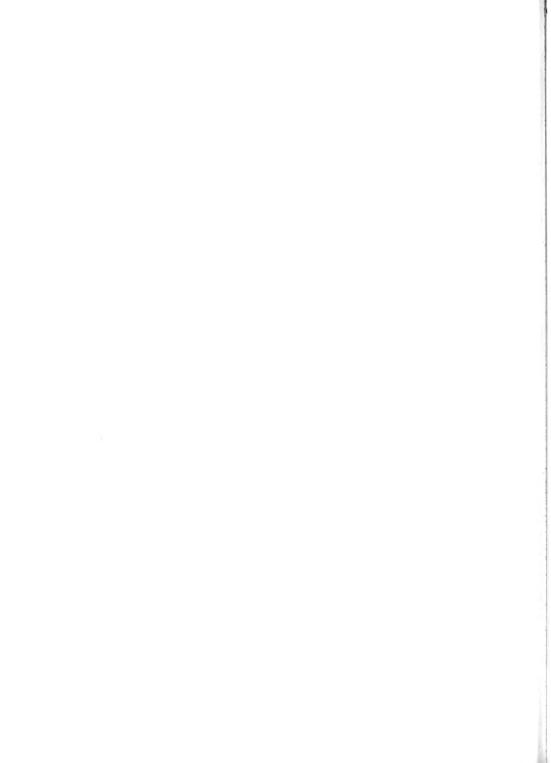


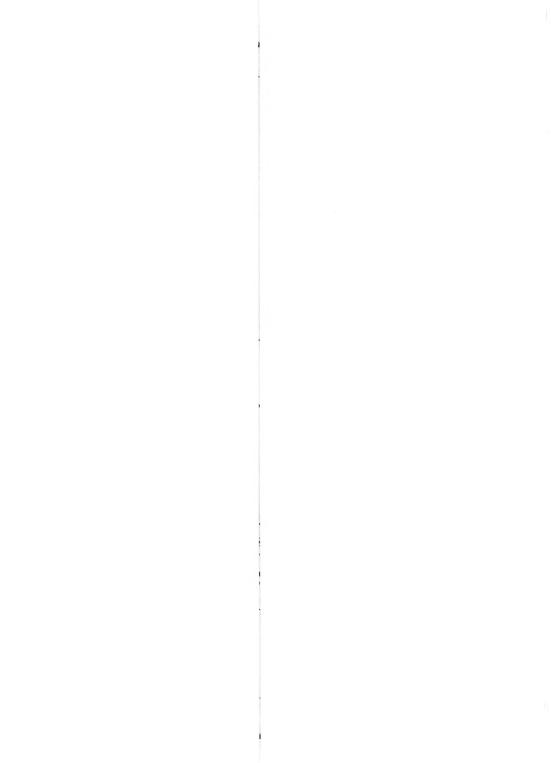


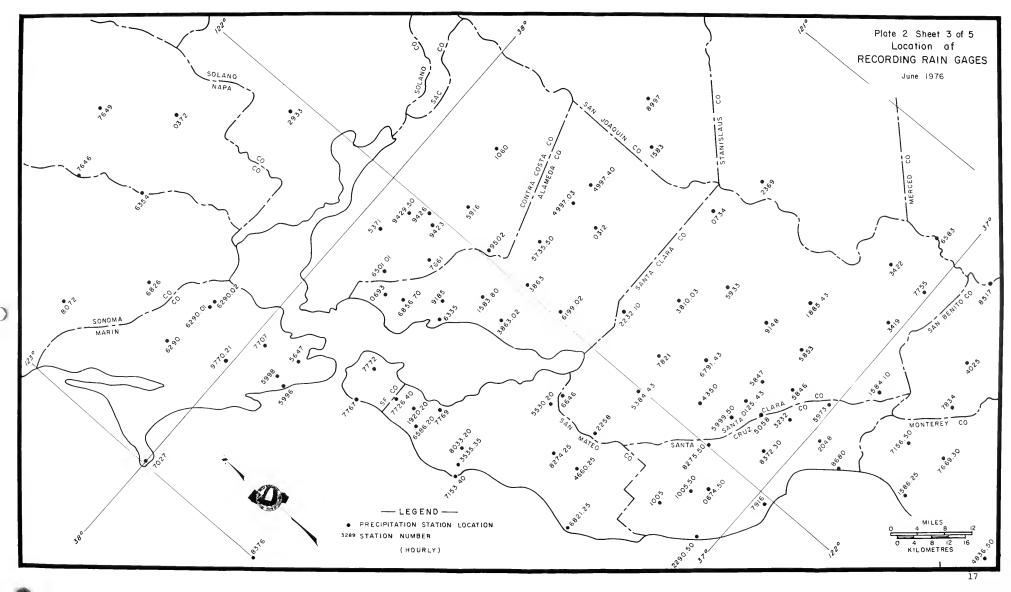


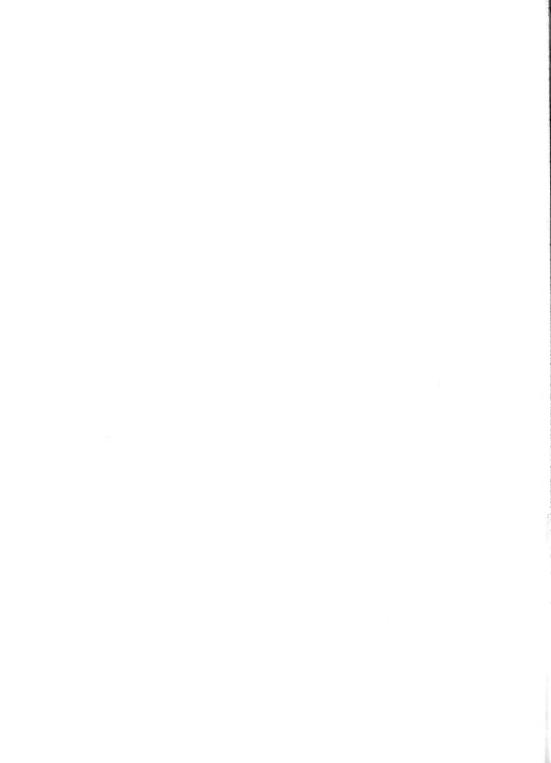
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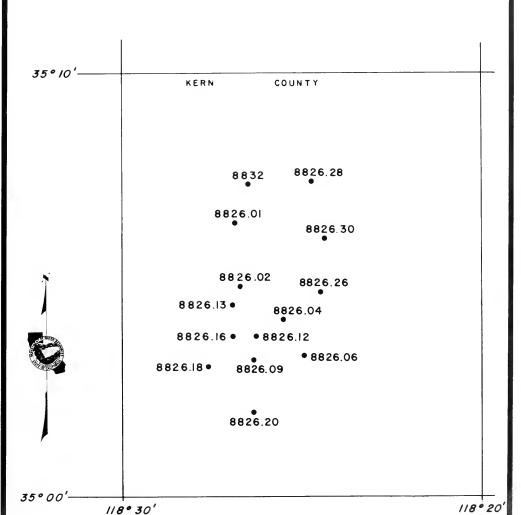








## Plate 2 Sheet 4 of 5 Location of RECORDING RAIN GAGES June 1976



--- LEGEND ---

PRECIPITATION STATION LOCATION
3209 STATION NUMBER
(HOURLY)

MILES

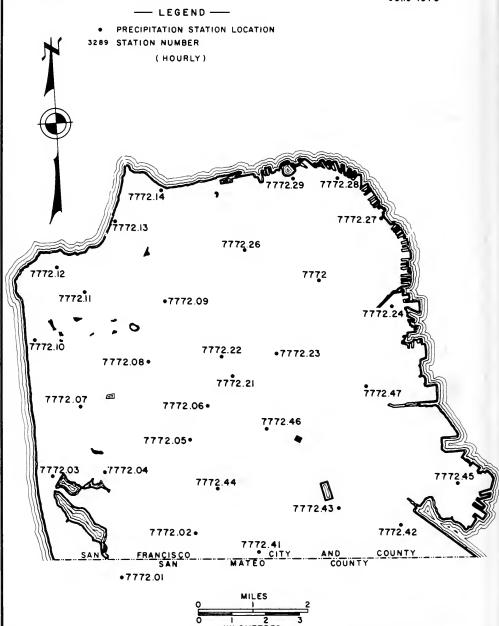
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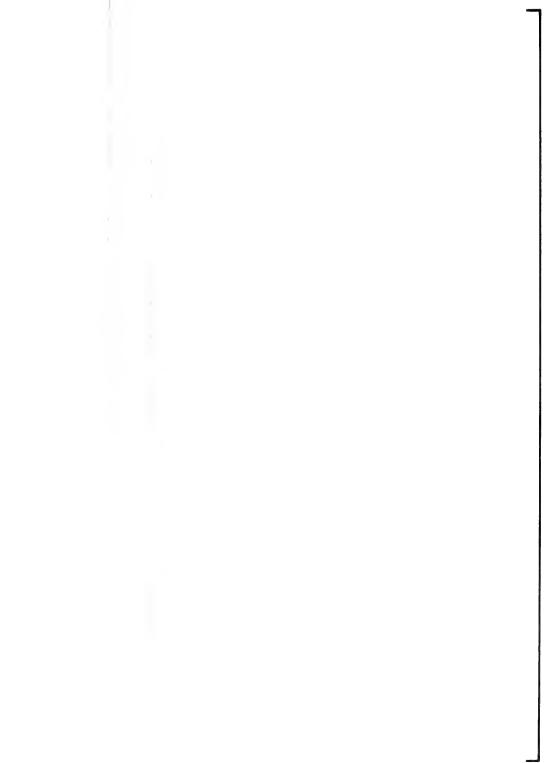
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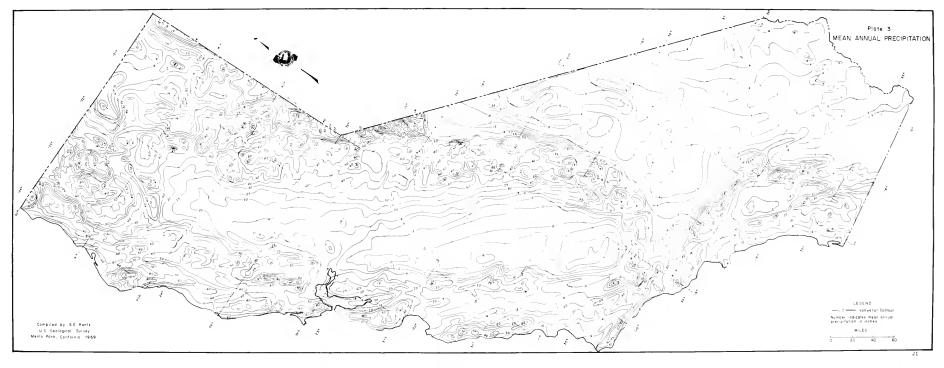
KILOMETRES

## Plate 2 Sheet 5 of 5 Location of RECORDING RAIN GAGES

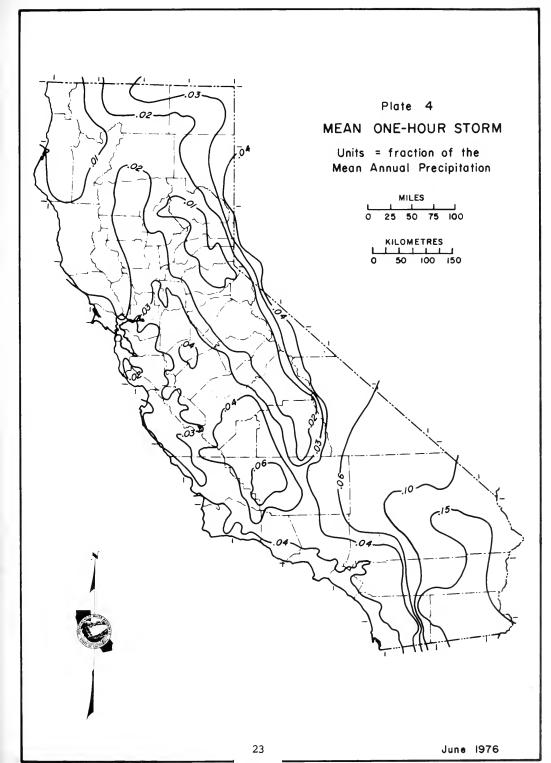
June 1976

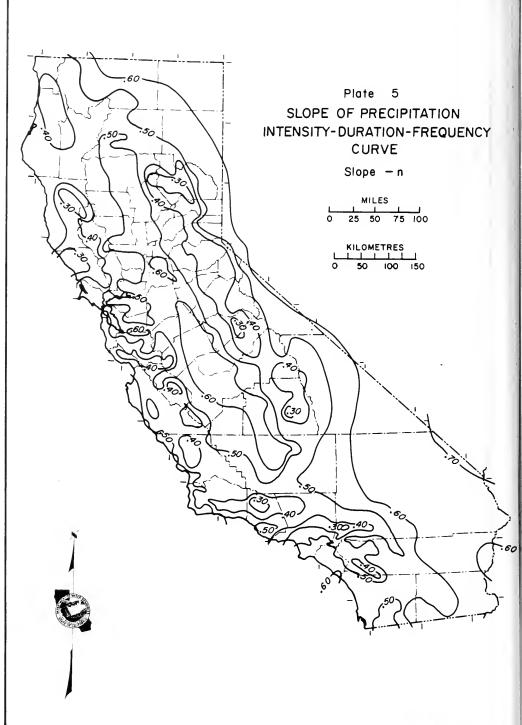




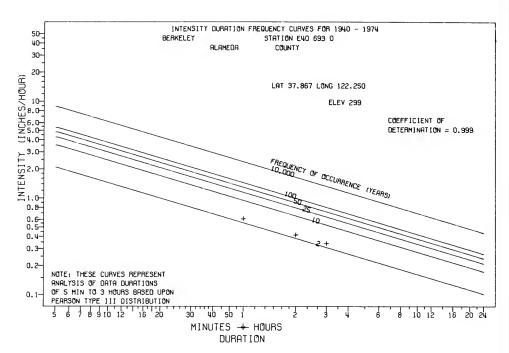


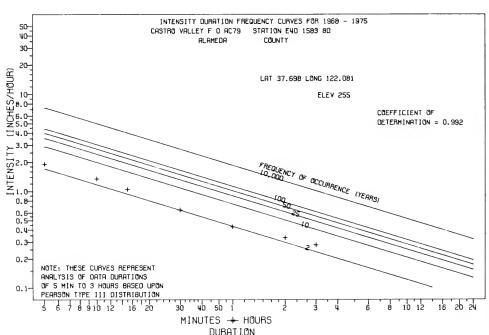


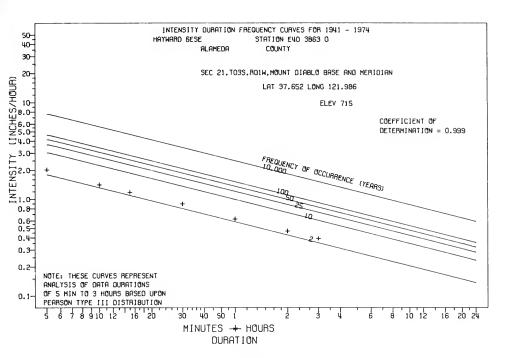


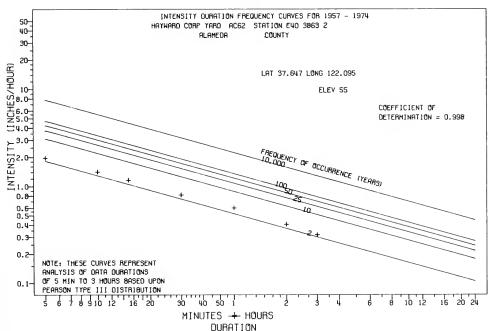


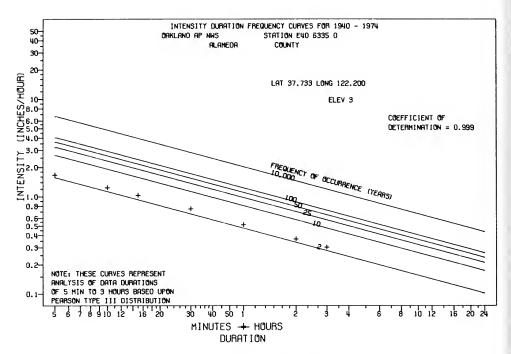
INTENSITY-DURATION-FREQUENCY CURVES

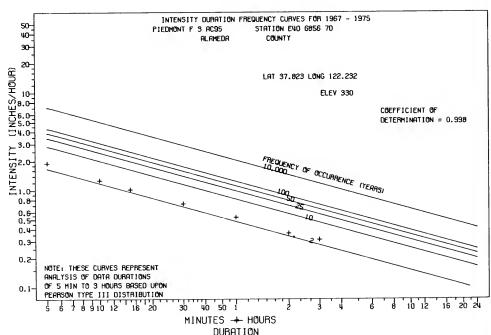


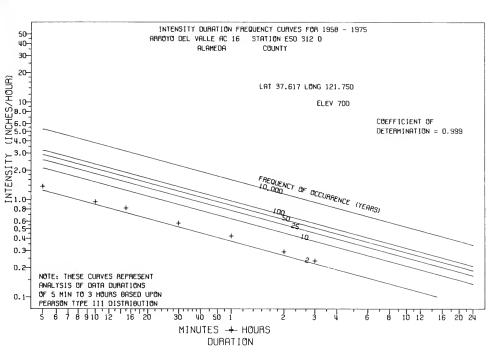


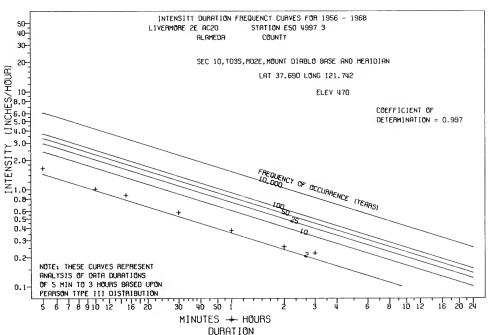


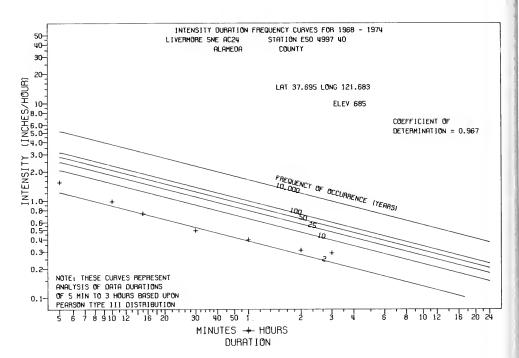


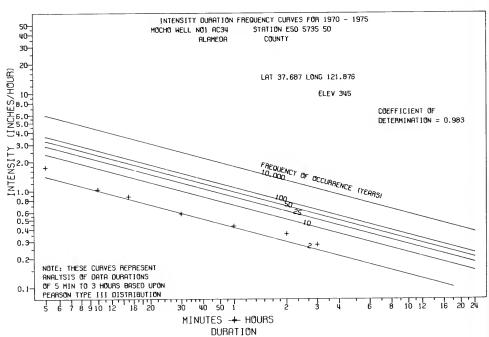


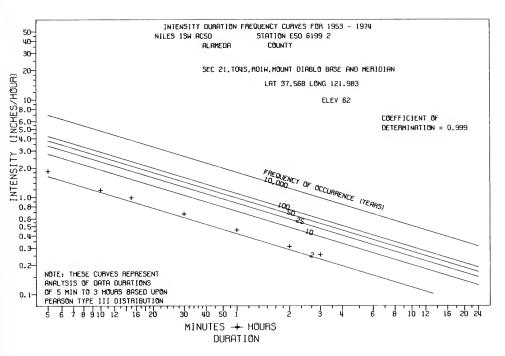


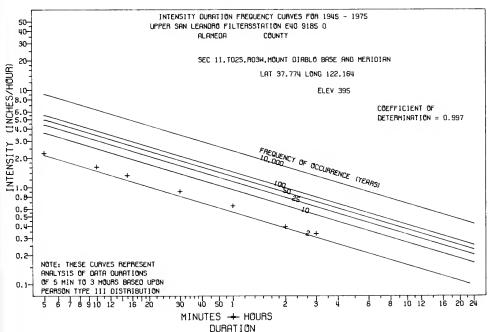


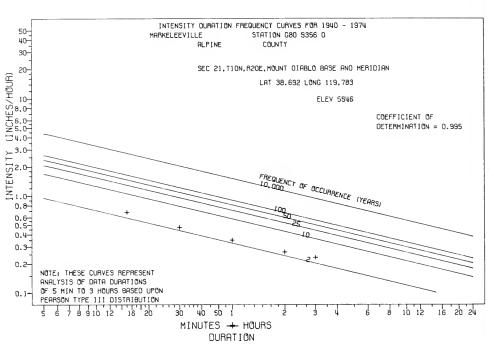


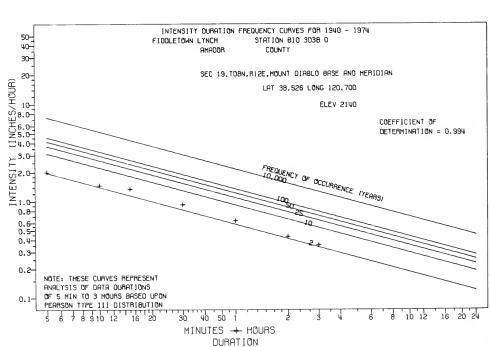


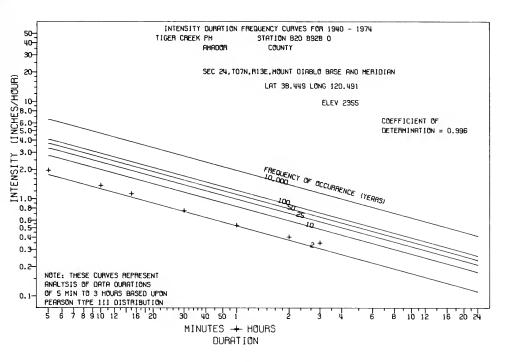


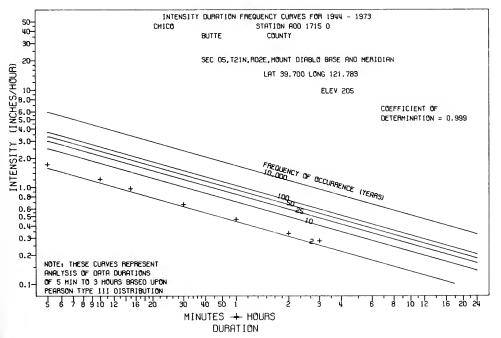


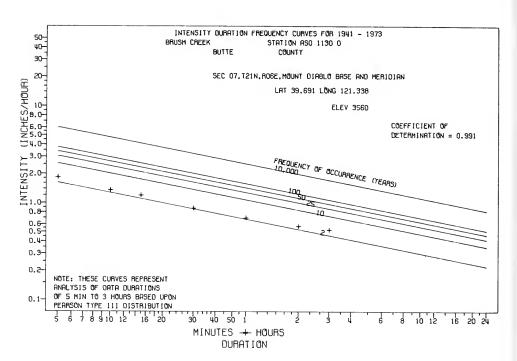


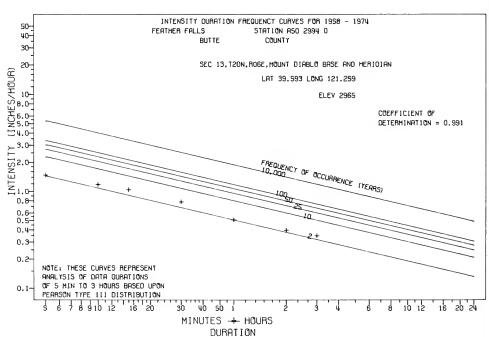


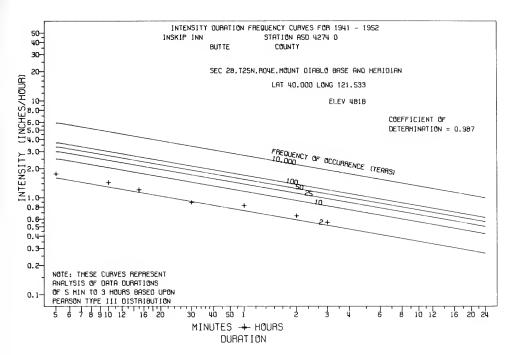


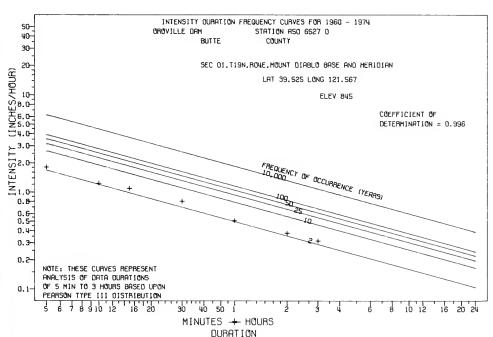


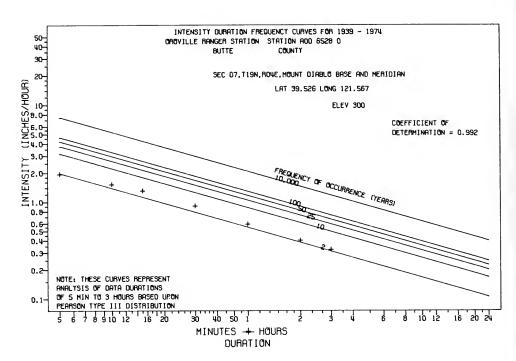


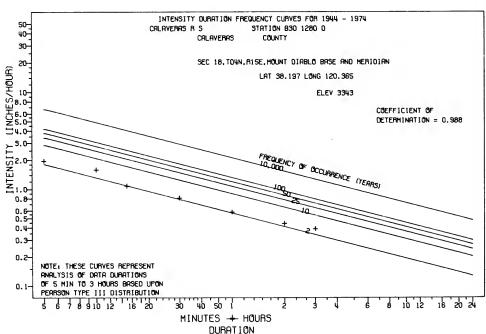


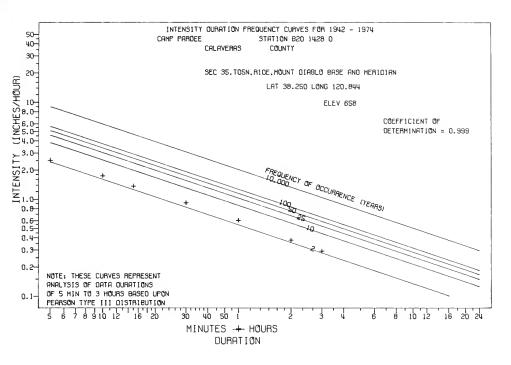


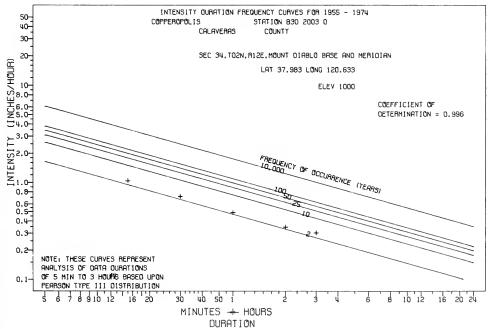


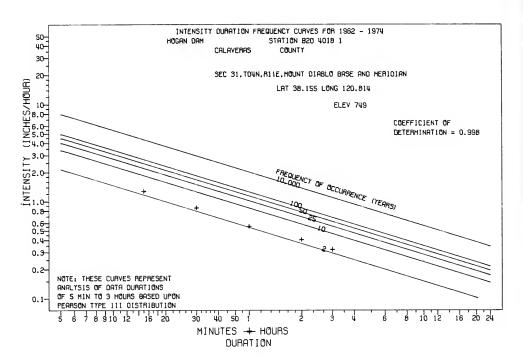


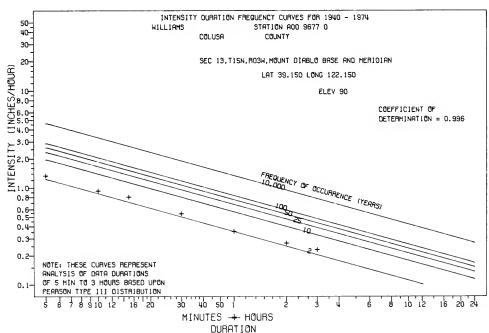


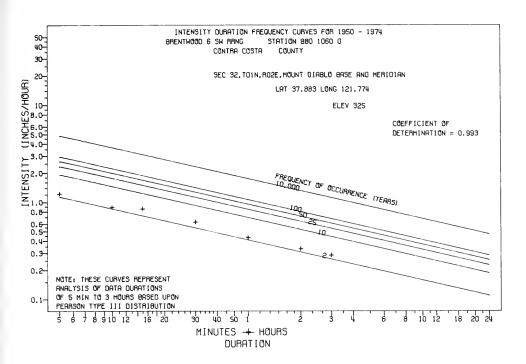


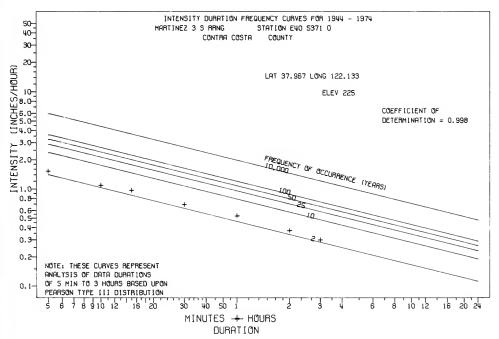


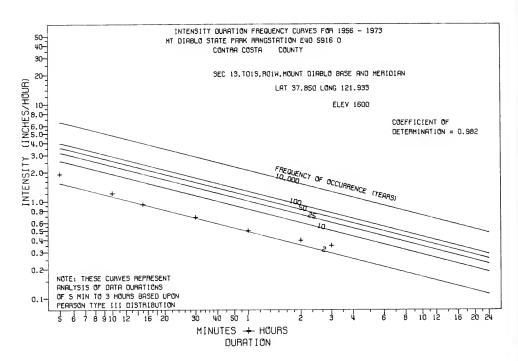


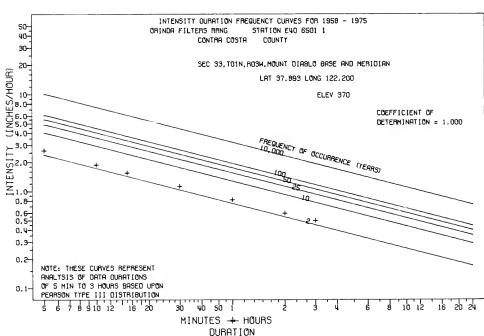


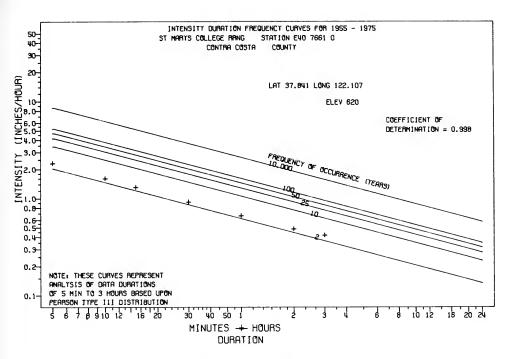


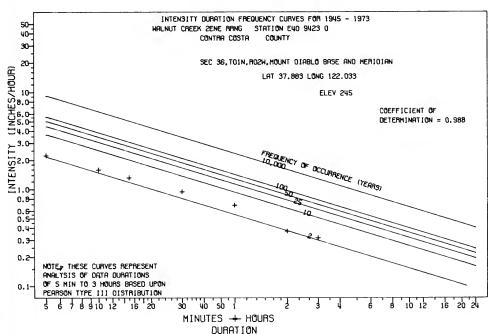


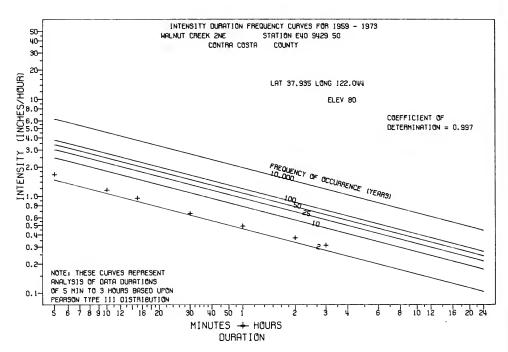


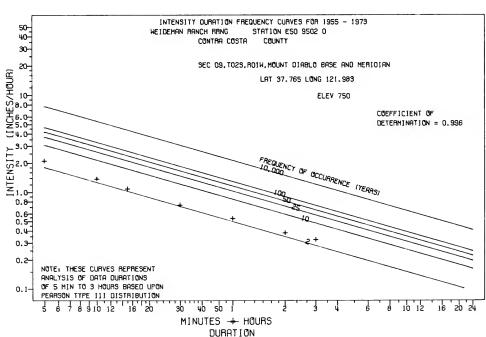


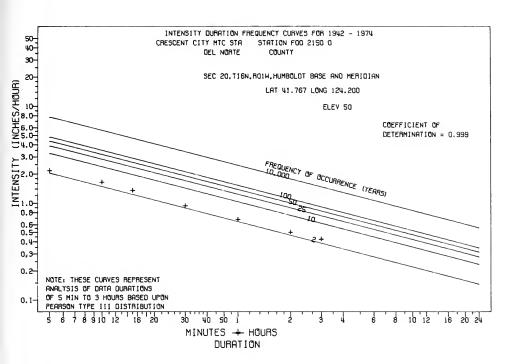


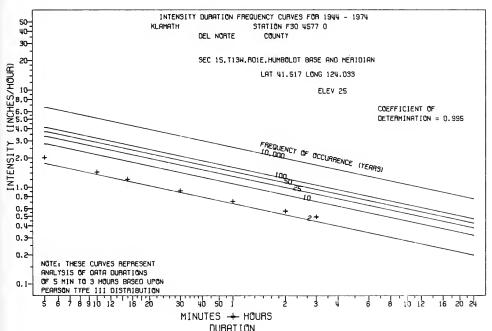


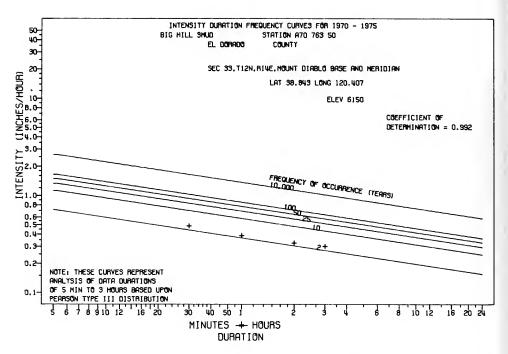


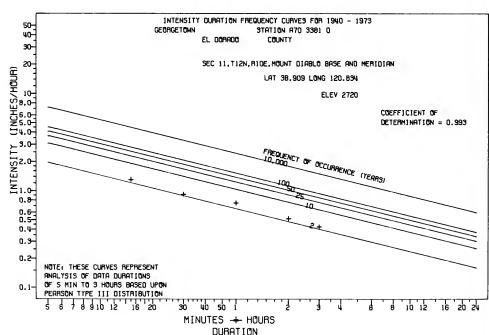


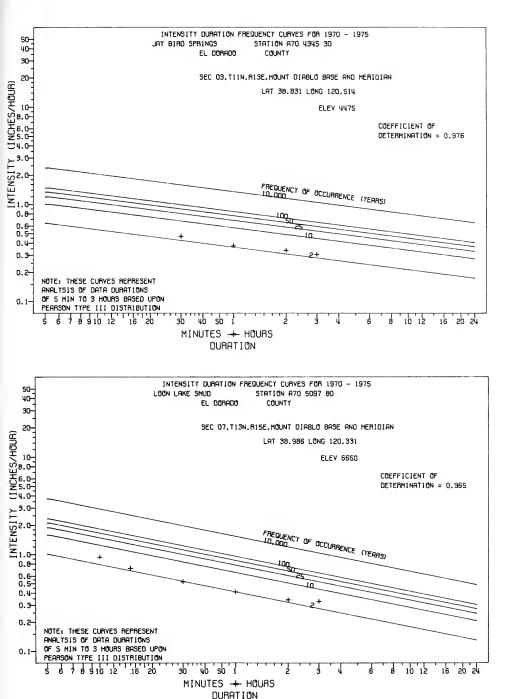


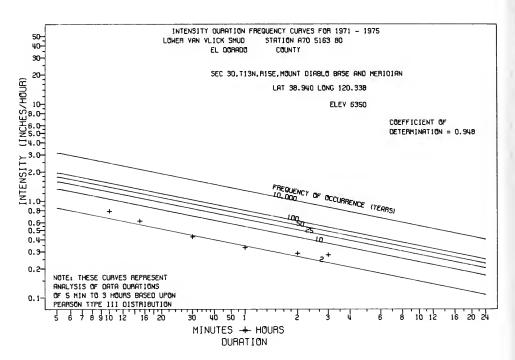


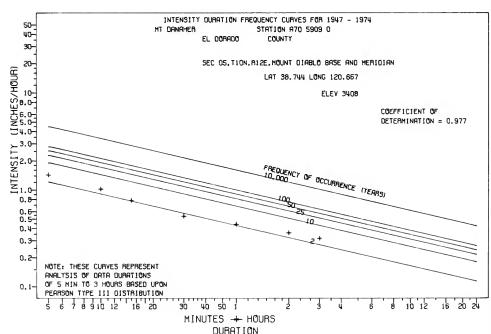


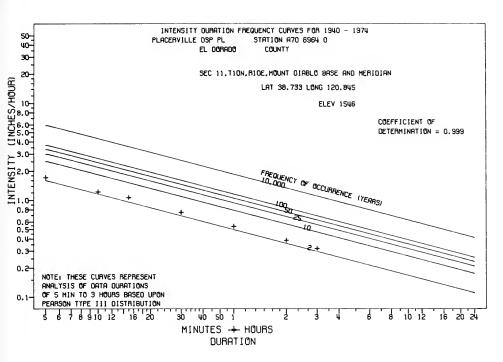


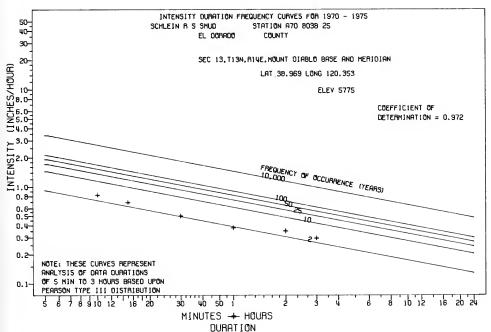


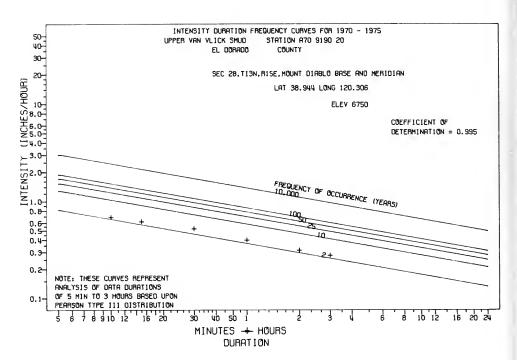


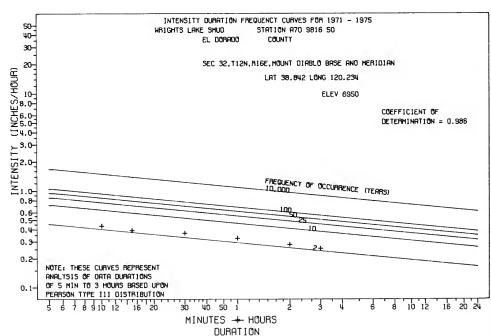


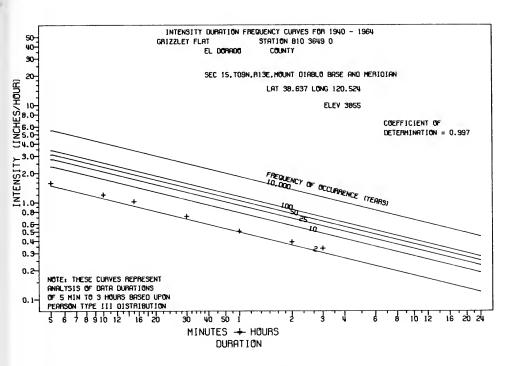


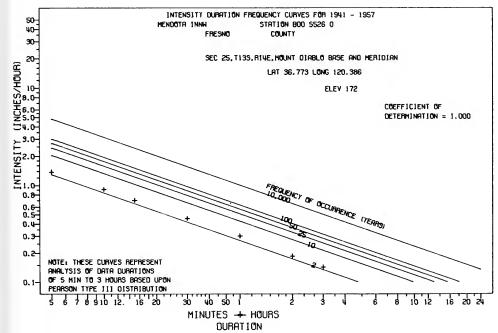


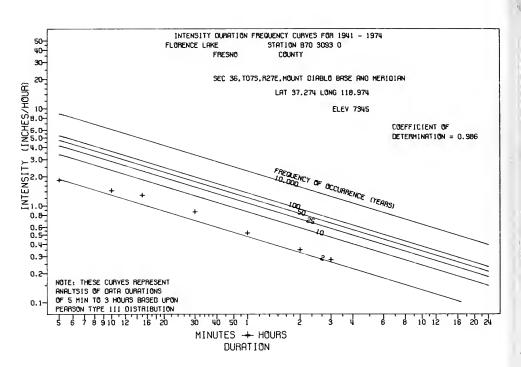


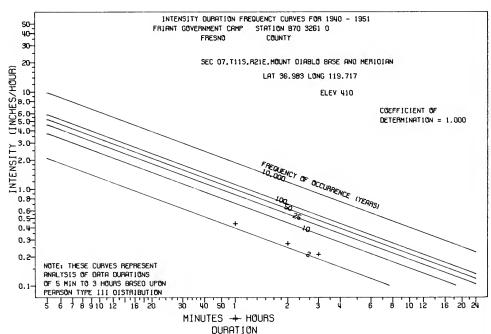


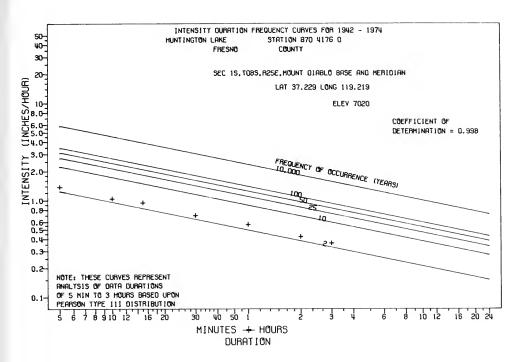


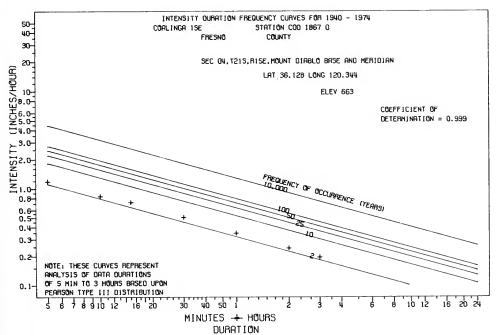


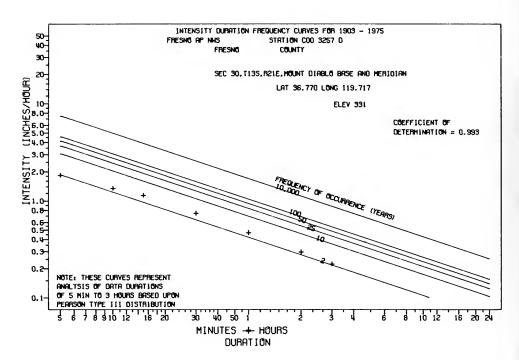


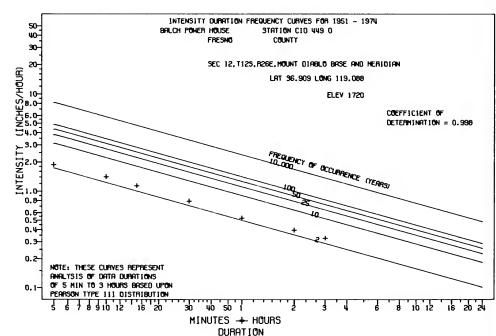


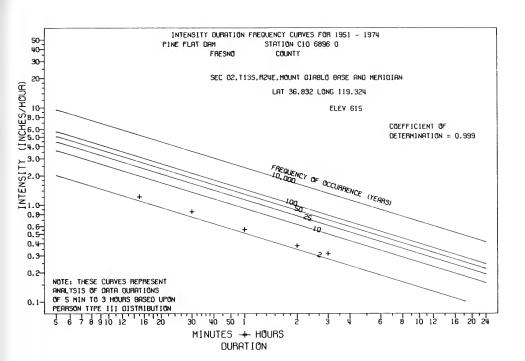


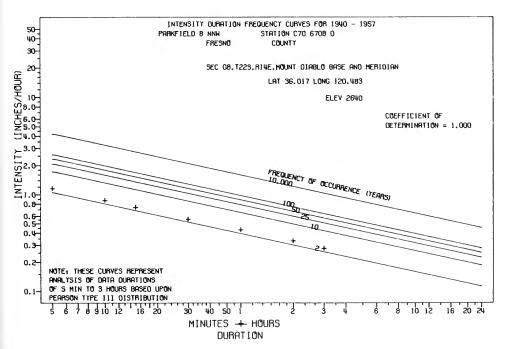


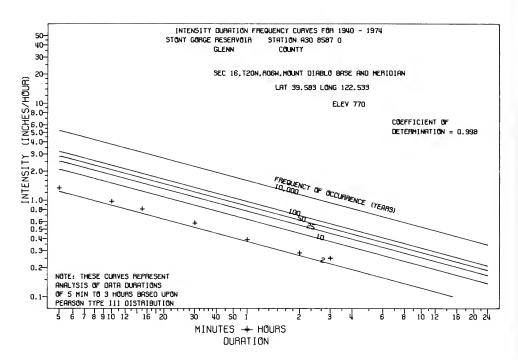


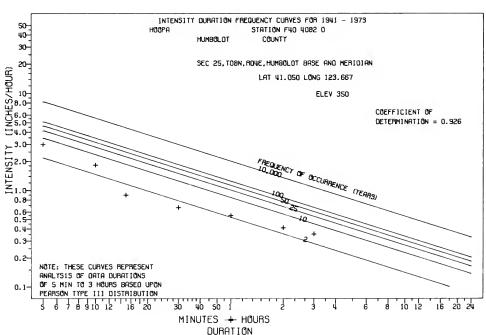


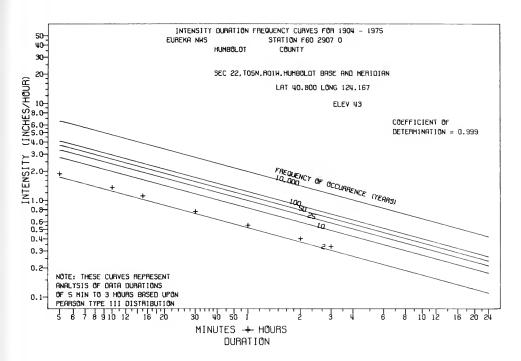


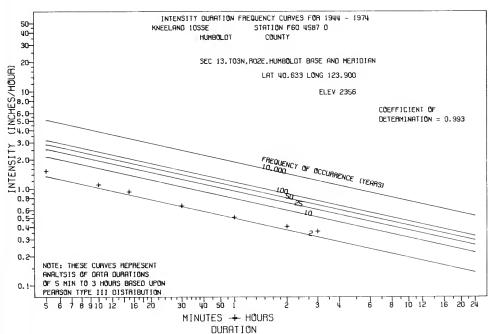


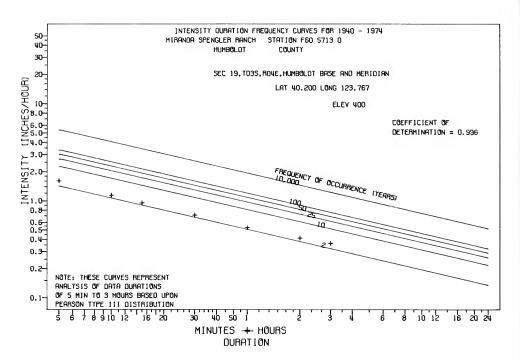


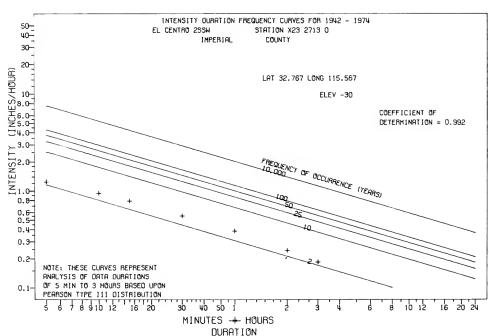


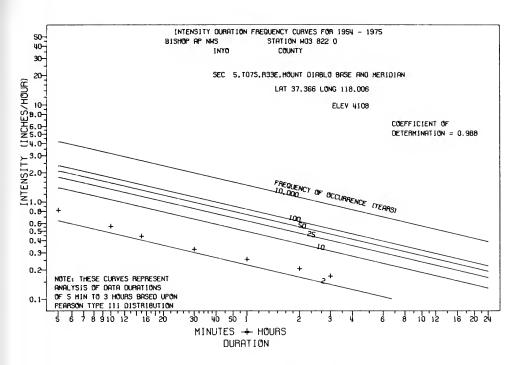


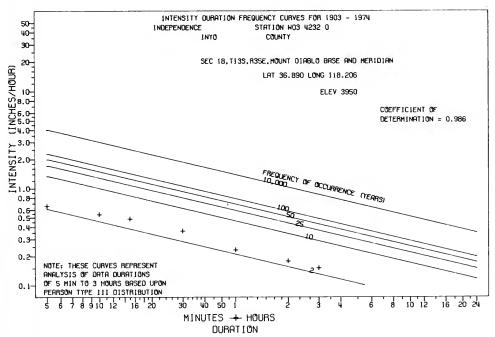


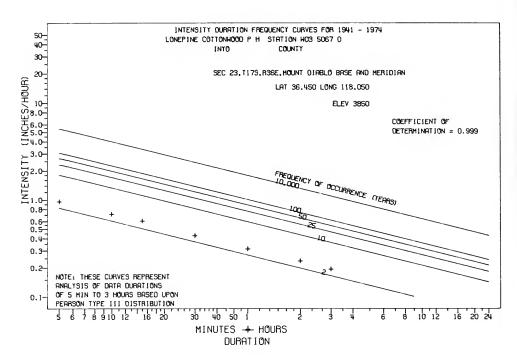


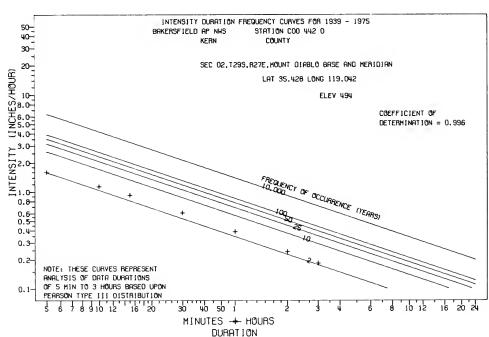


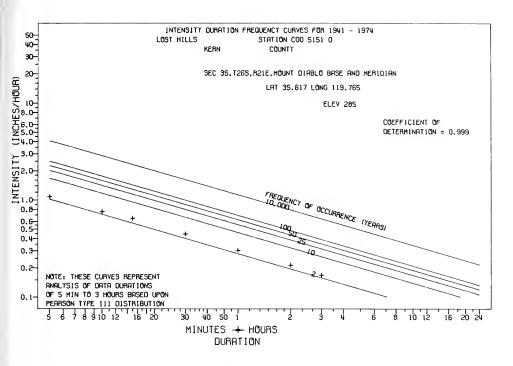


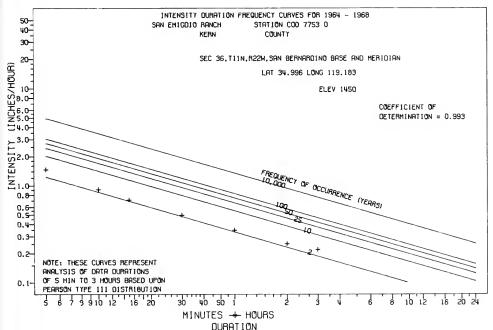


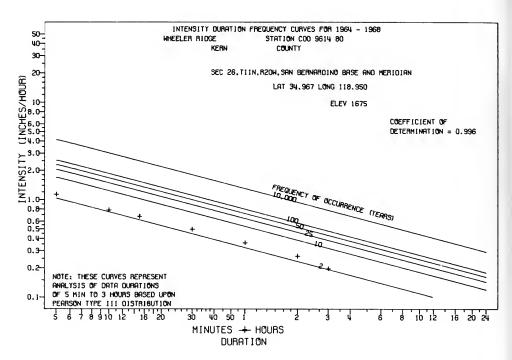


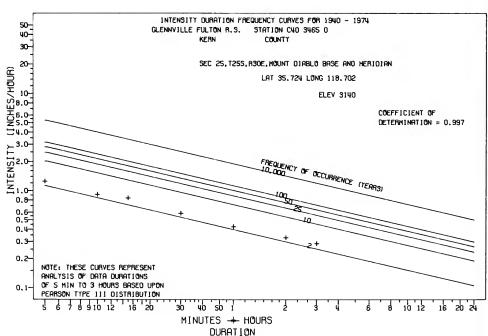


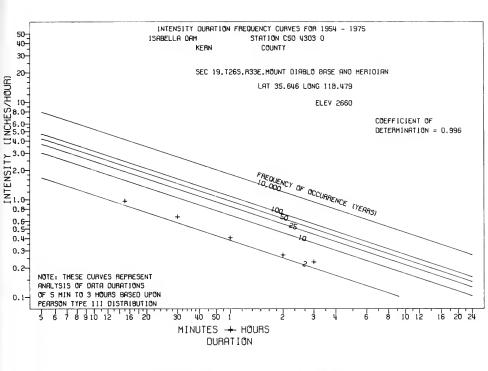


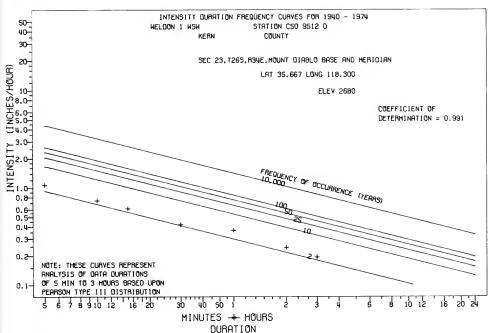


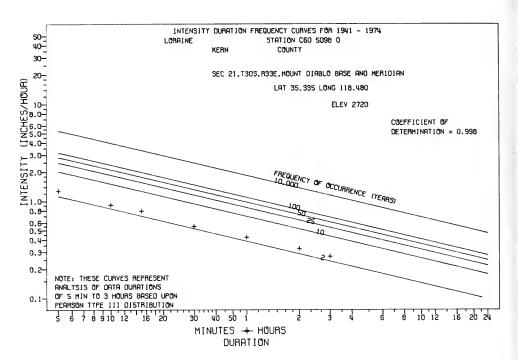


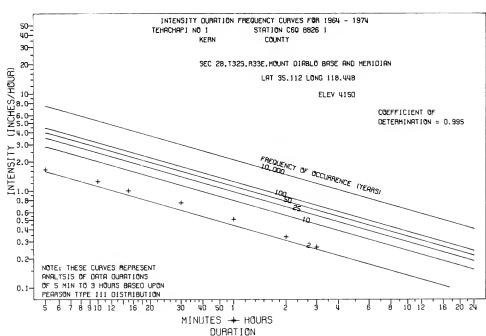


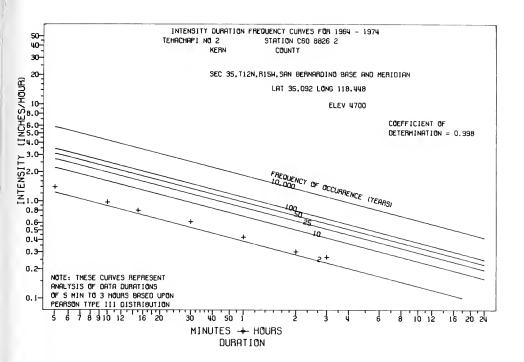


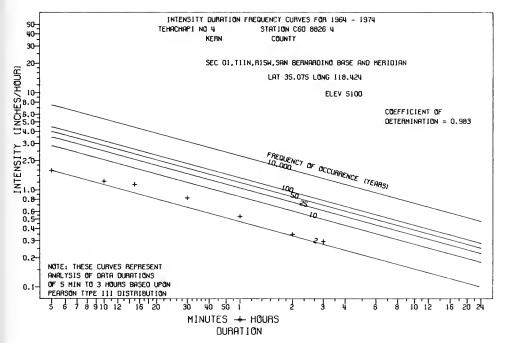


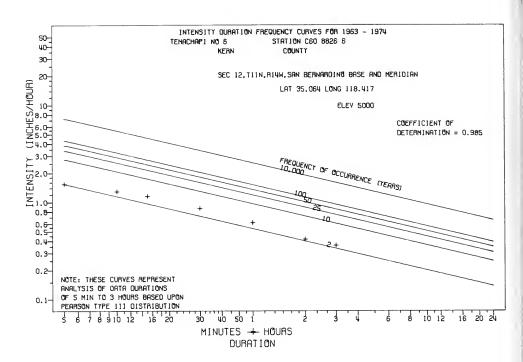


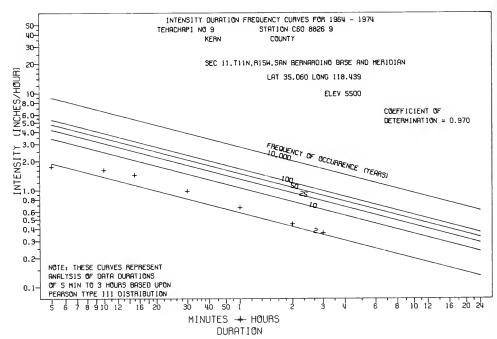


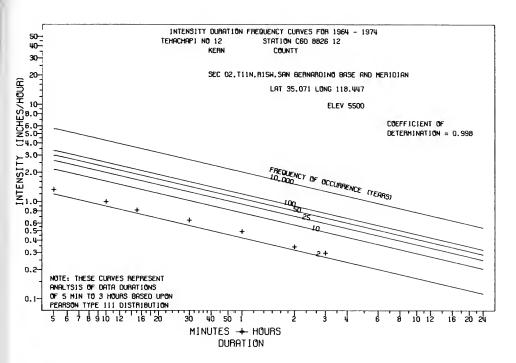


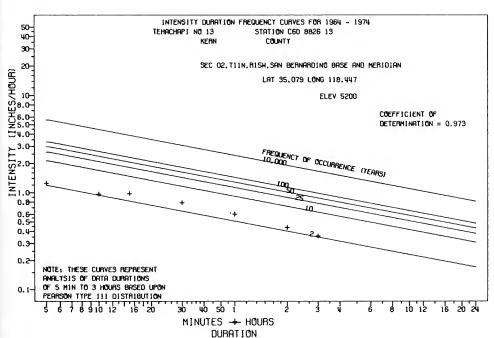


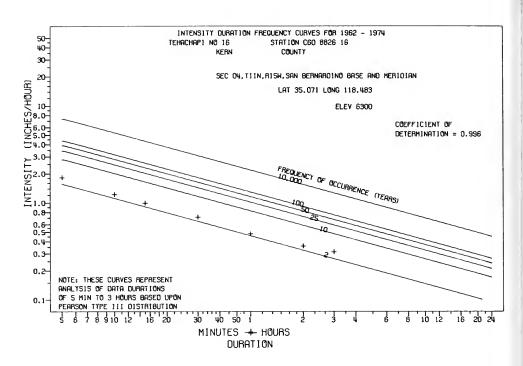


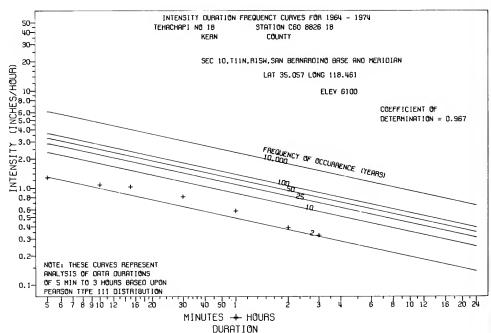


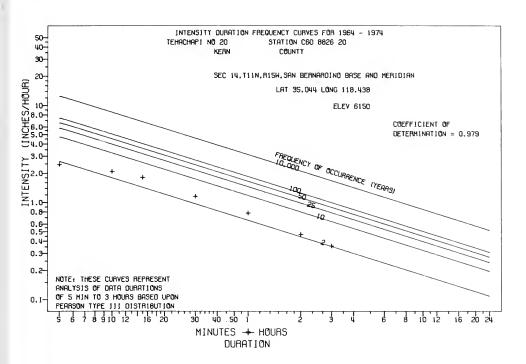


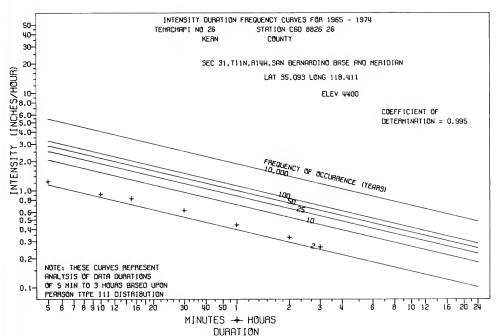


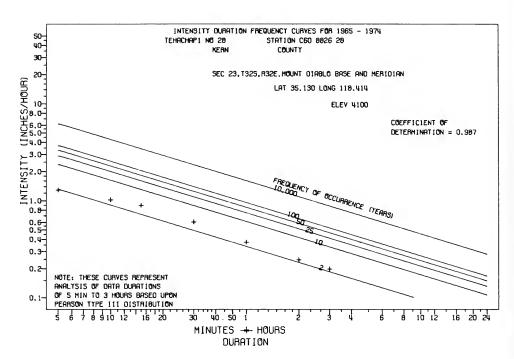


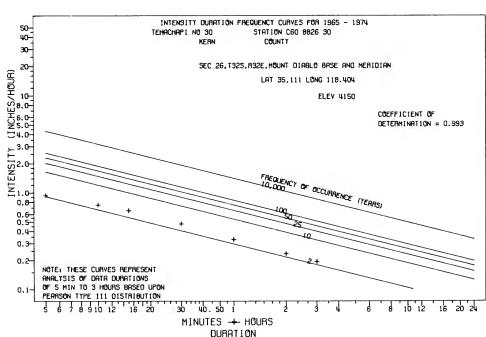


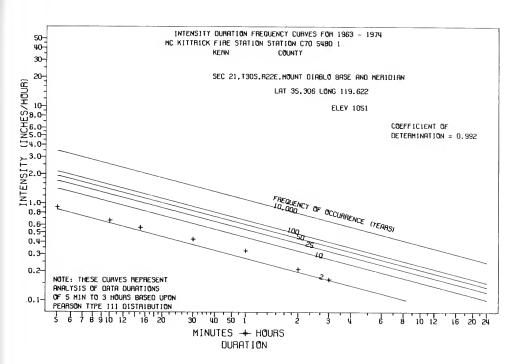


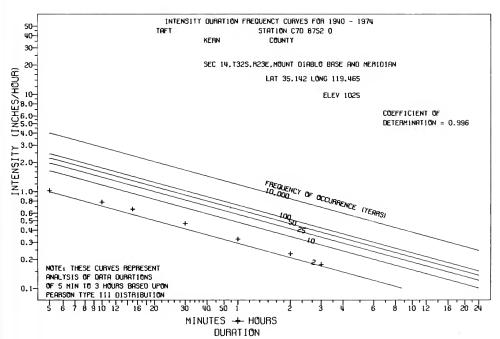


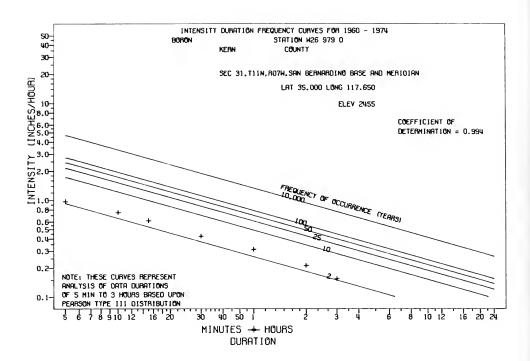


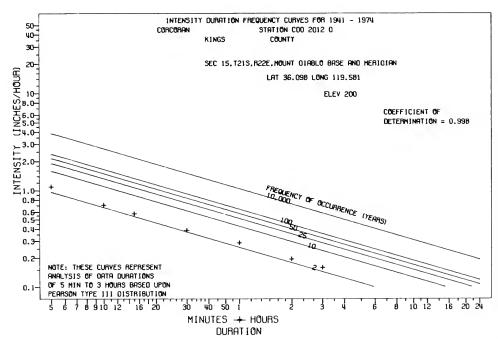


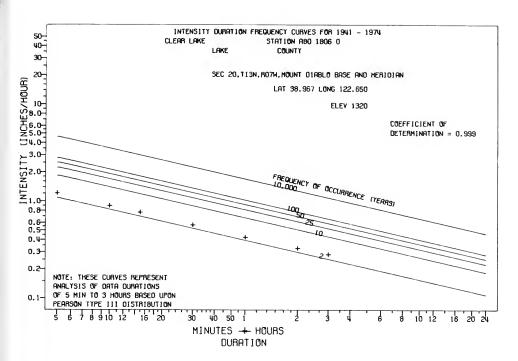


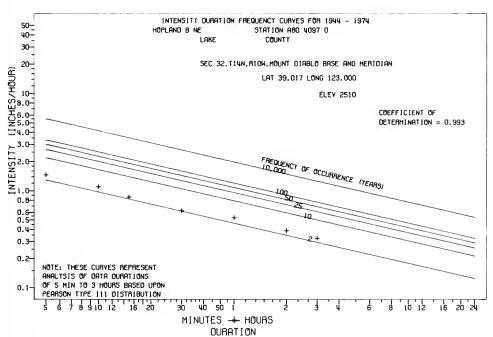


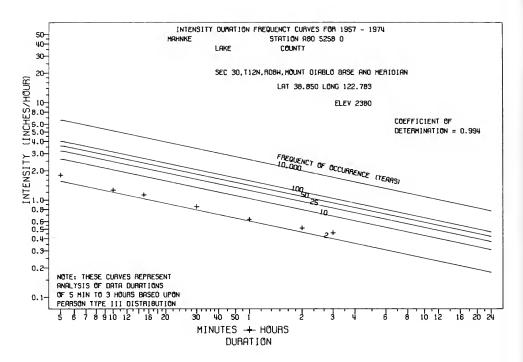


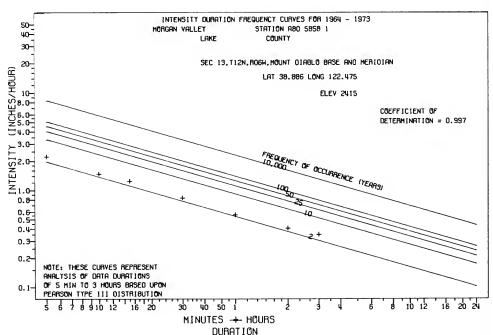


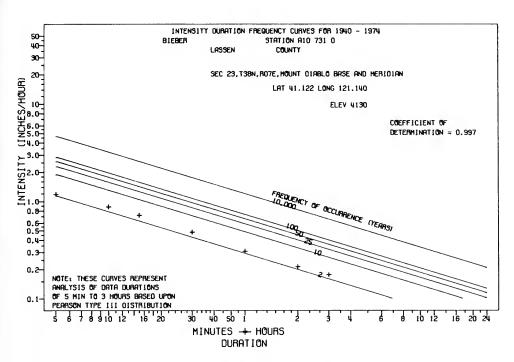


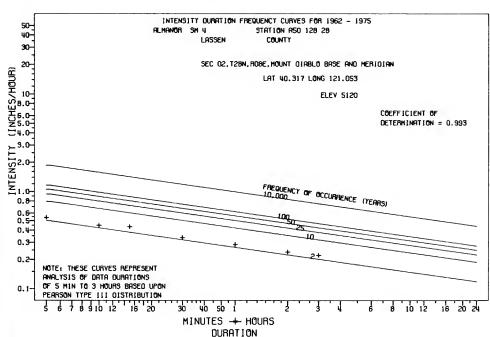


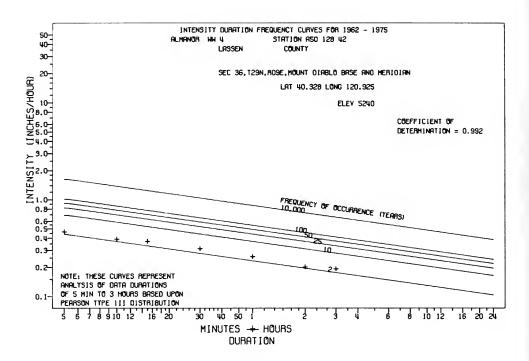


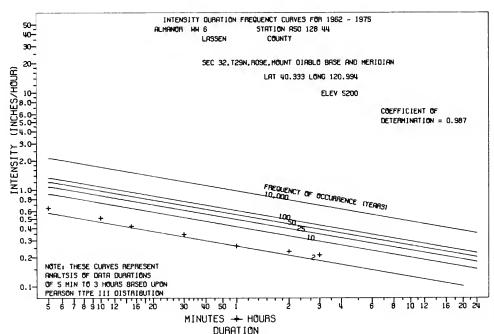


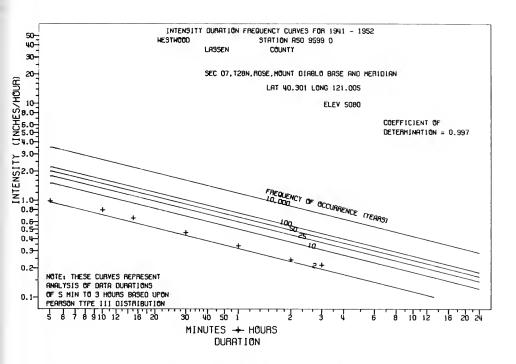


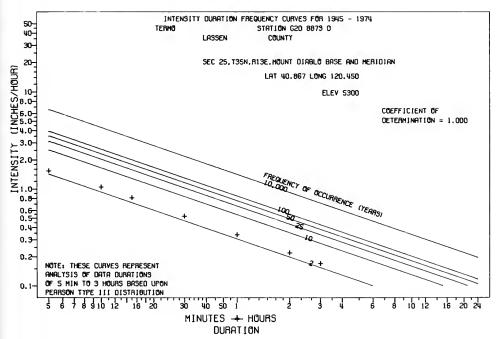


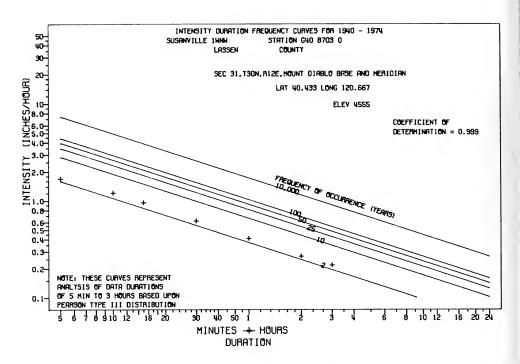


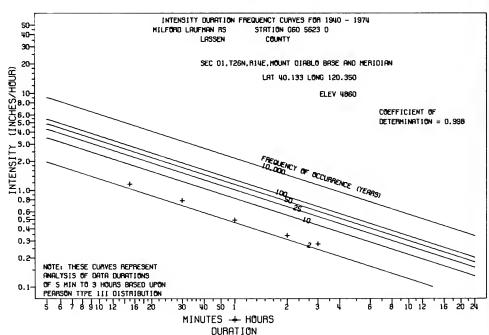


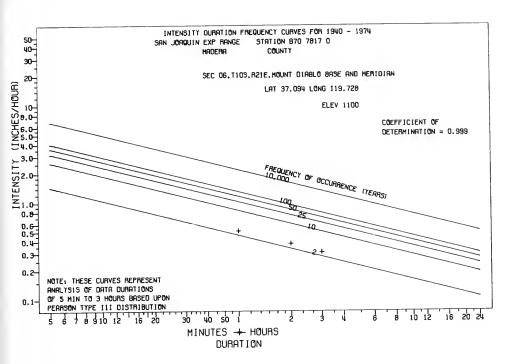


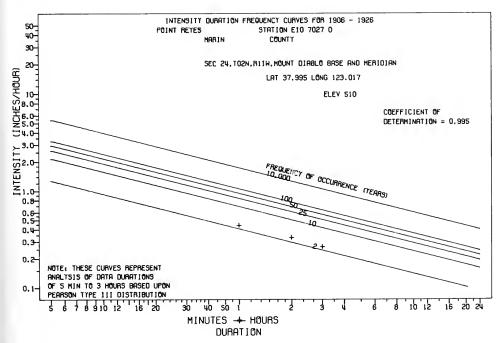


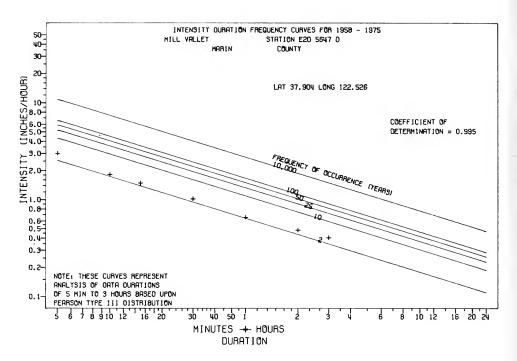


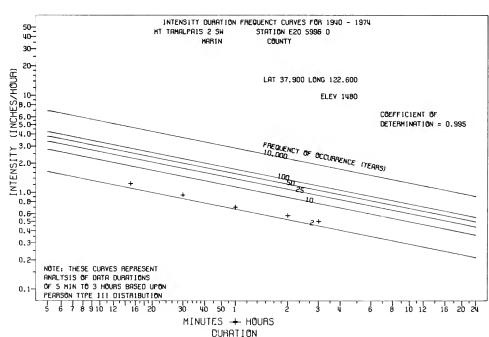


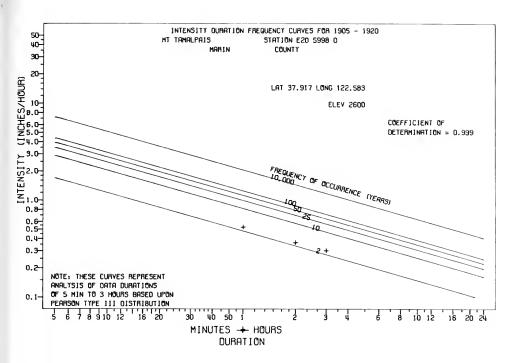


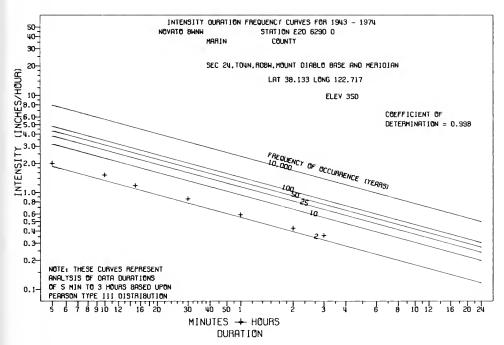


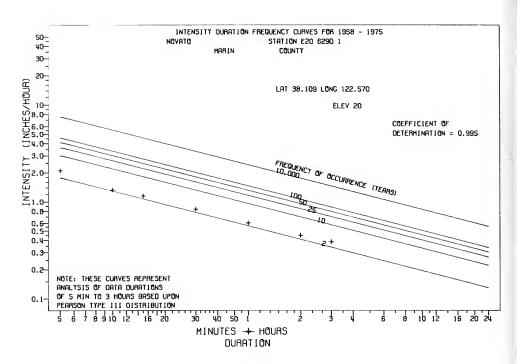


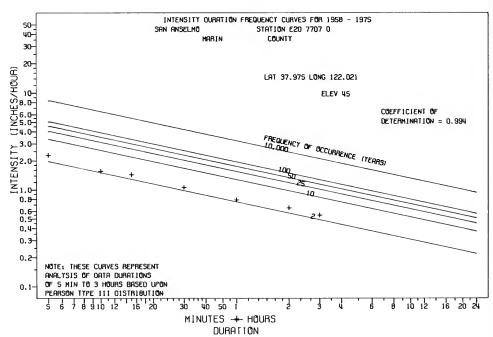


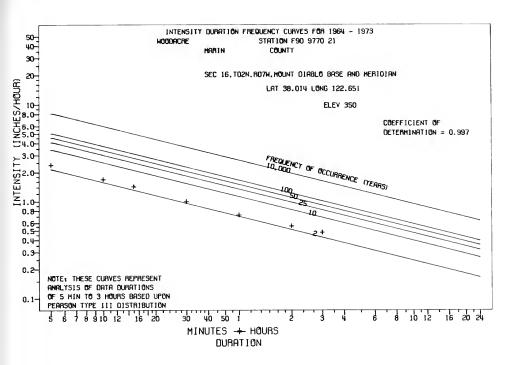


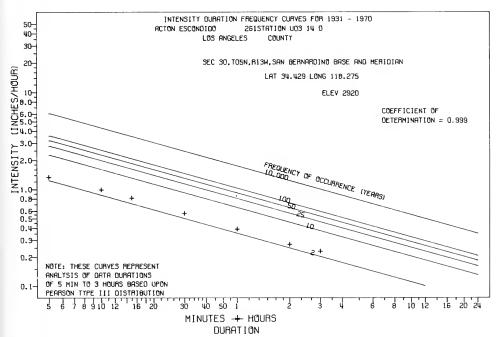


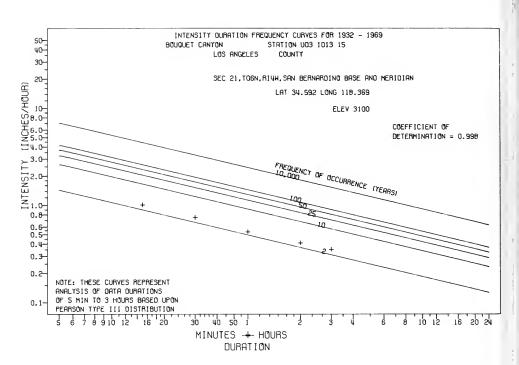


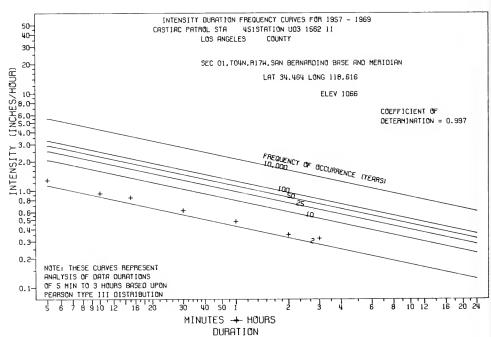


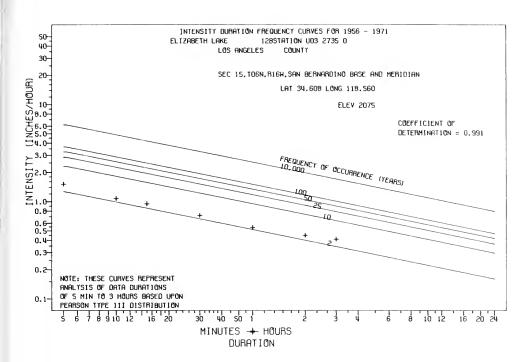


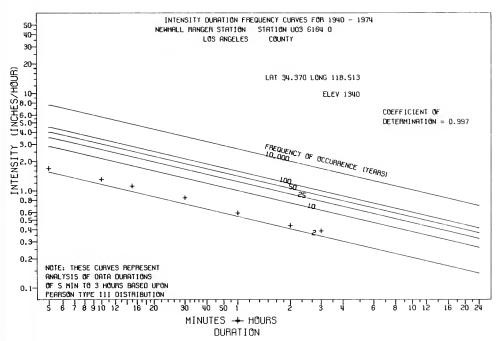


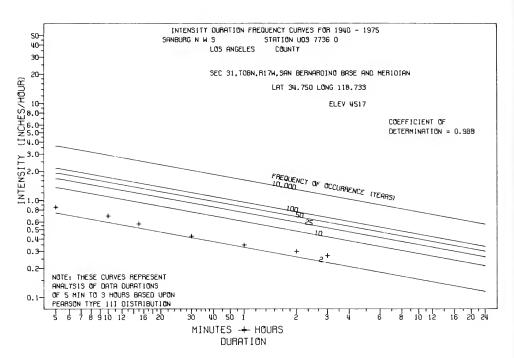


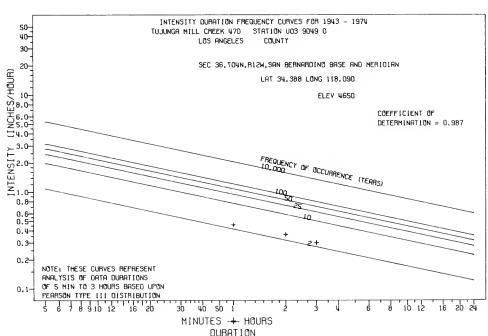


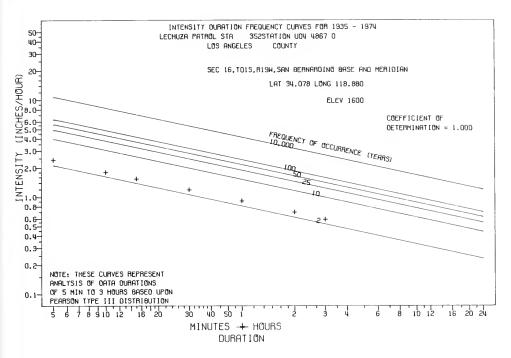


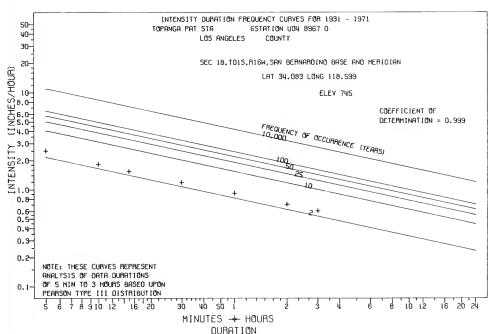


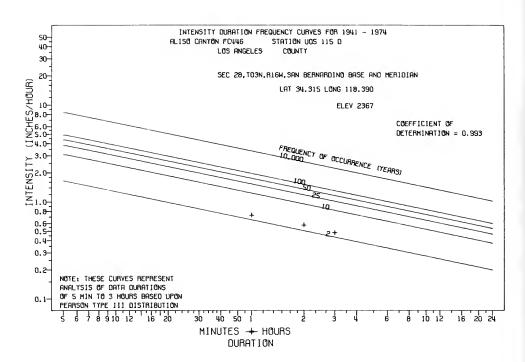


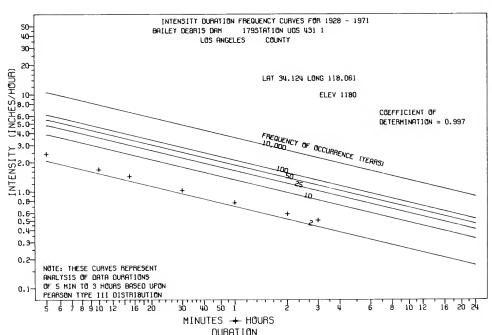


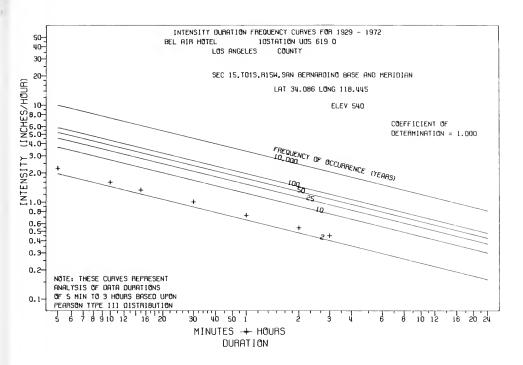


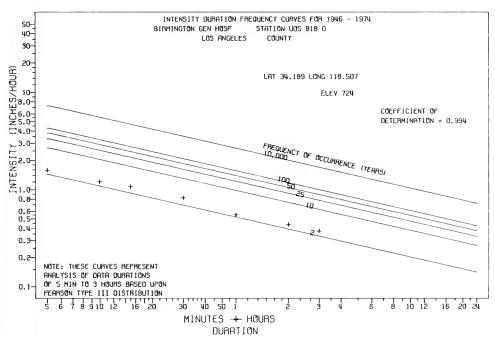


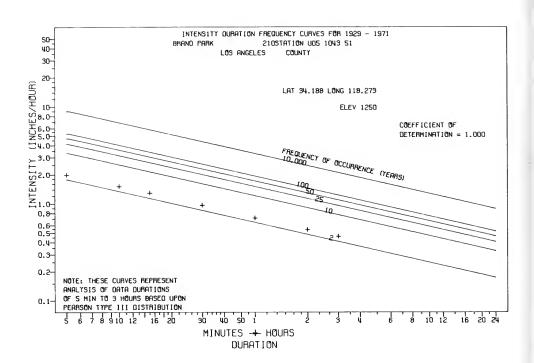


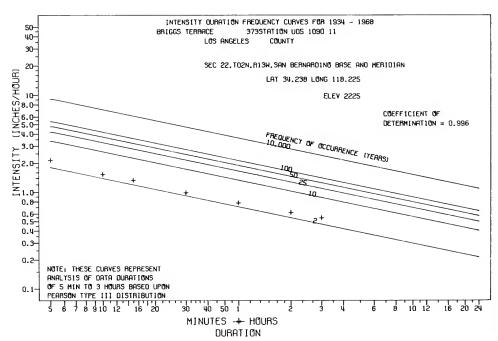


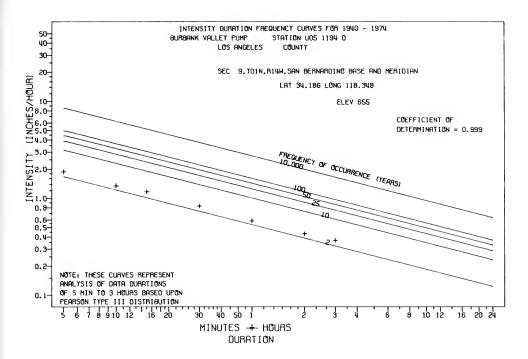


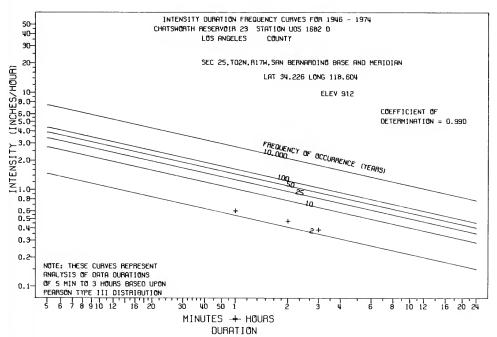


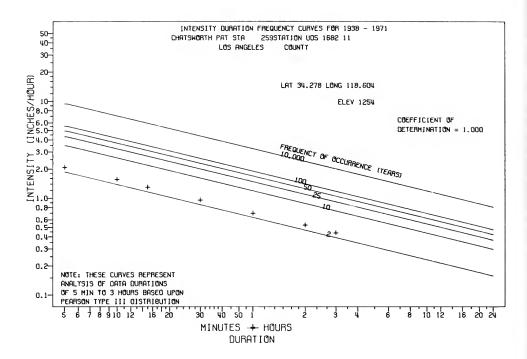


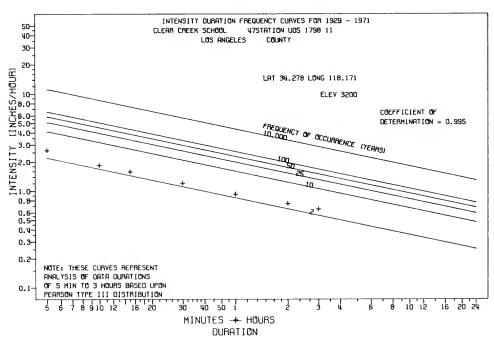


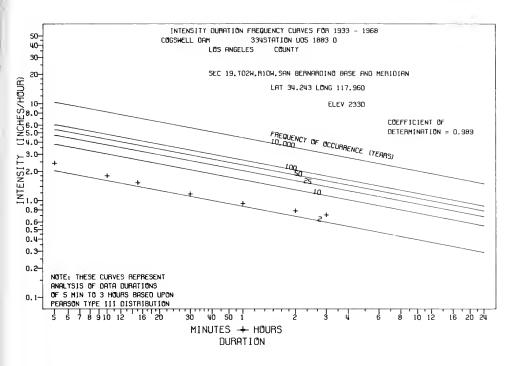


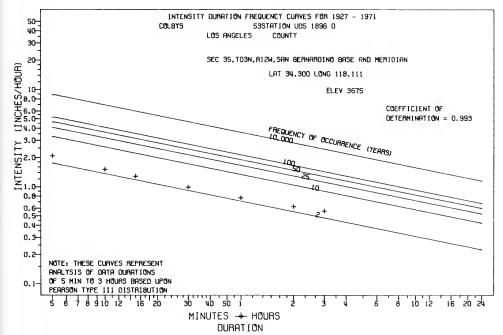


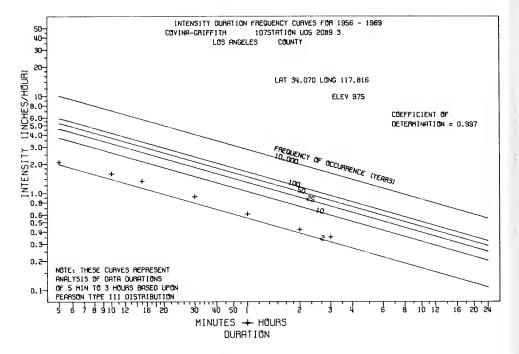


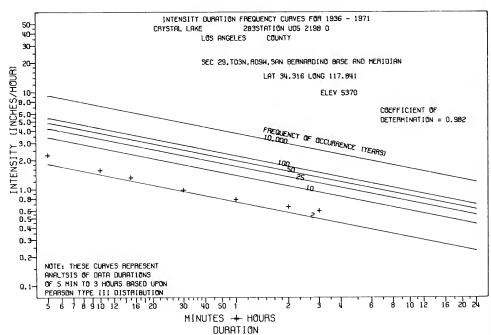


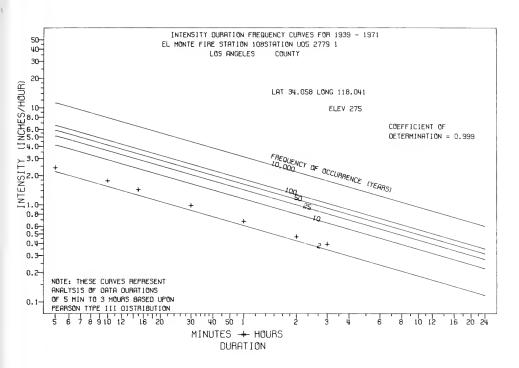


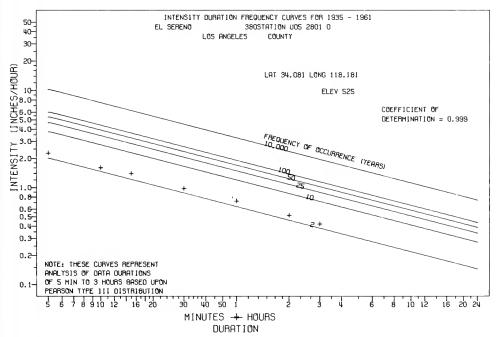


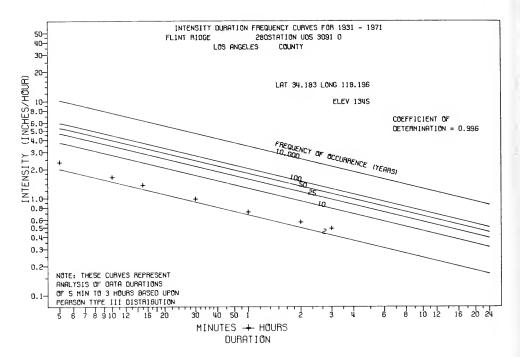


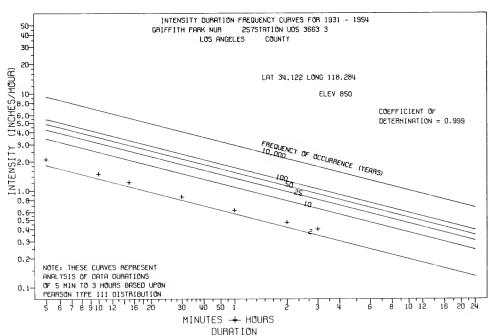


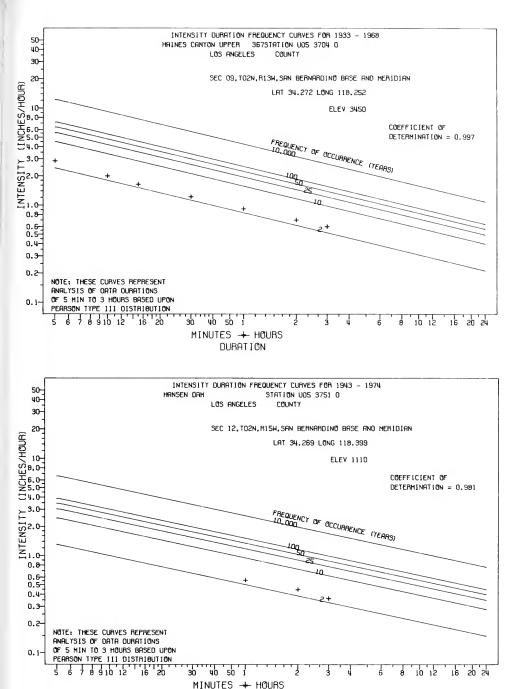




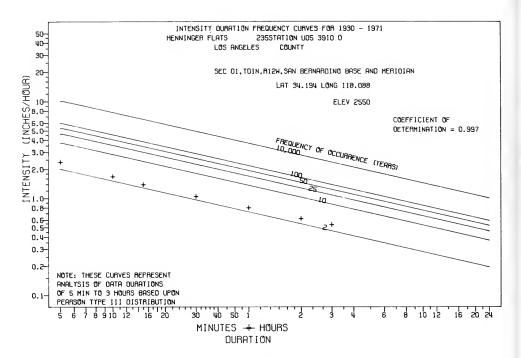


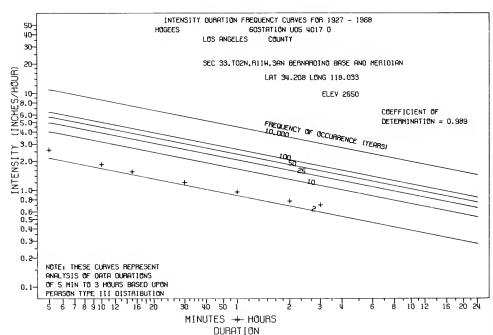


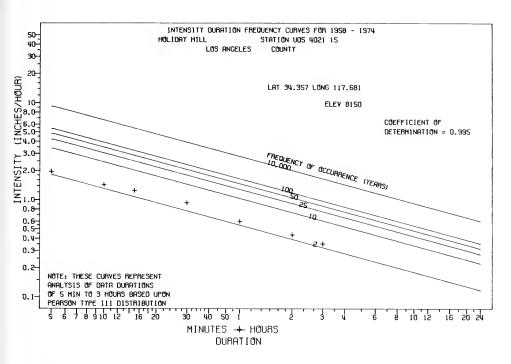


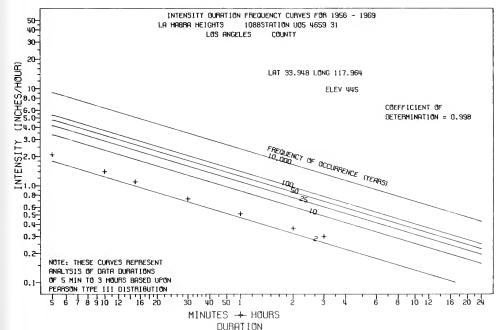


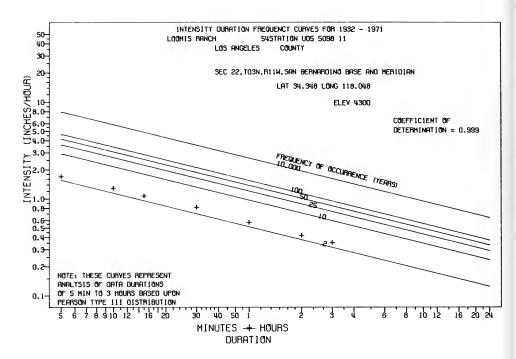
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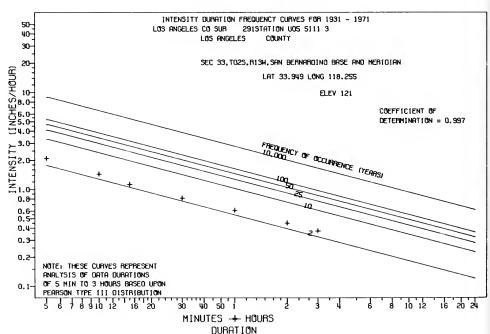


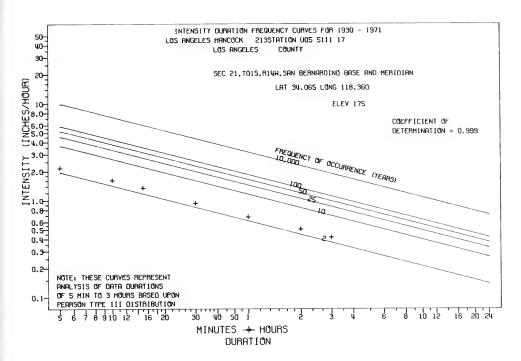


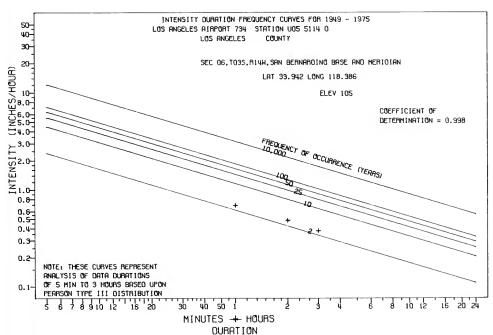


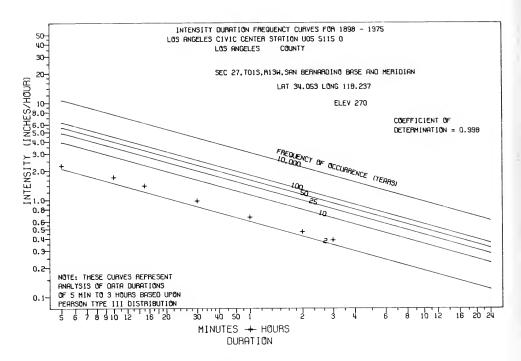


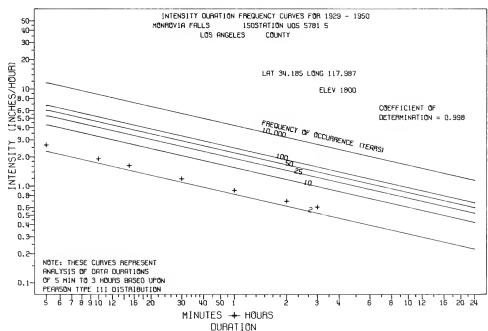


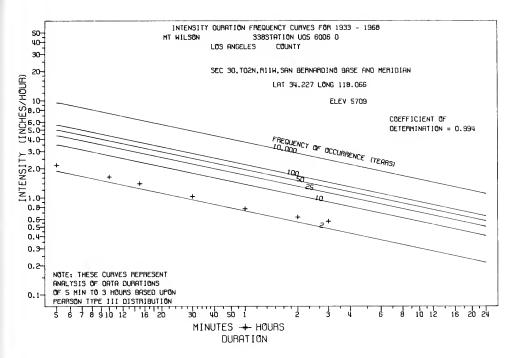


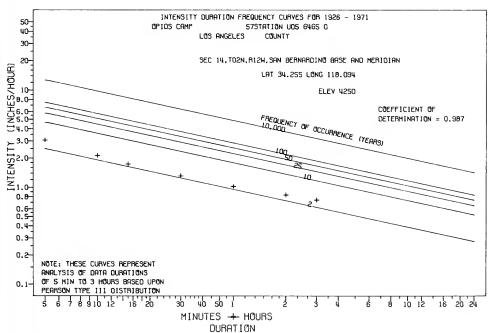


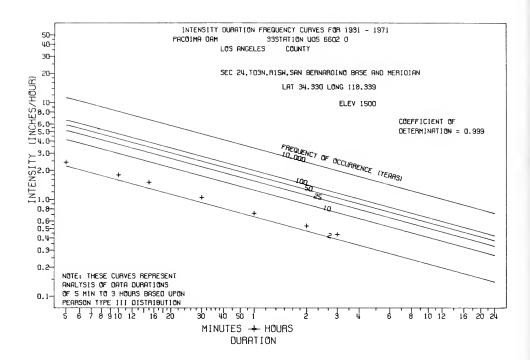


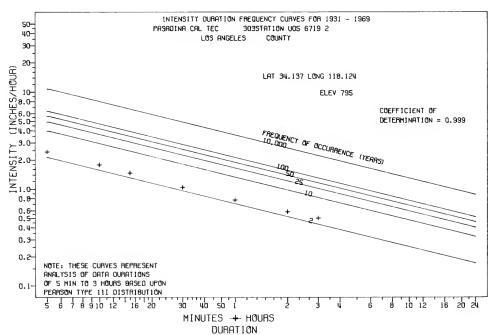


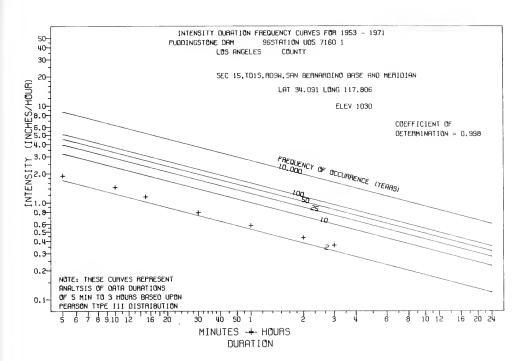


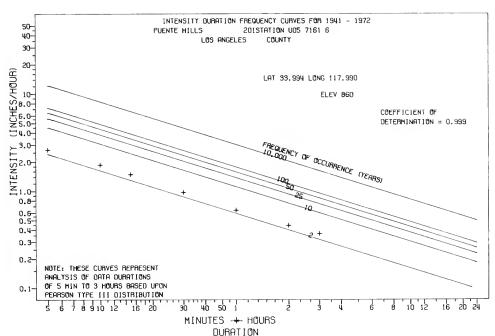


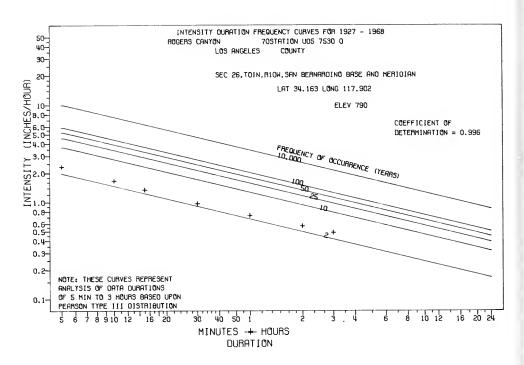


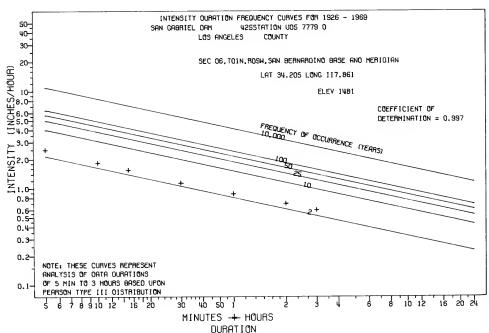


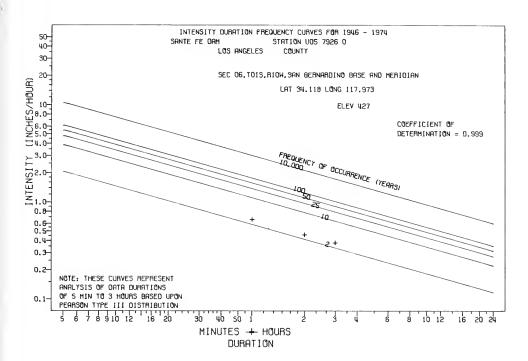


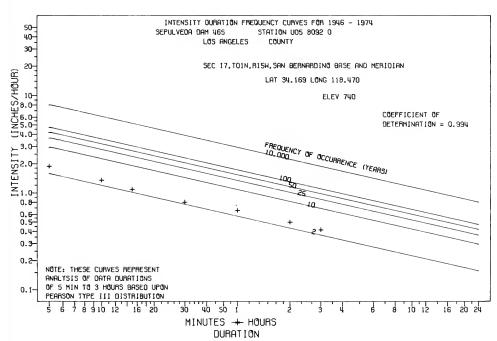


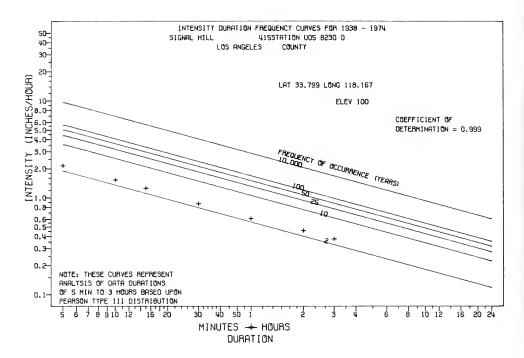


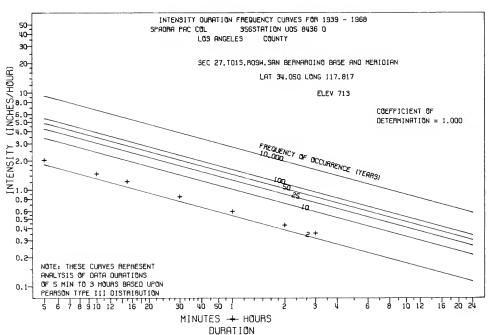


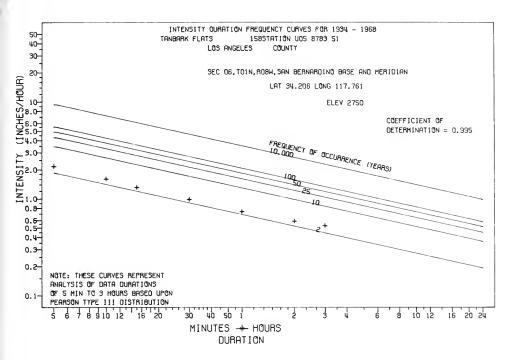


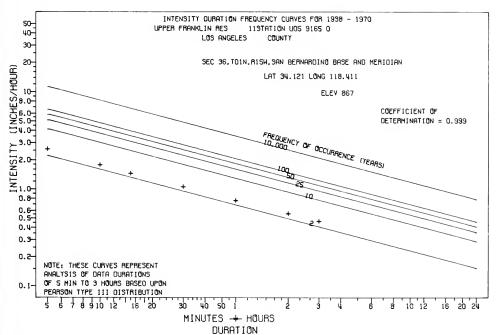


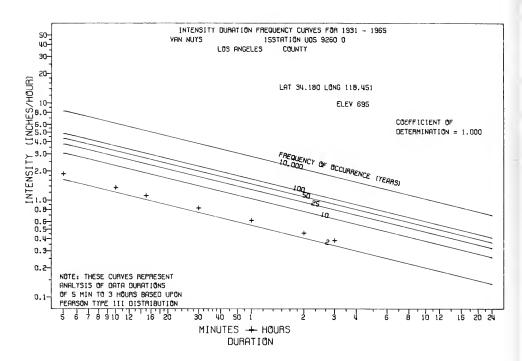


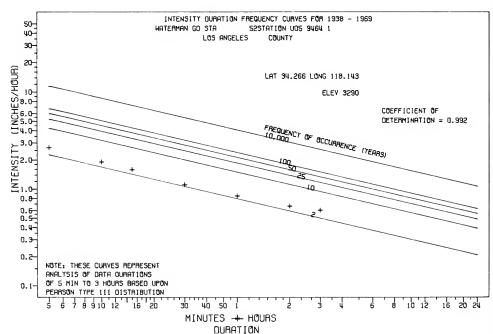


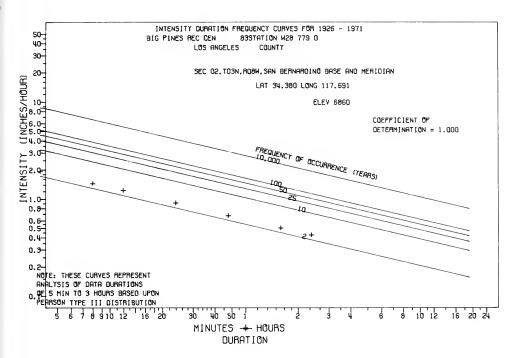


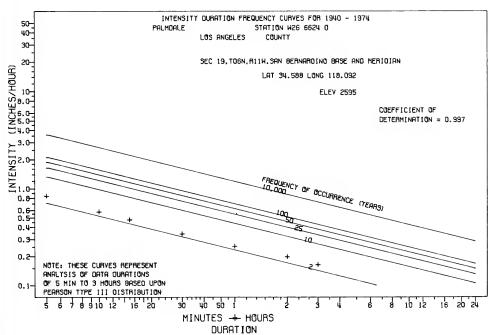


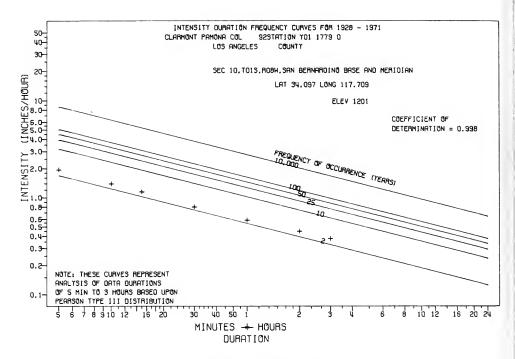


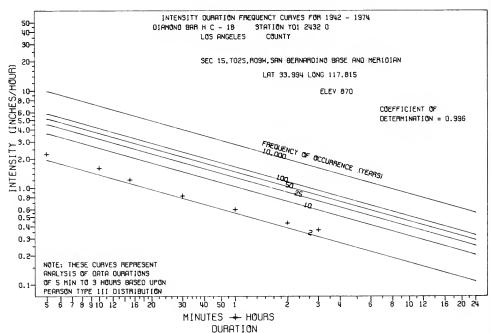


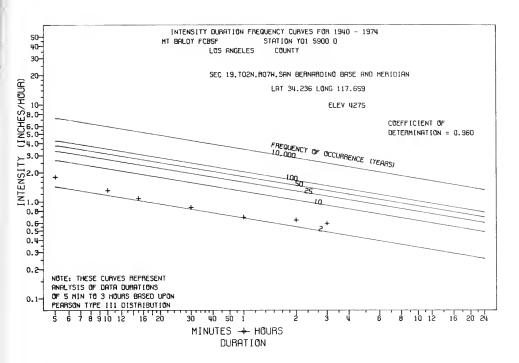


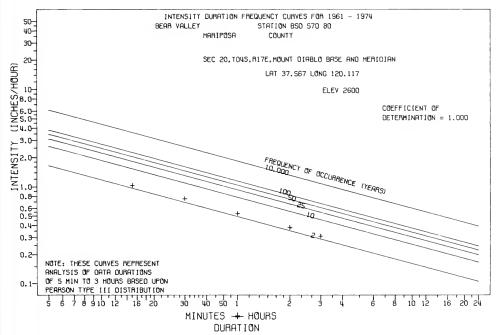


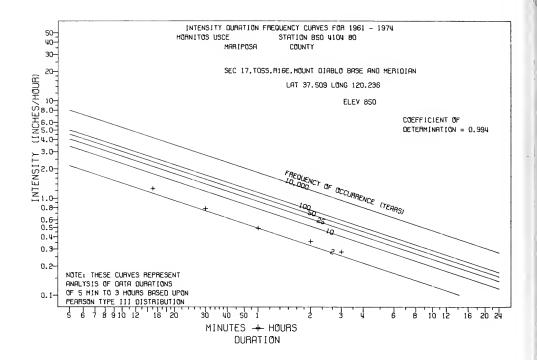


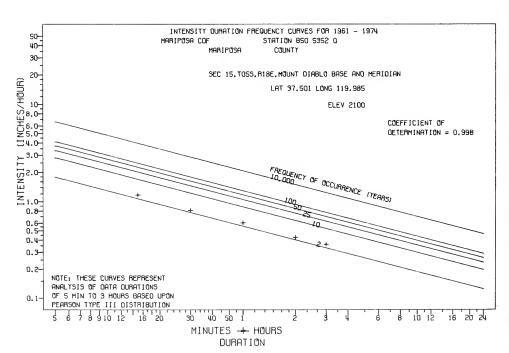


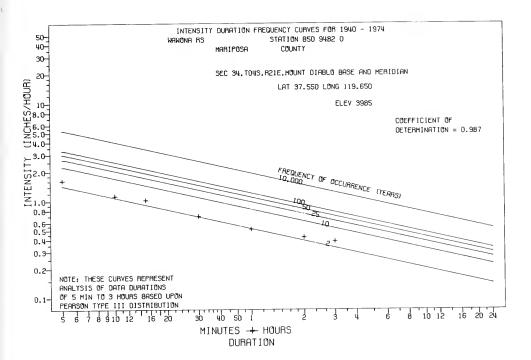


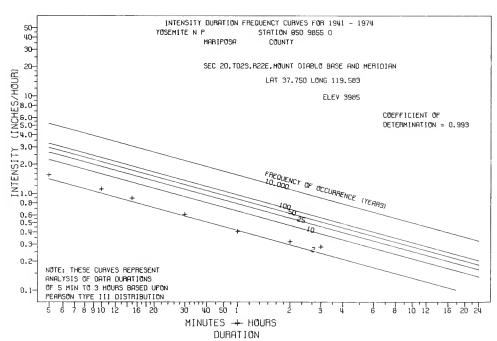


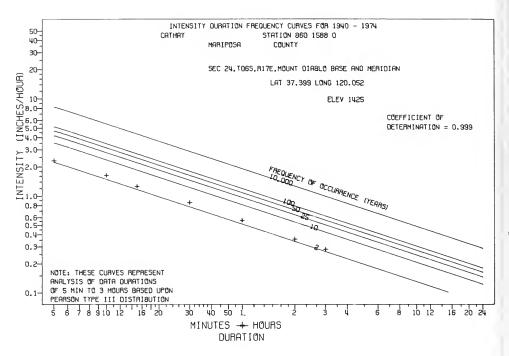


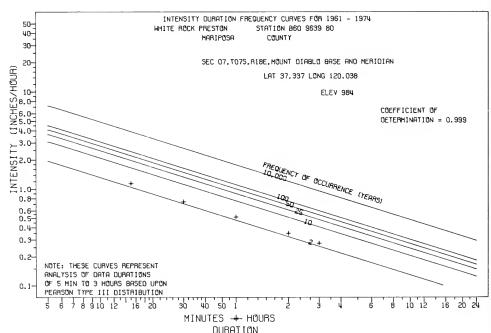


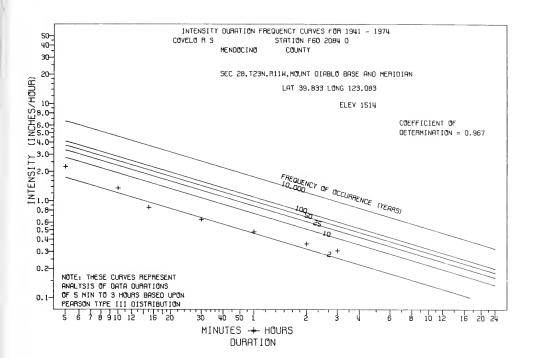


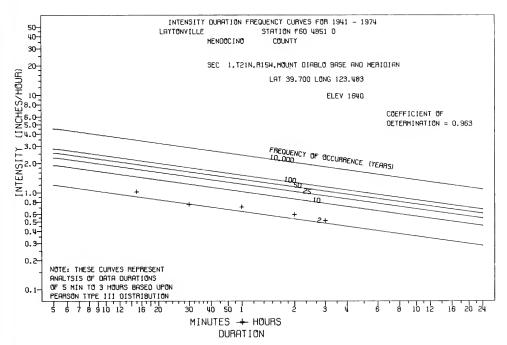


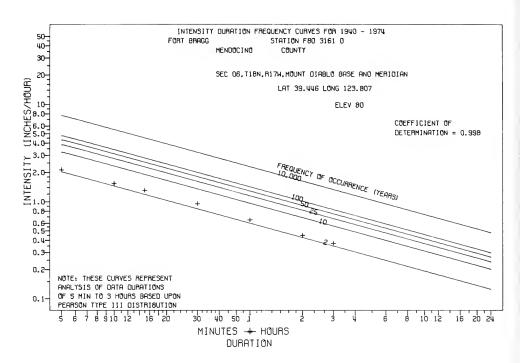


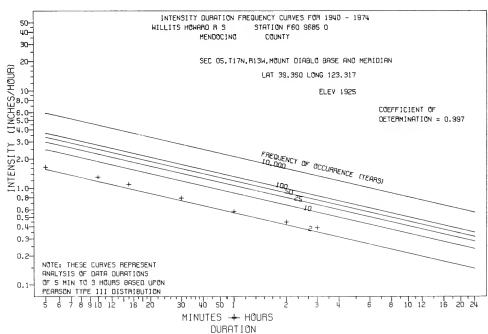


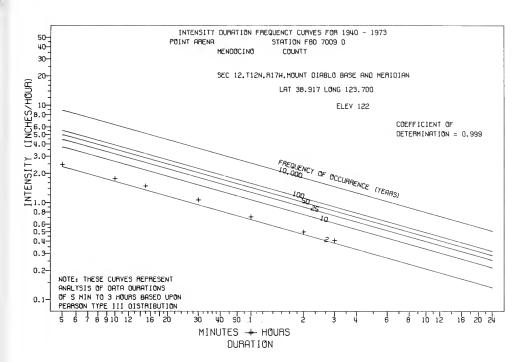


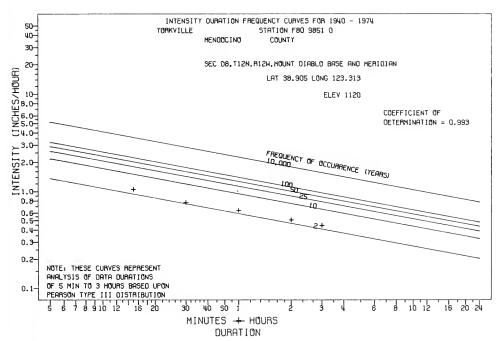


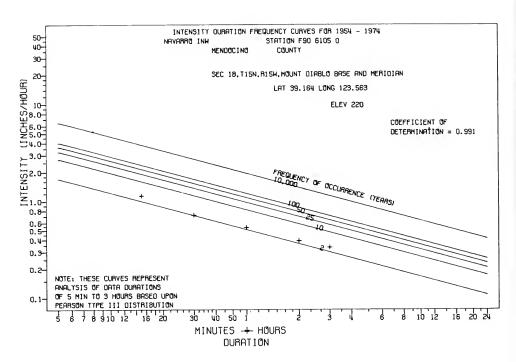


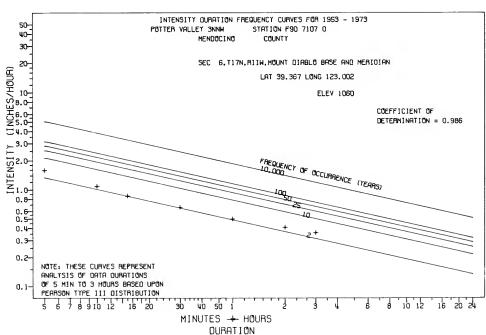


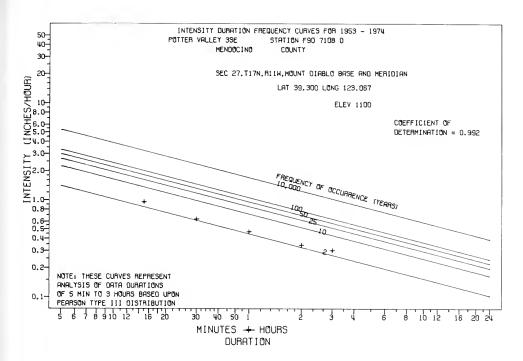


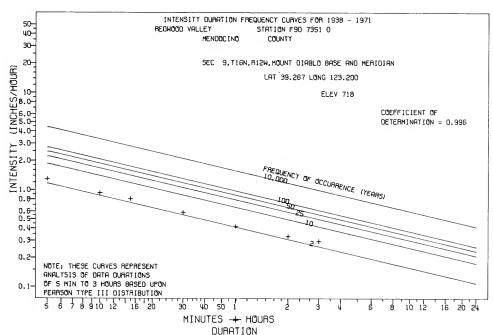


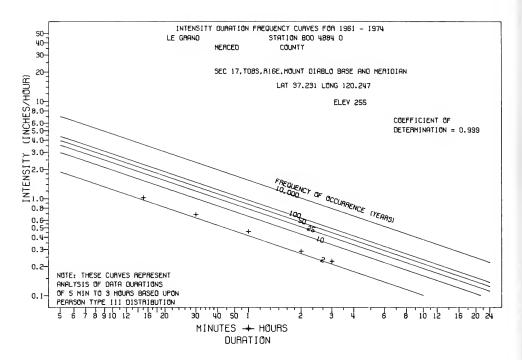


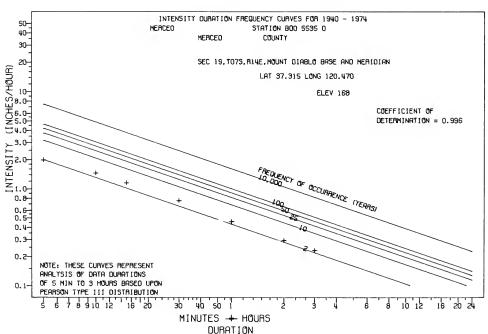


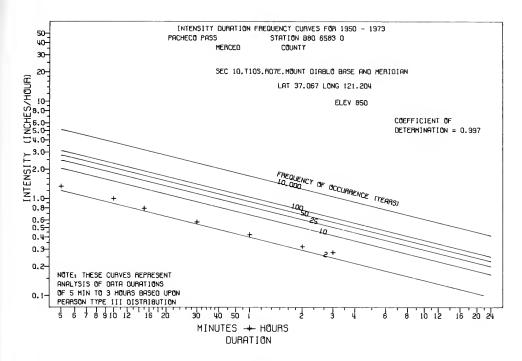


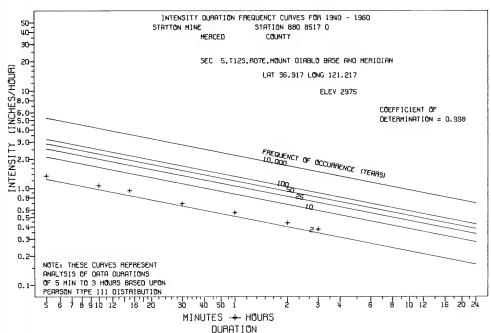


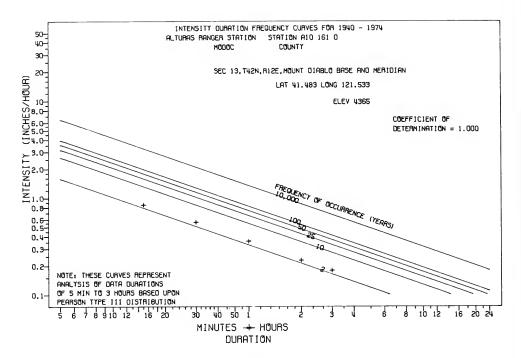


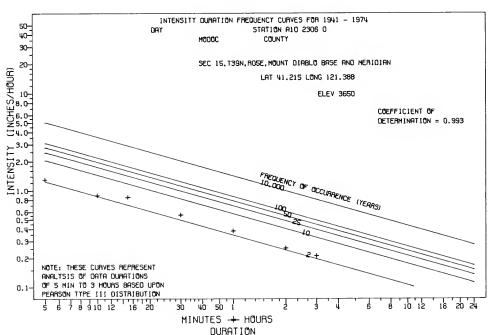


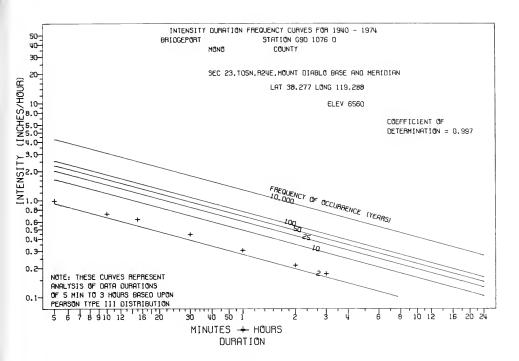


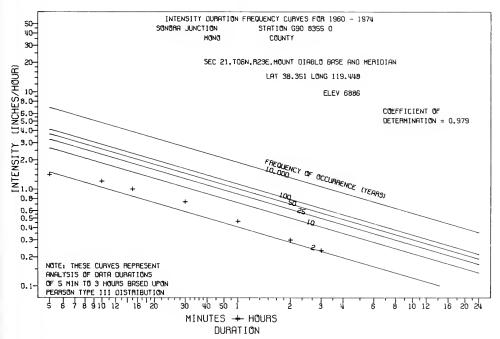


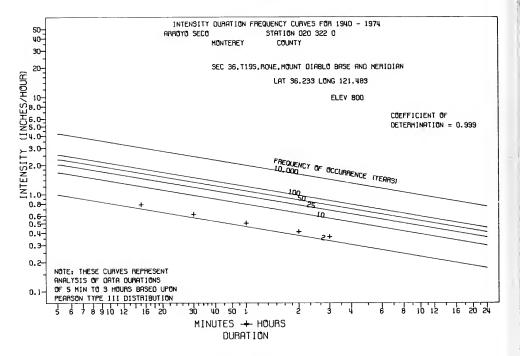


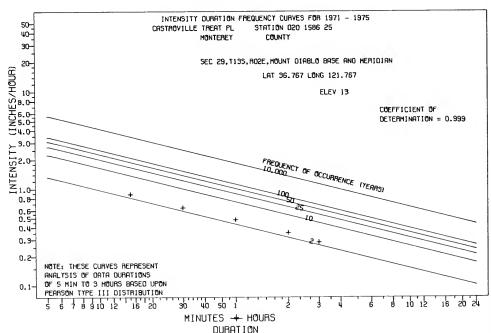


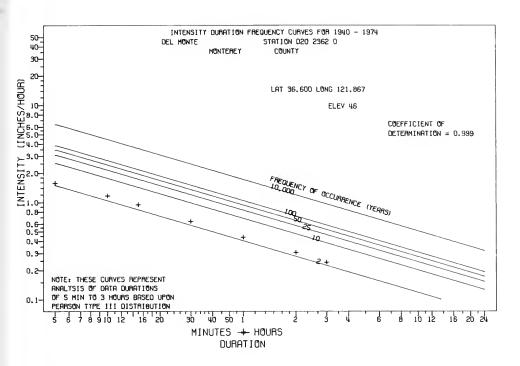


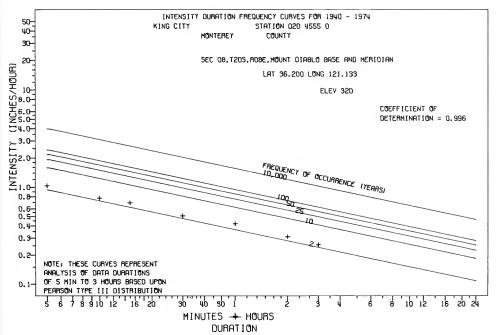


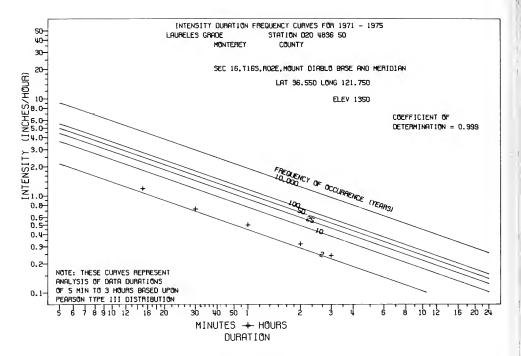


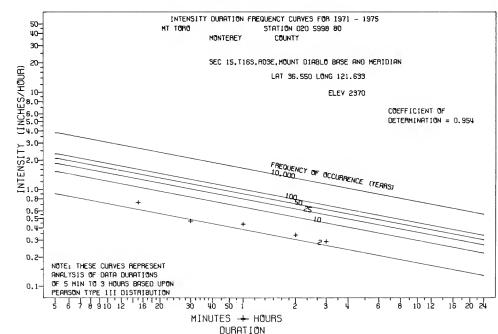


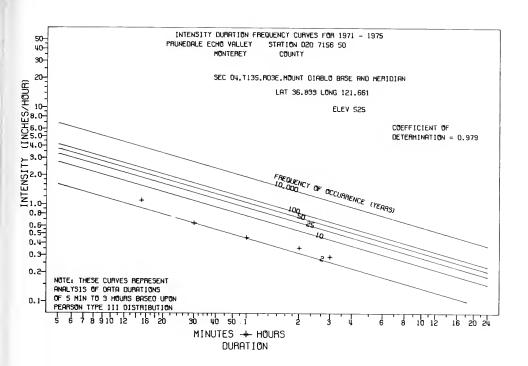


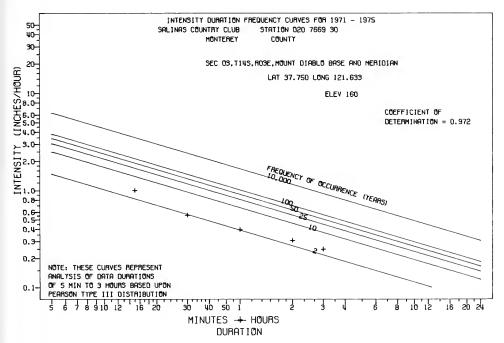


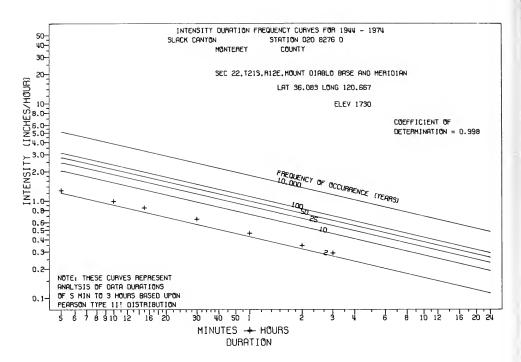


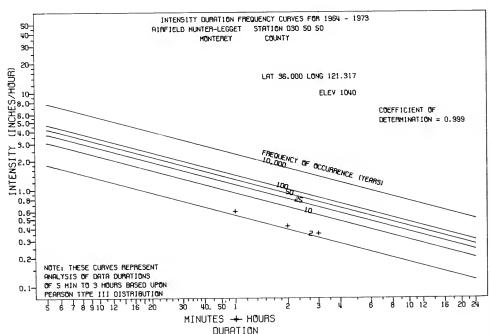


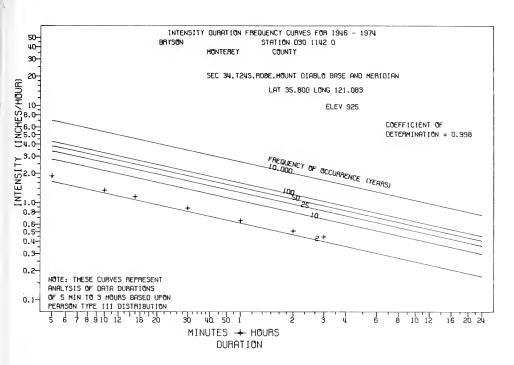


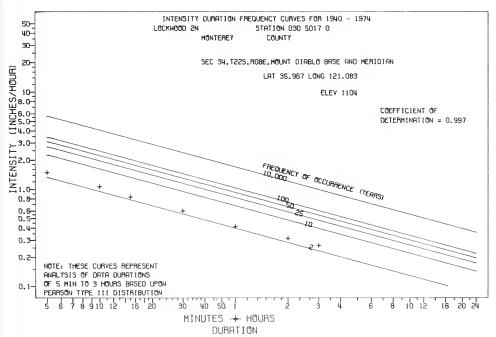


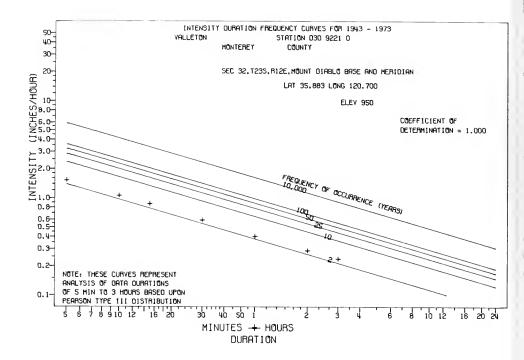


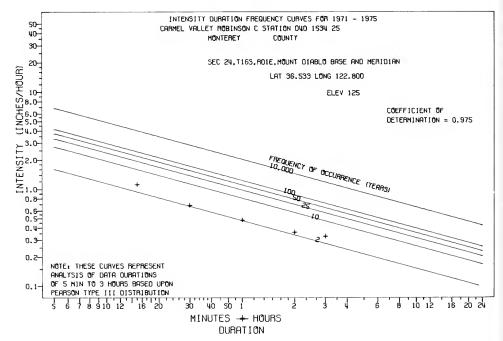


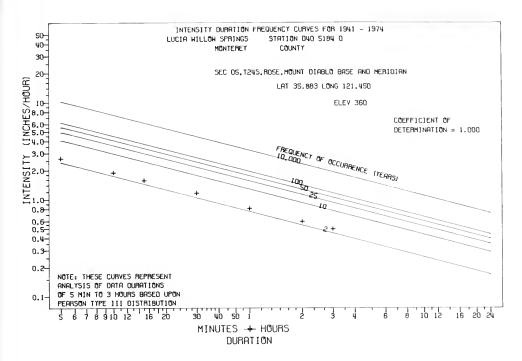


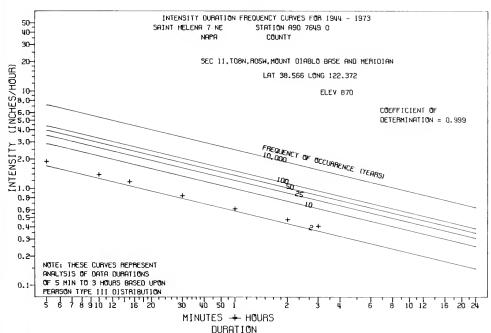


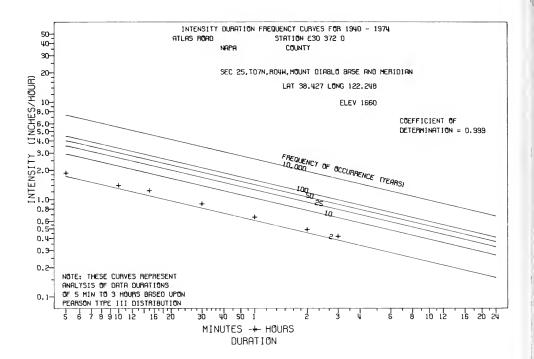


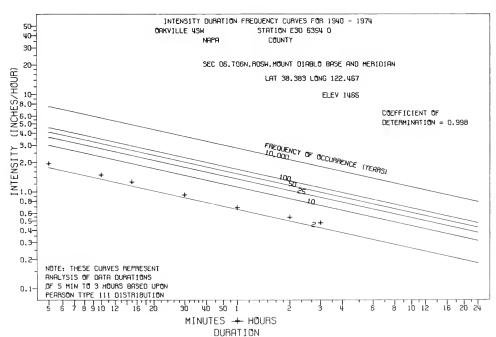


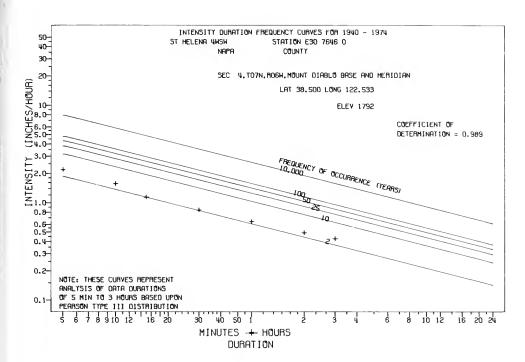


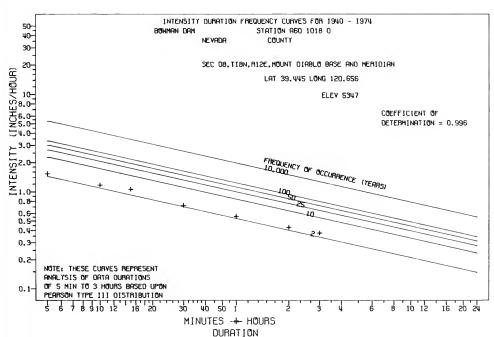


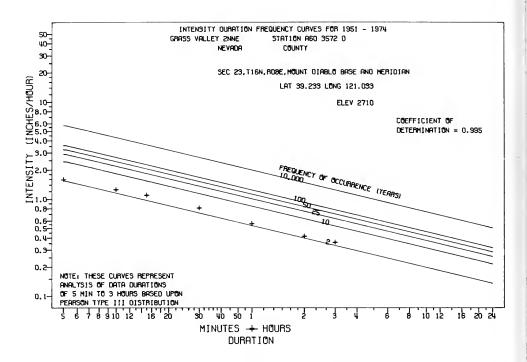


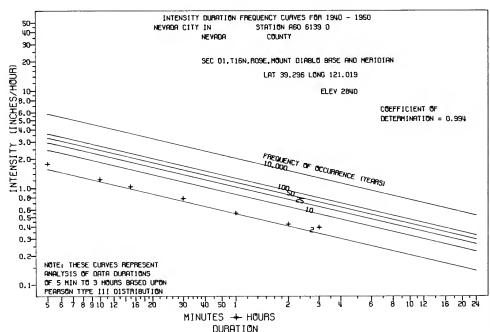


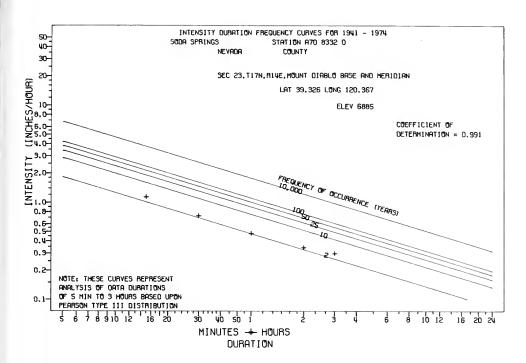


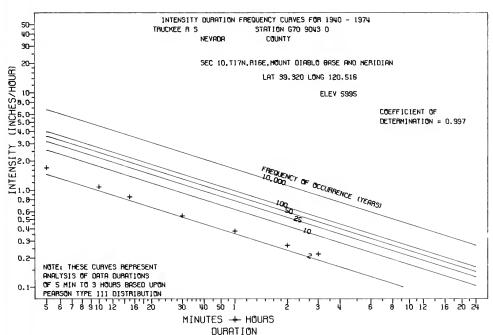


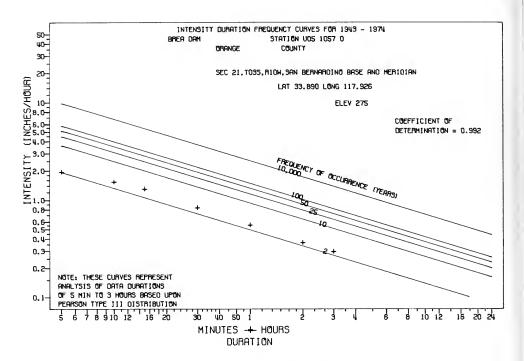


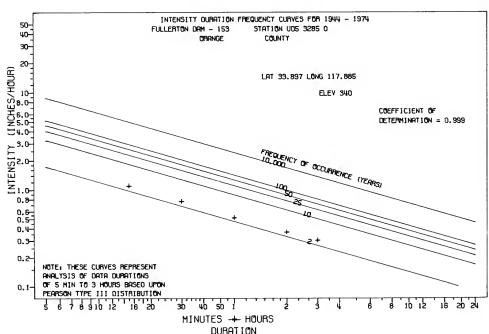


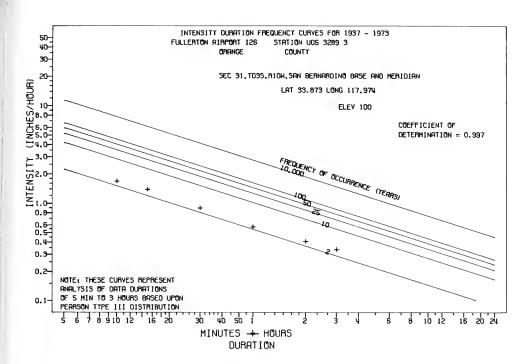


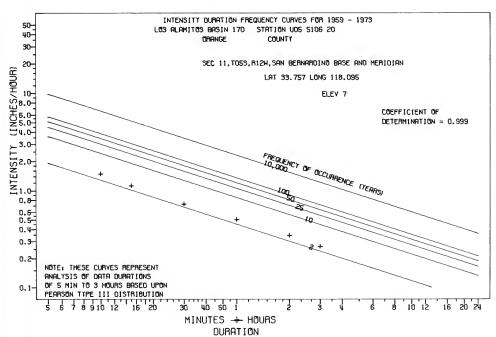


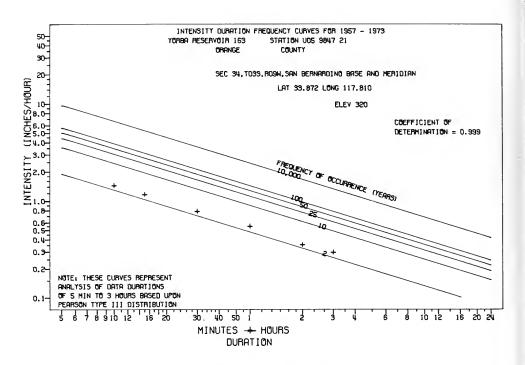


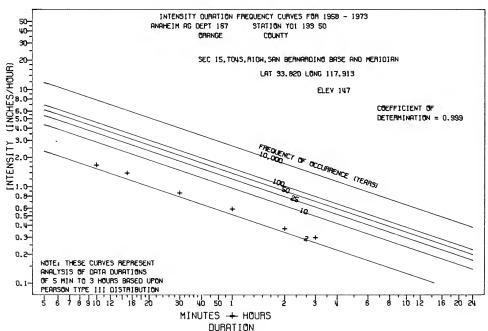


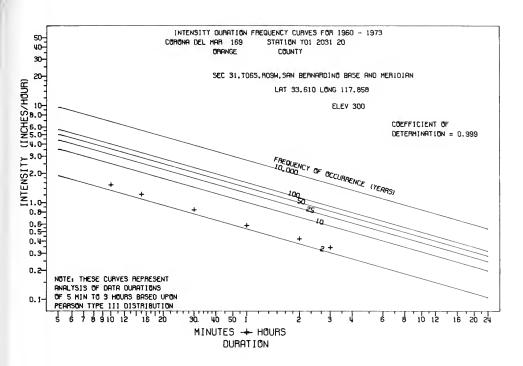


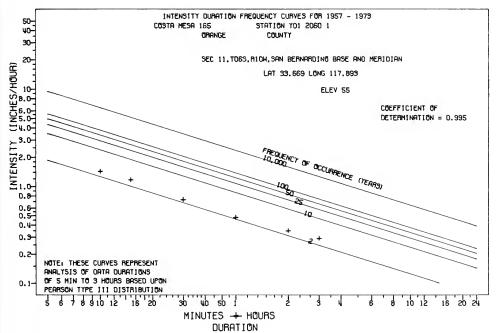


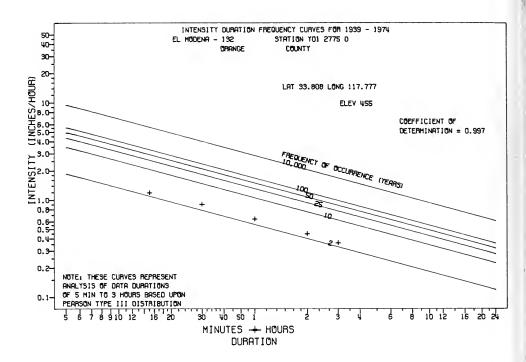


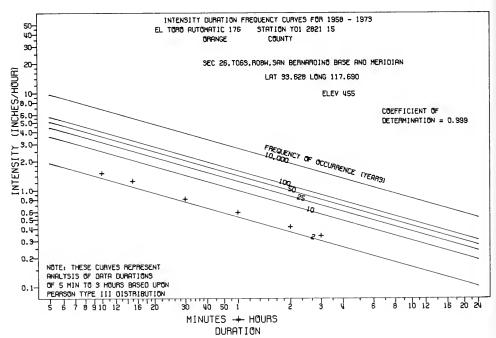


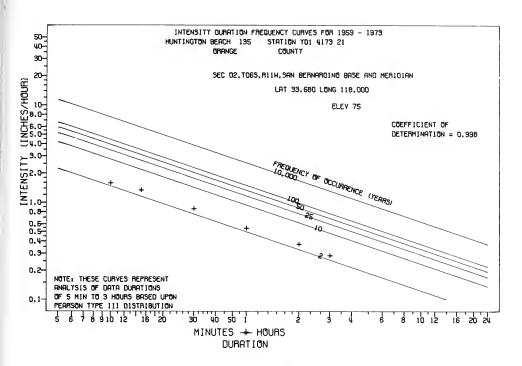


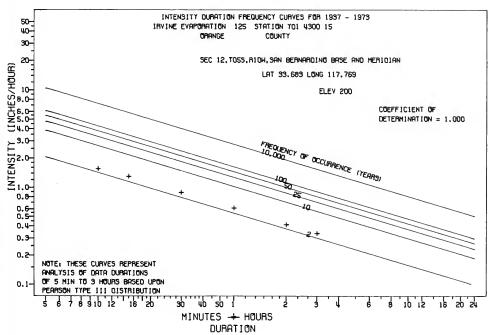


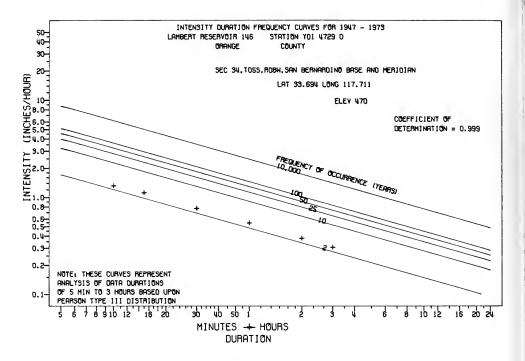


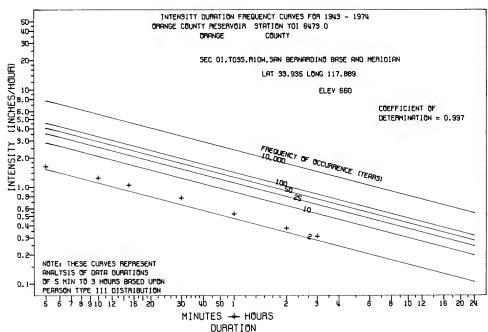


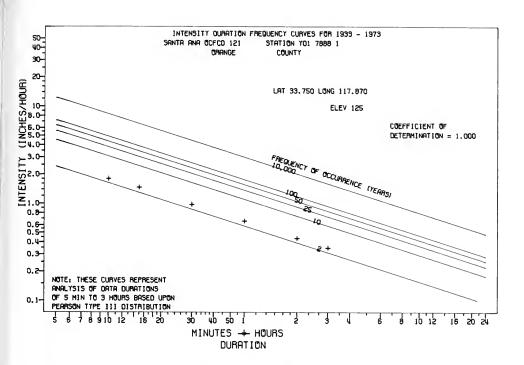


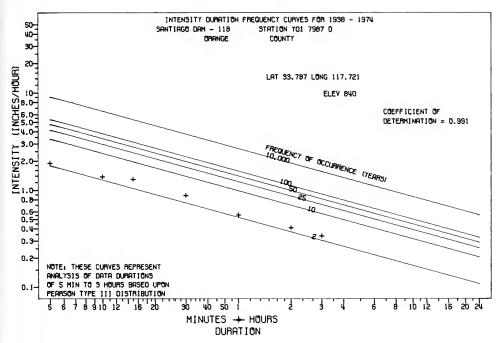


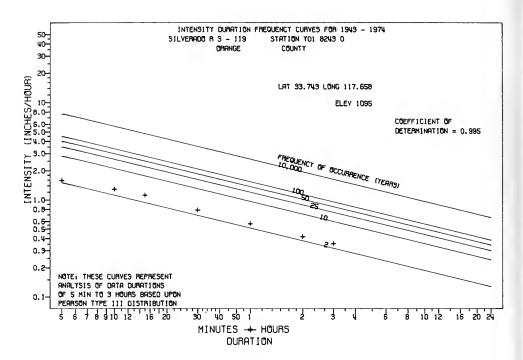


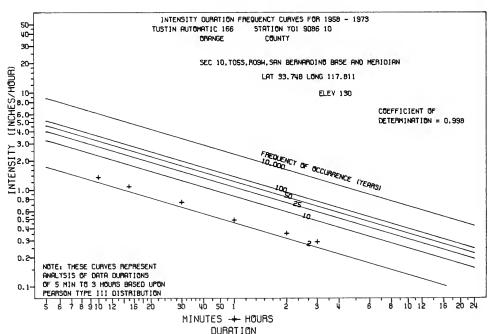


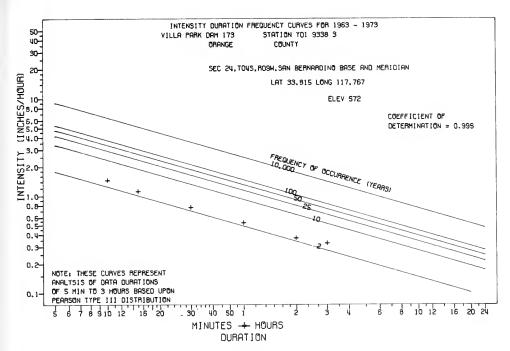


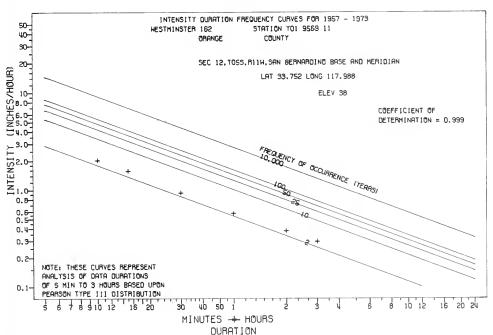


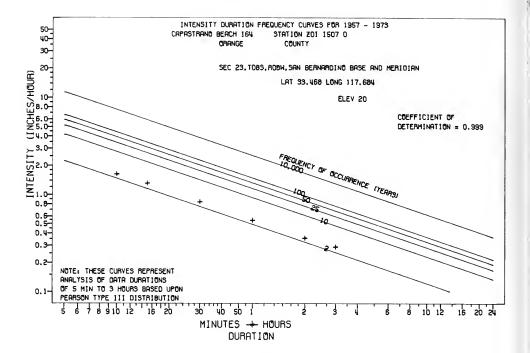


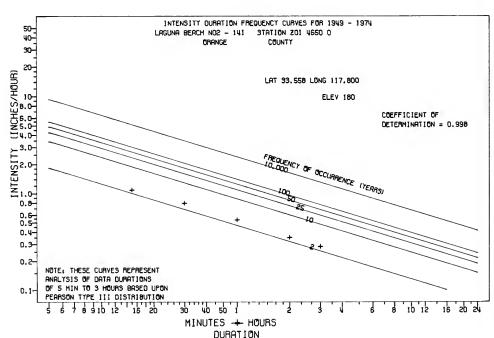


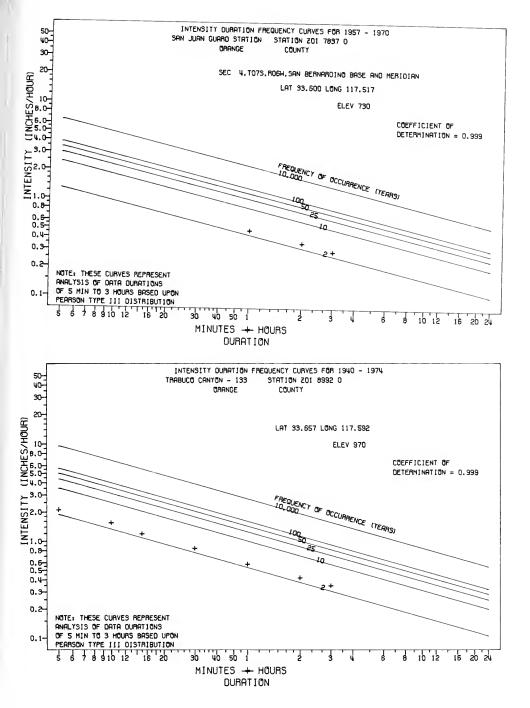


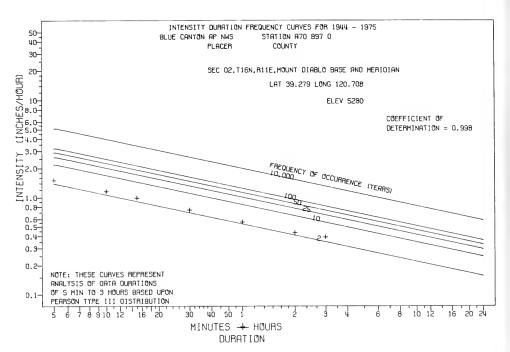


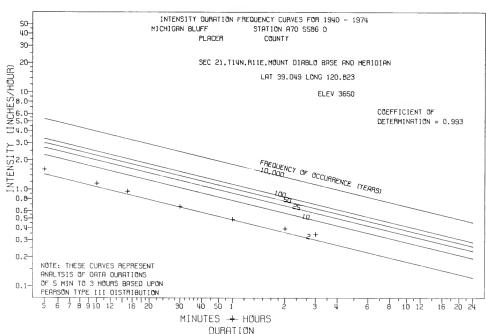


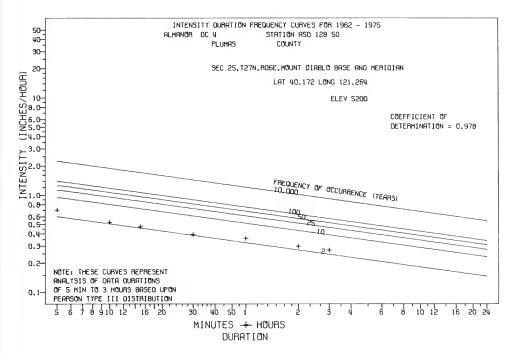


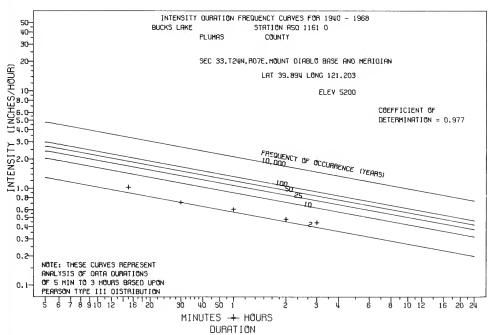


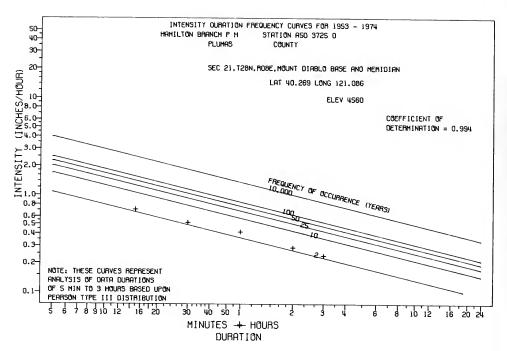


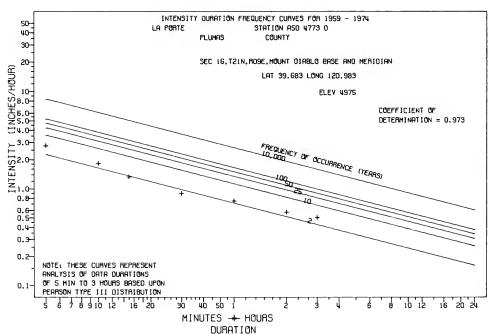


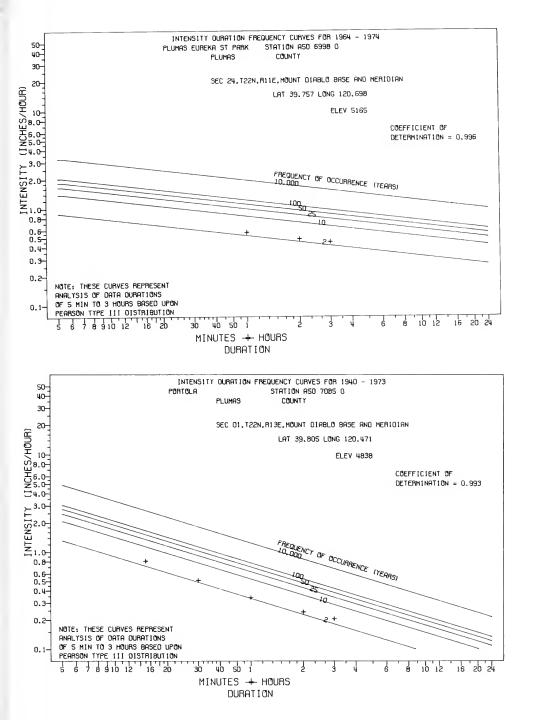


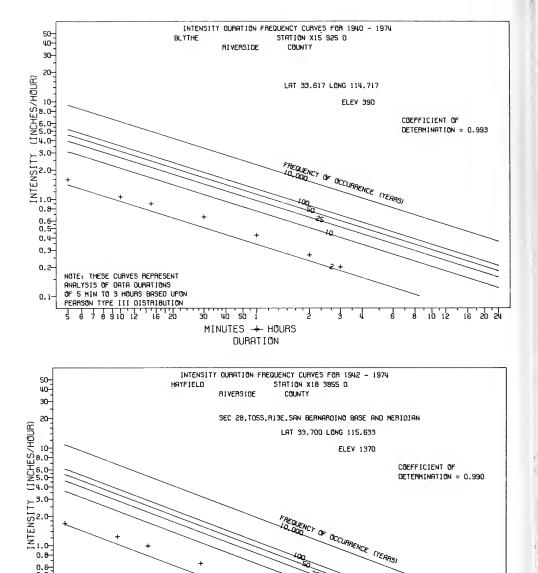












10 12

20 24

40 50 1

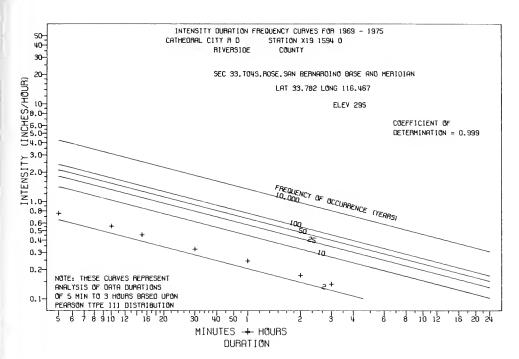
MINUTES + HOURS
DURATION

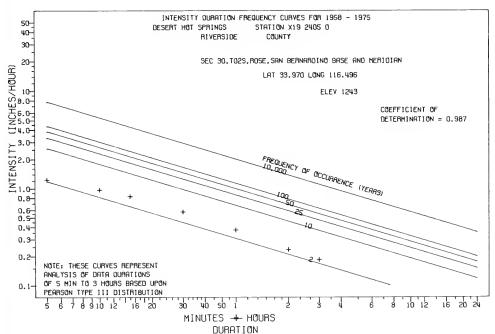
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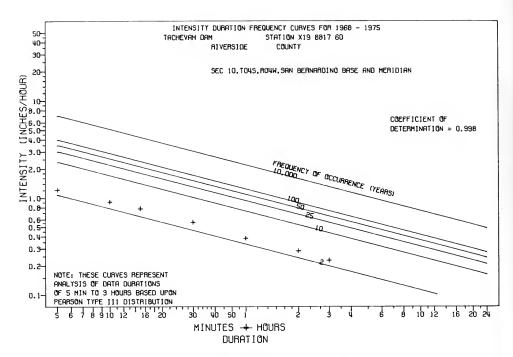
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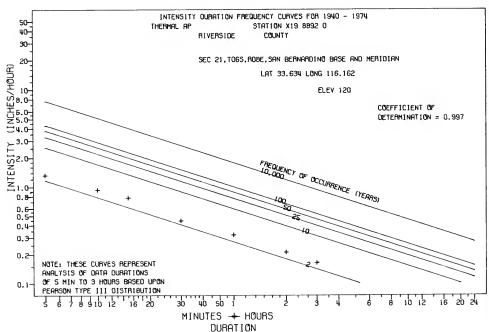
NOTE: THESE CURVES REPRESENT ANALYSIS OF DATA DURATIONS OF 5 MIN TO 3 HOURS BASED UPON

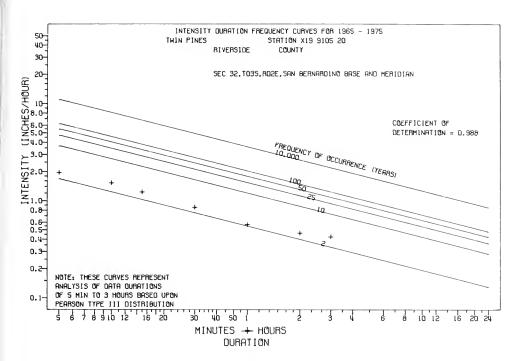
PEARSON TYPE 111 DISTRIBUTION
5 6 7 8 9 10 12 16 20

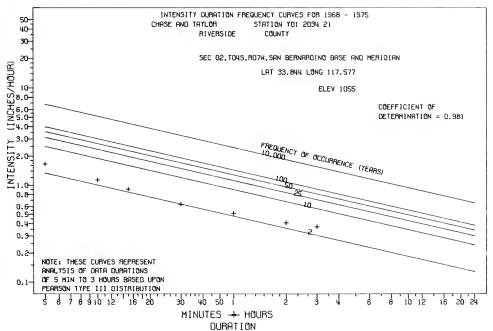


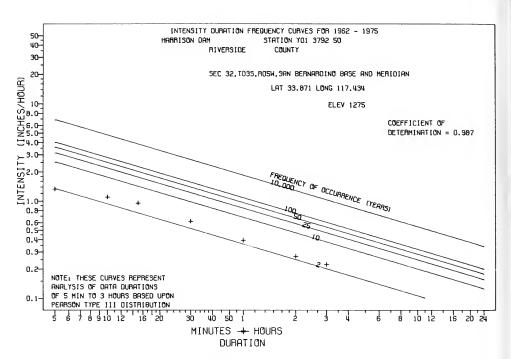


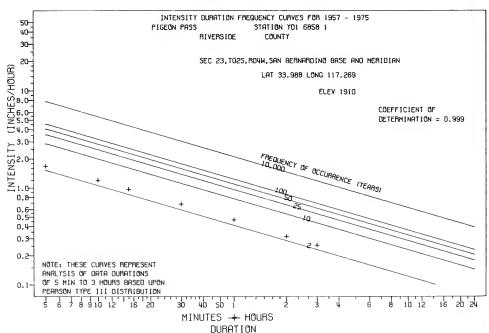


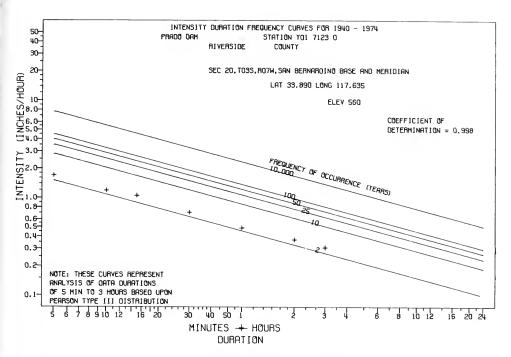


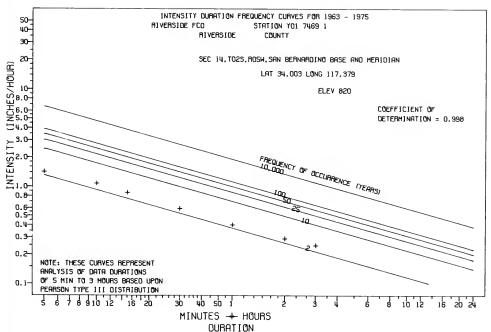


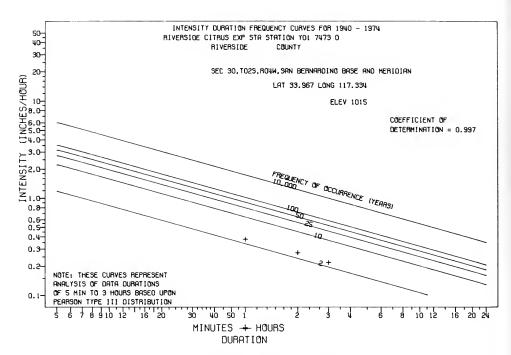


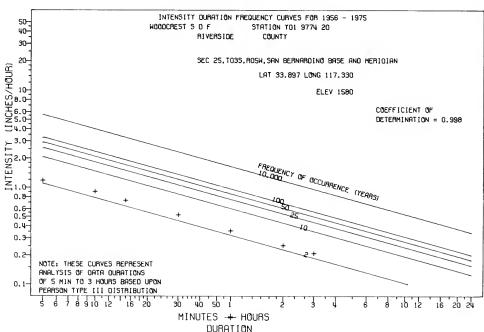


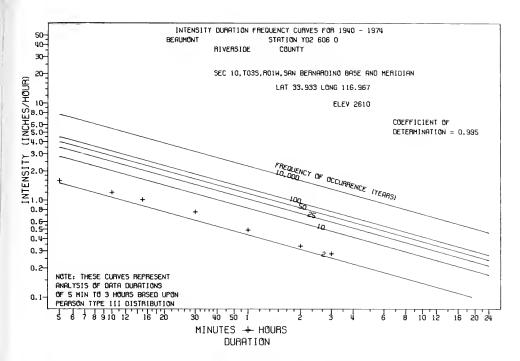


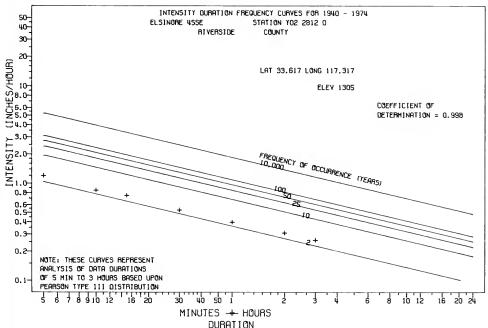


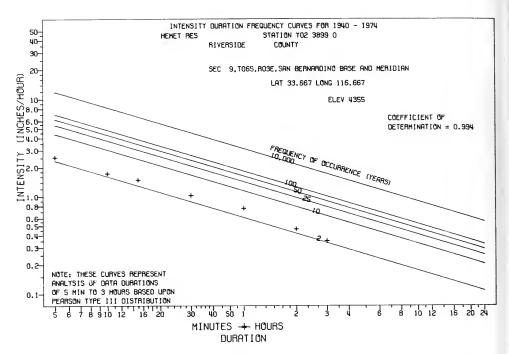


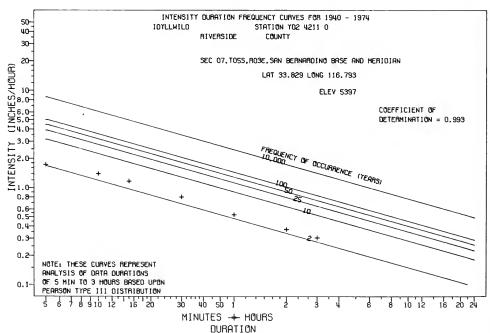


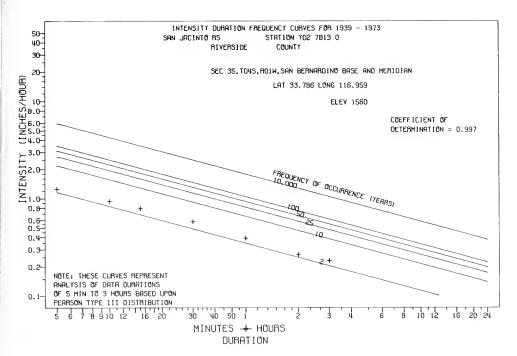


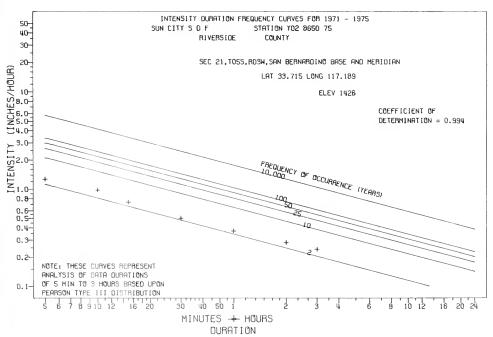


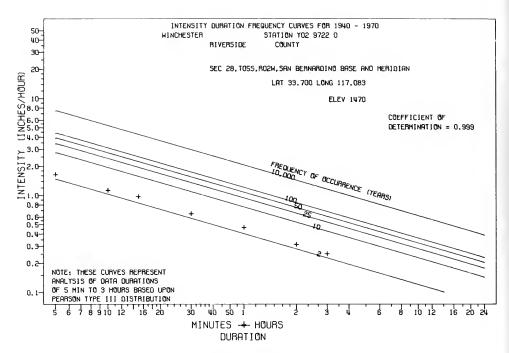


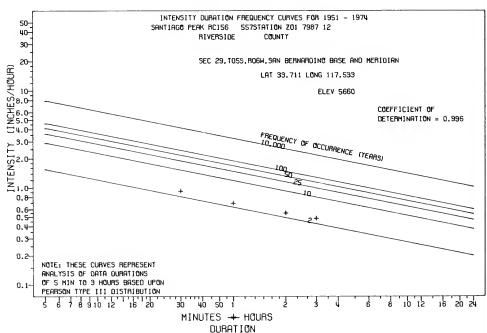


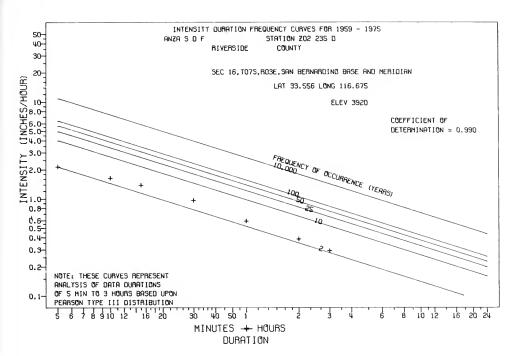


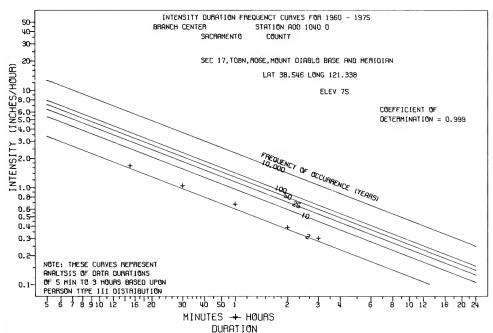


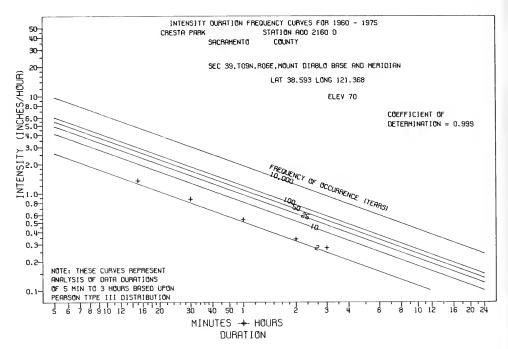


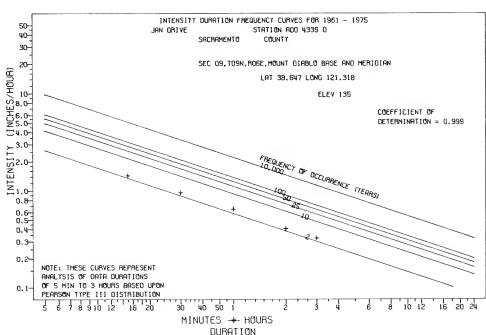


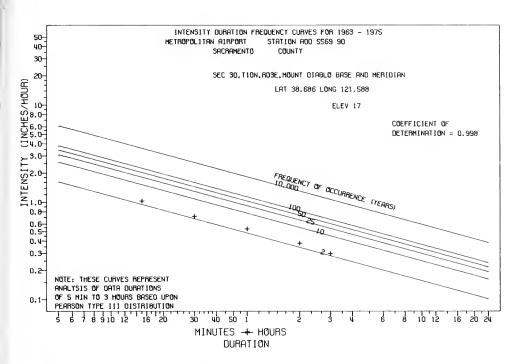


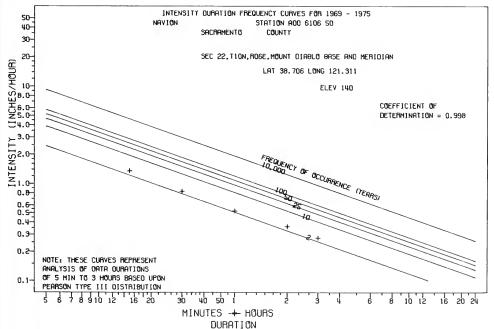


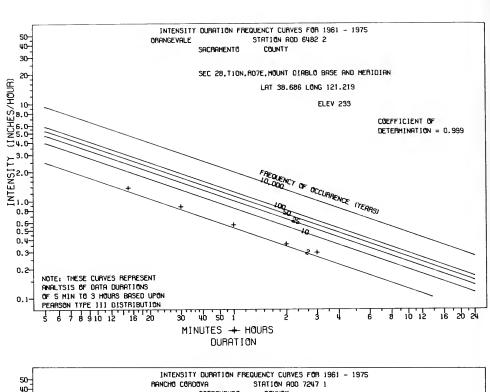


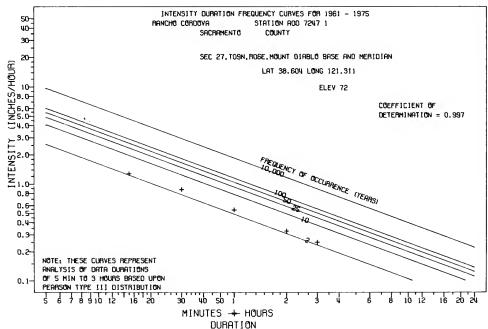


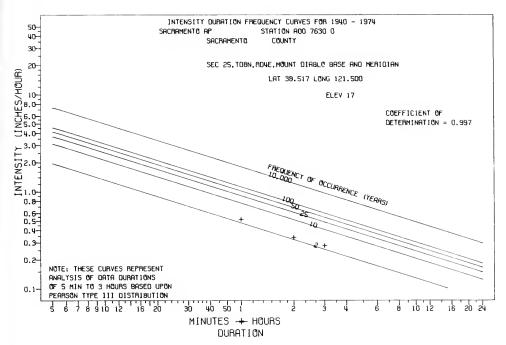


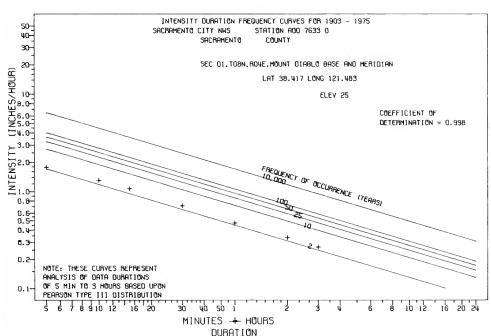


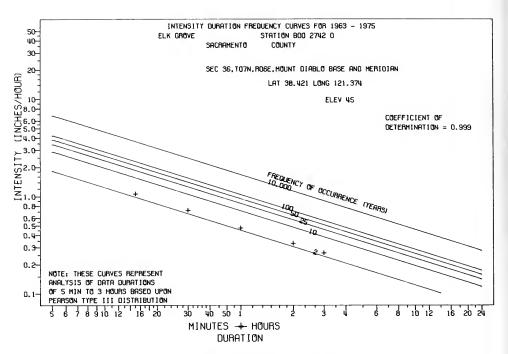


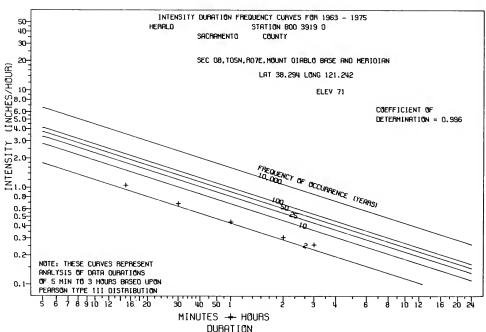


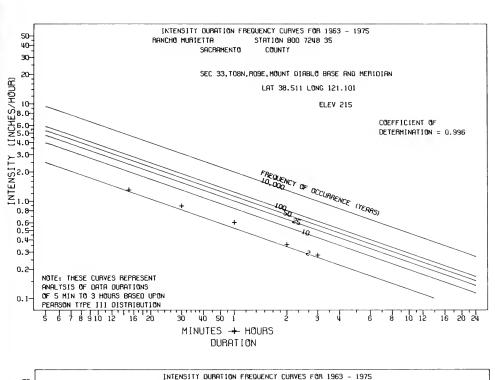


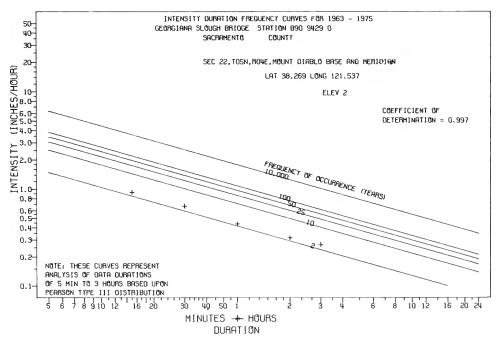


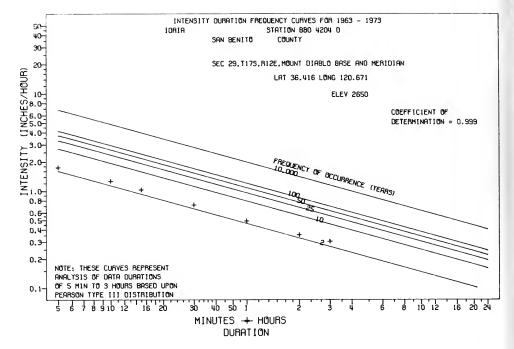


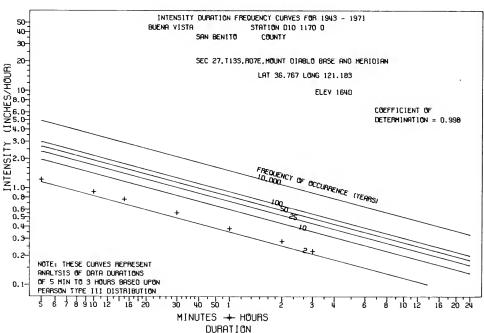


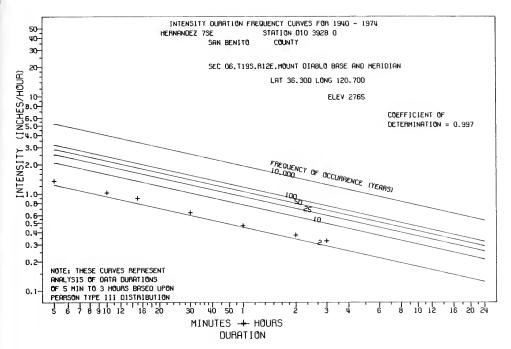


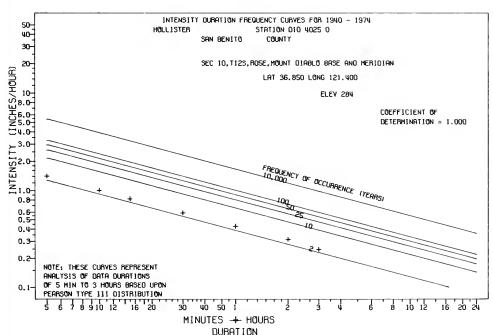


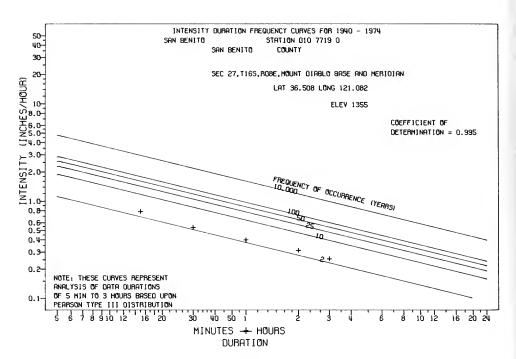


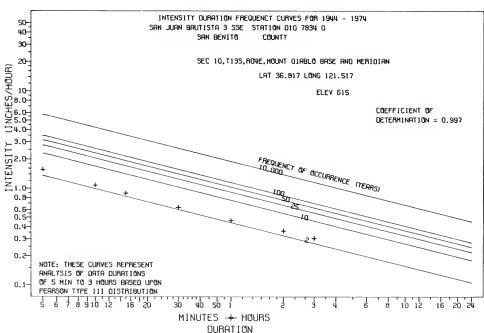


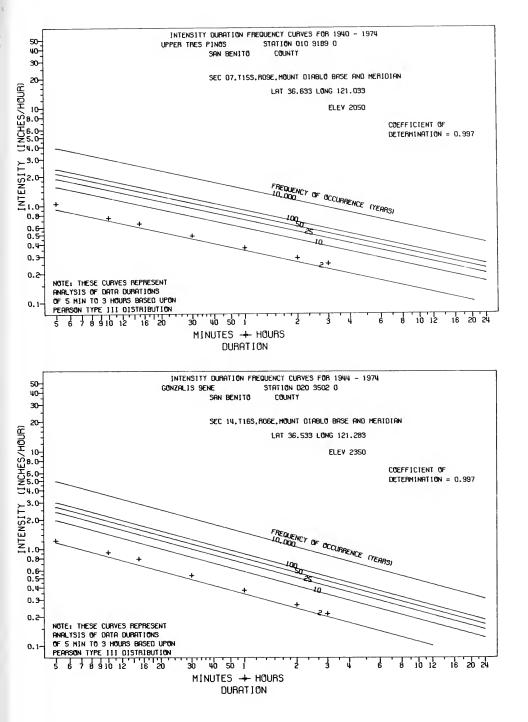


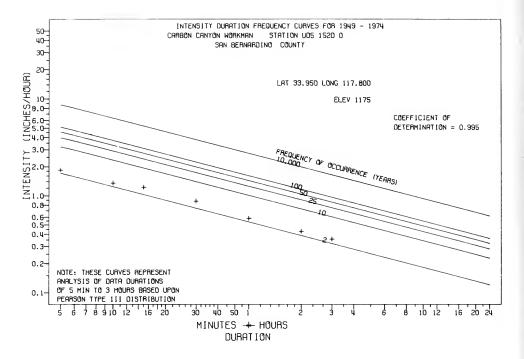


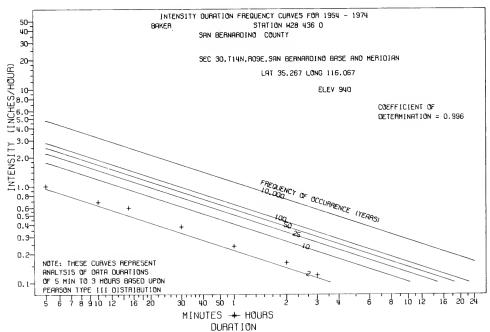


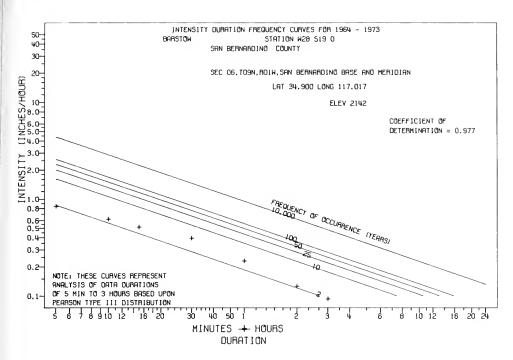


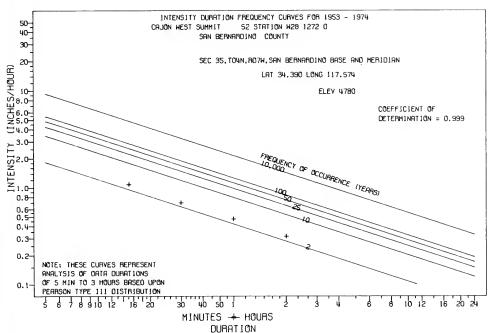


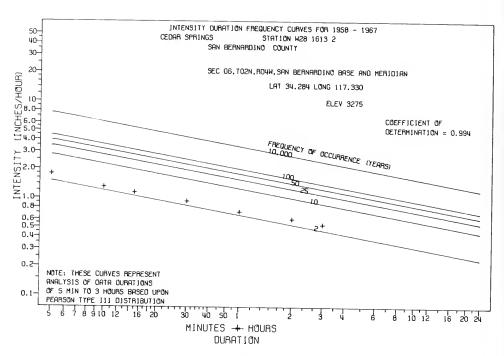


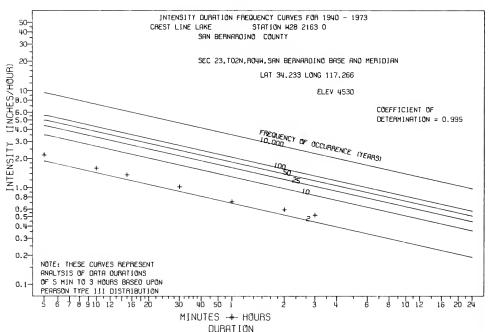


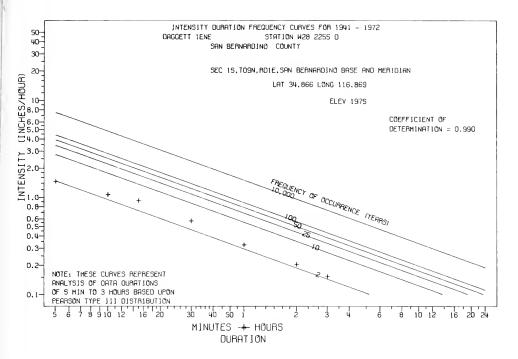


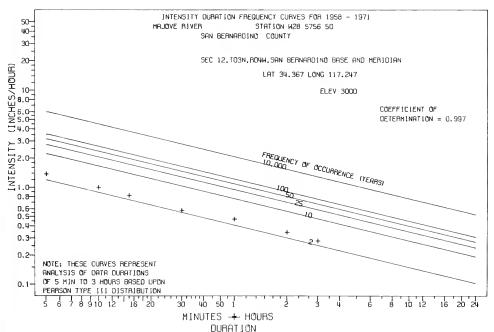


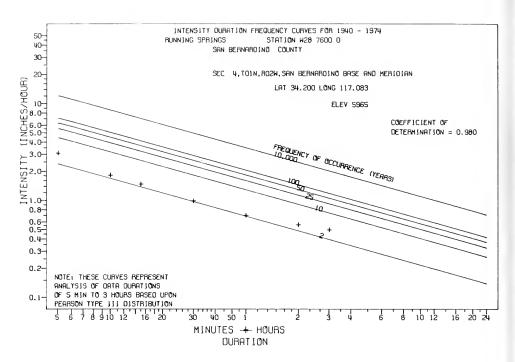


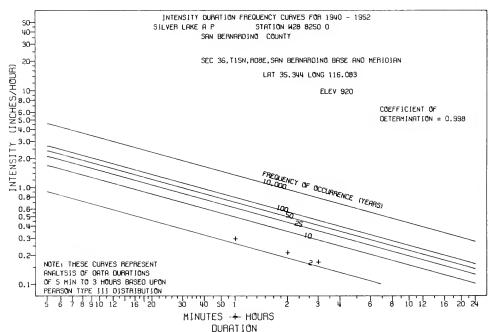


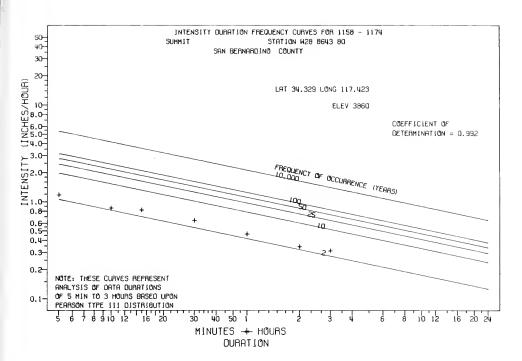


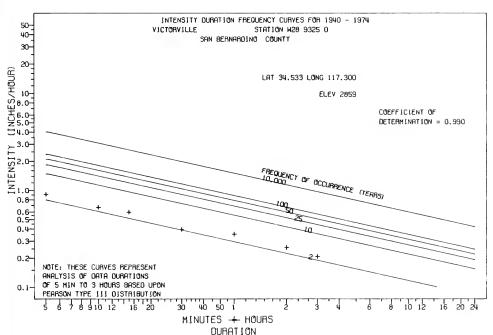


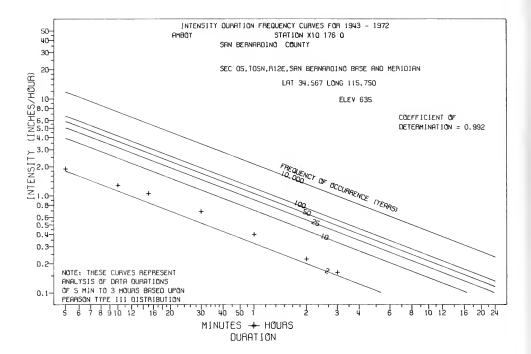


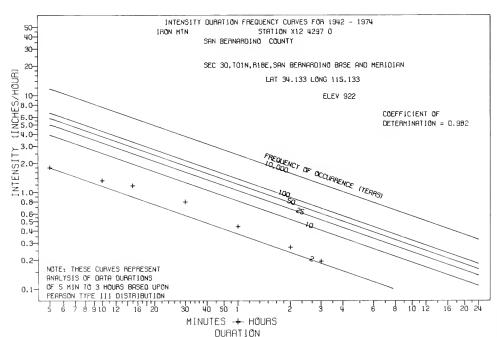


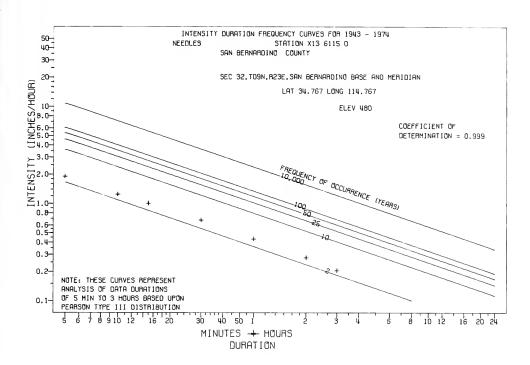


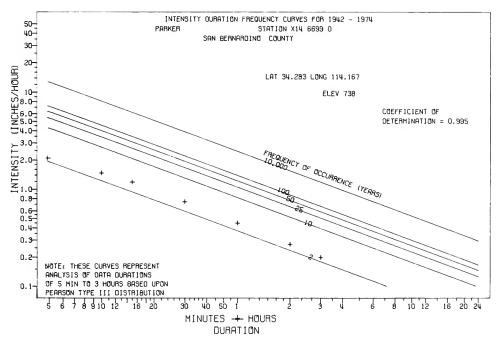


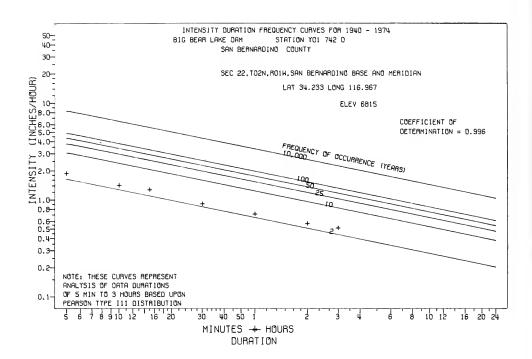


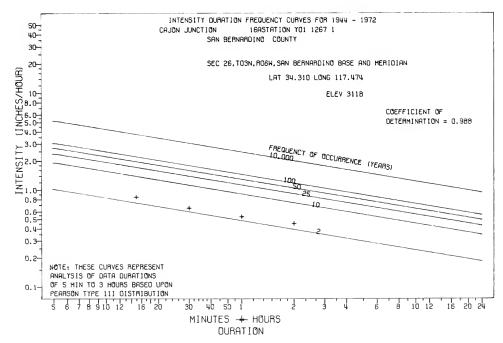


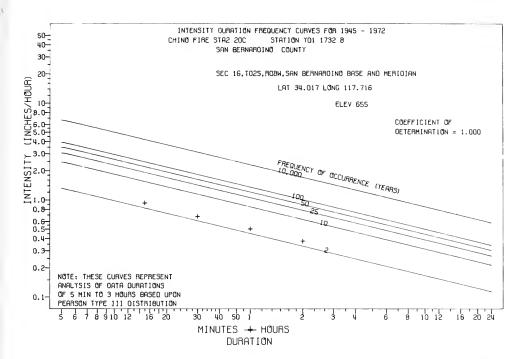


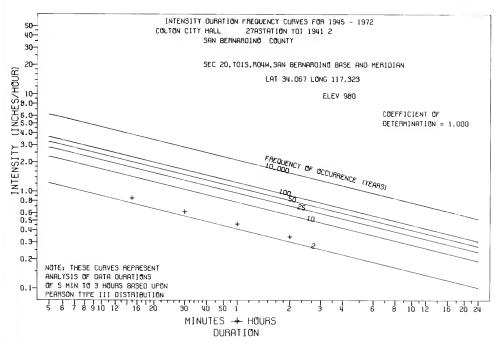


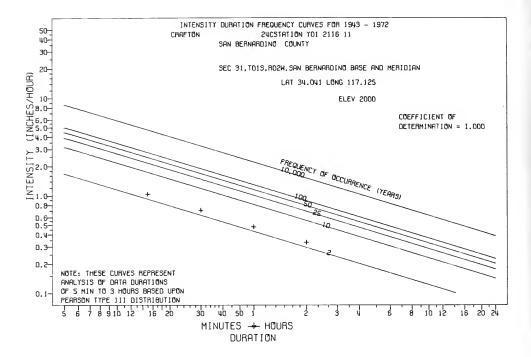


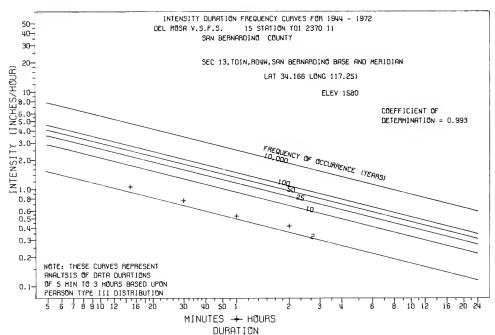


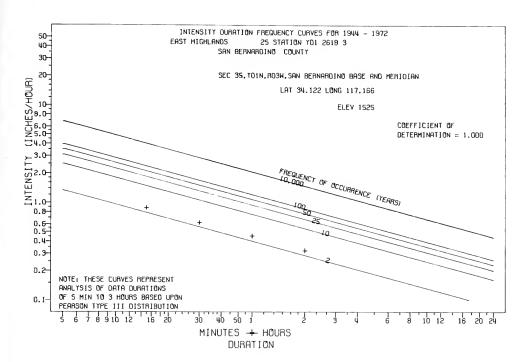


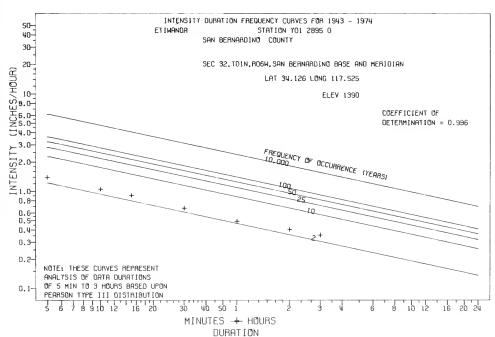


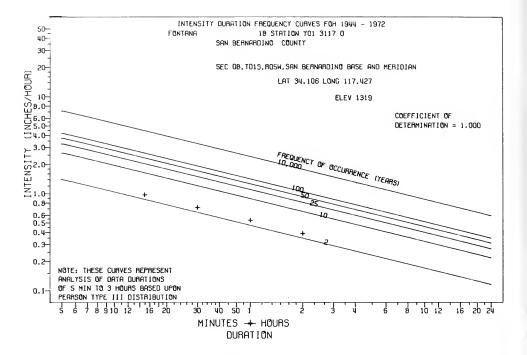


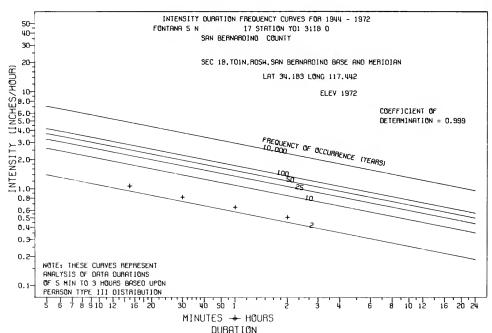


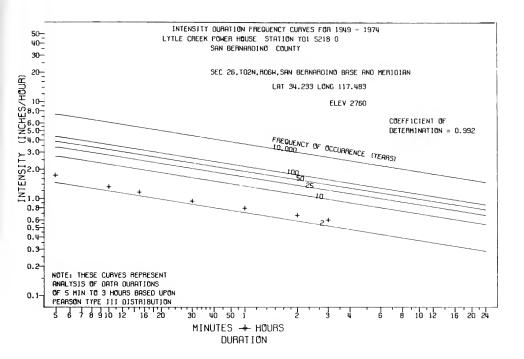


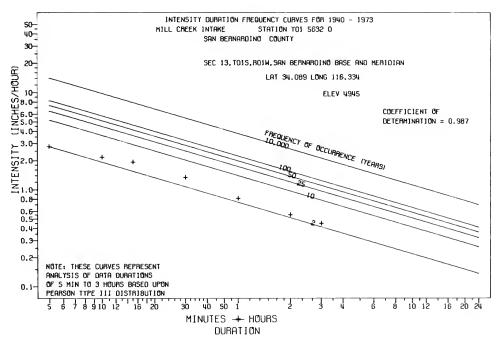


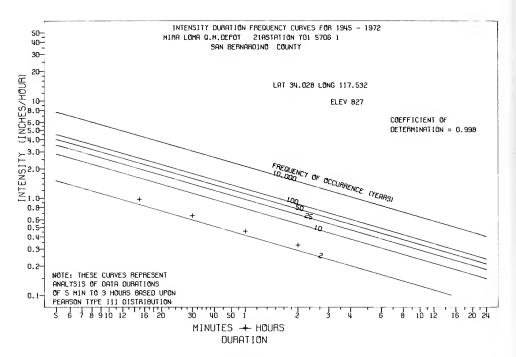


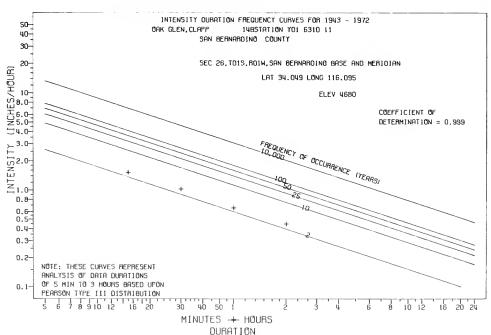


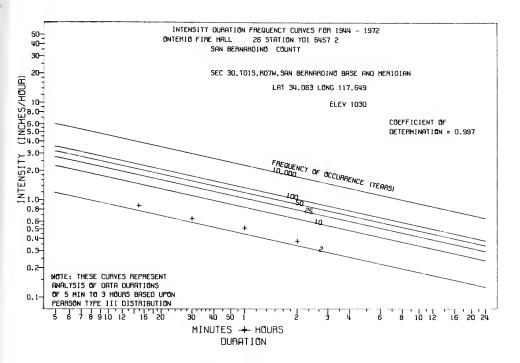


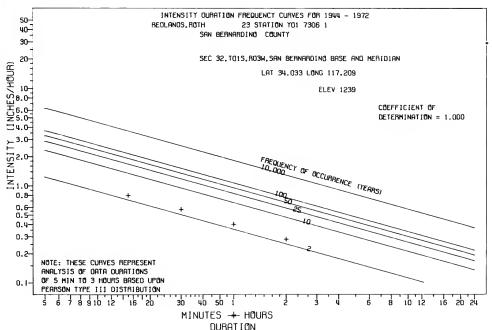


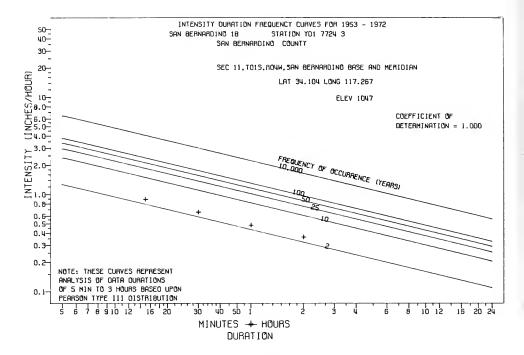


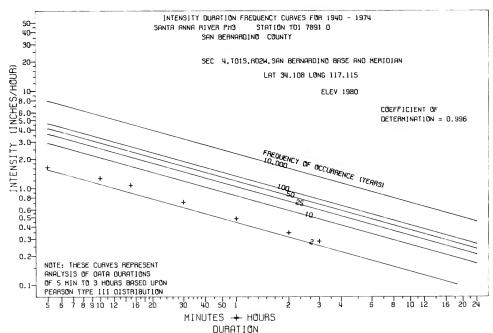


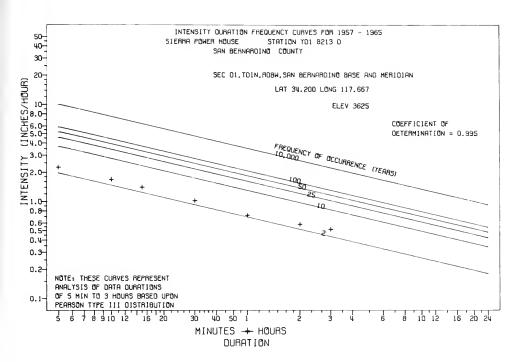


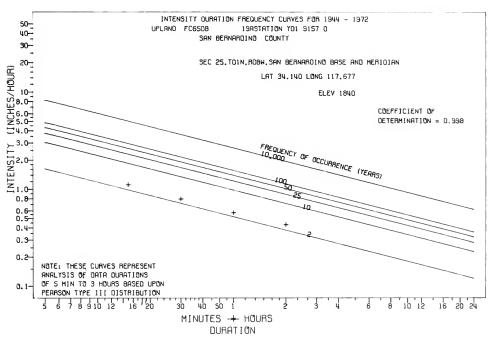


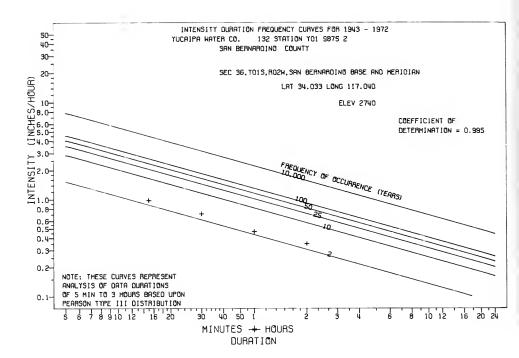


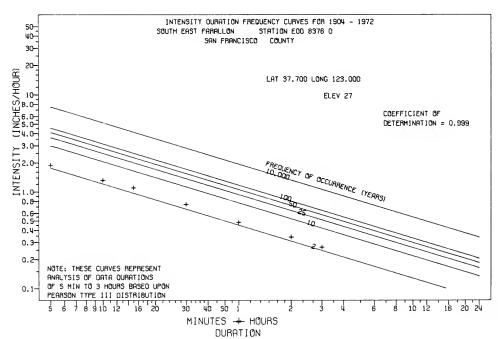


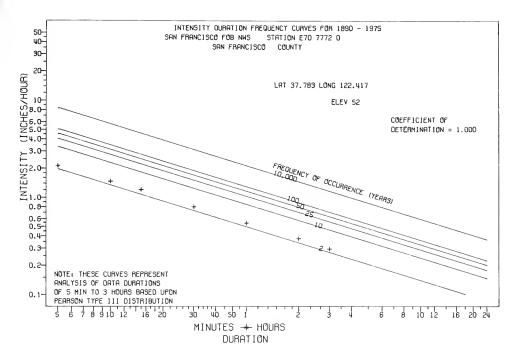


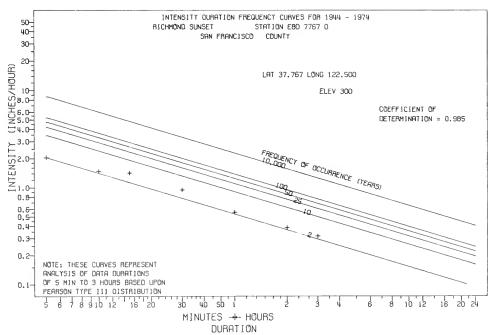


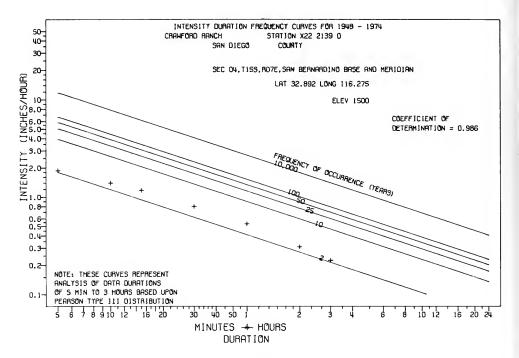


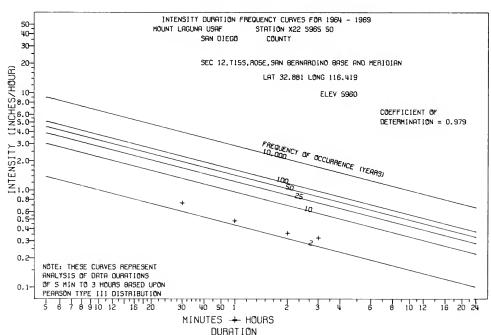


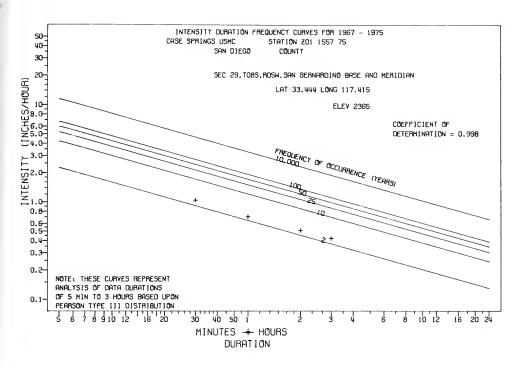


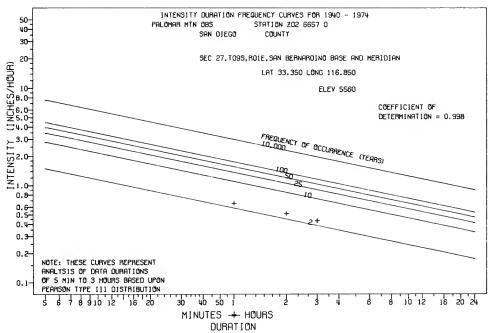


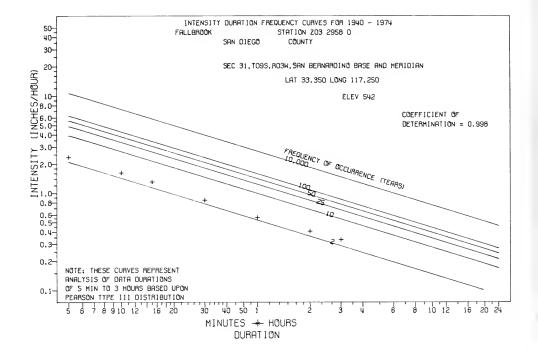


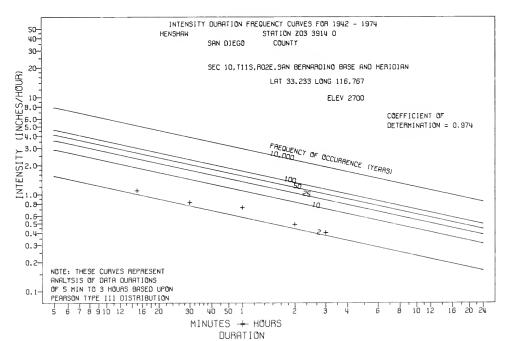


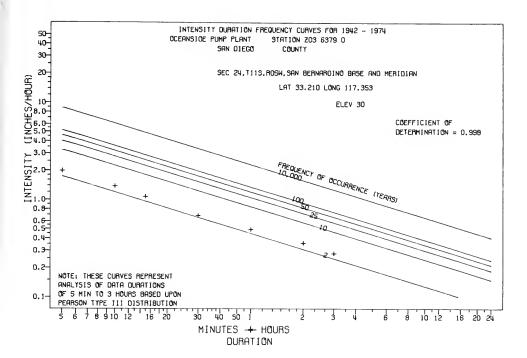


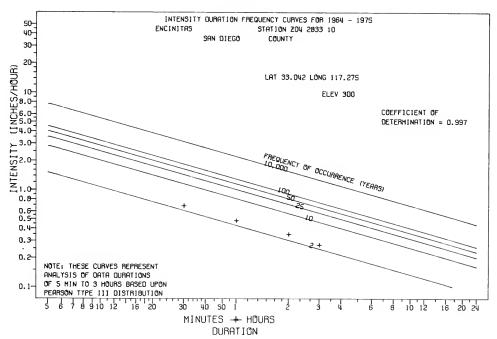


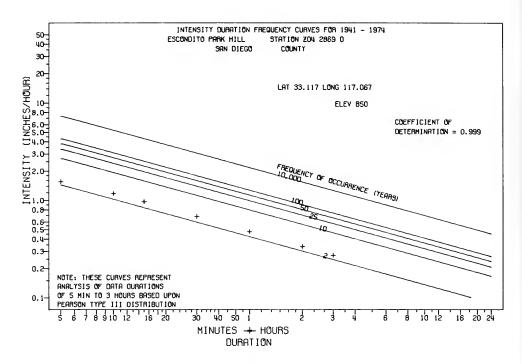


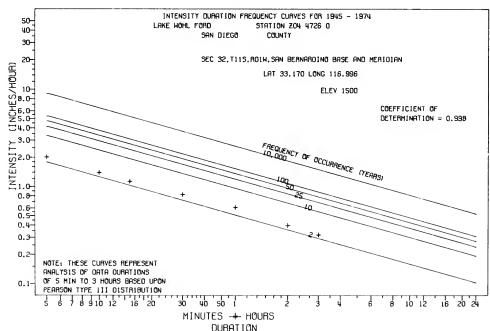


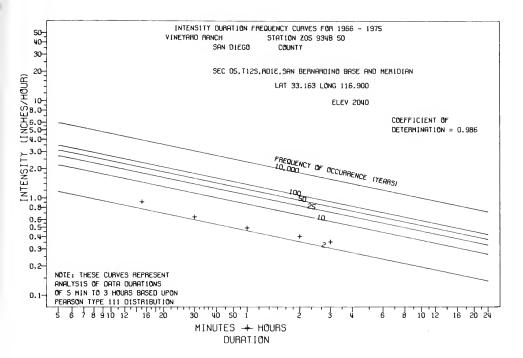


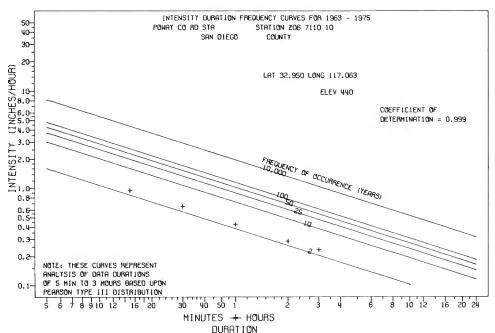


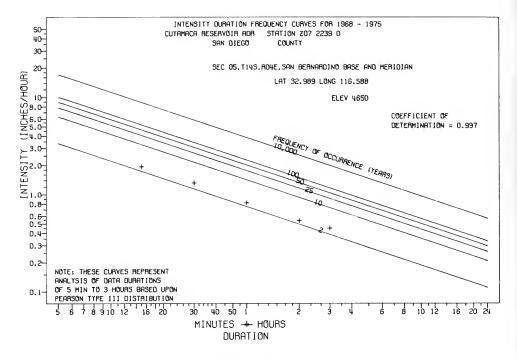


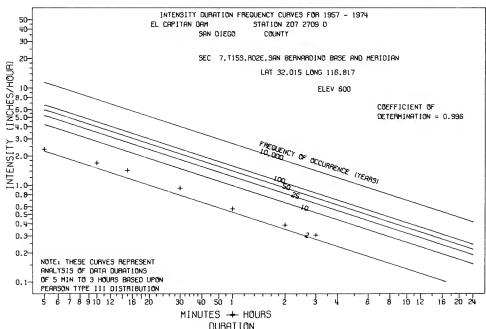


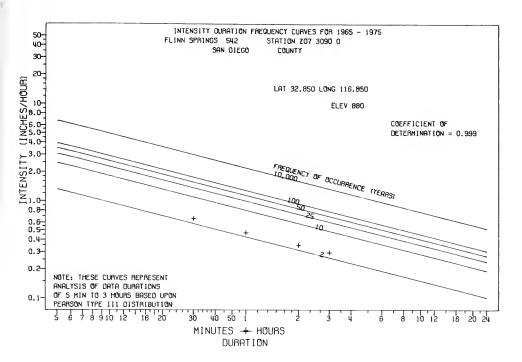


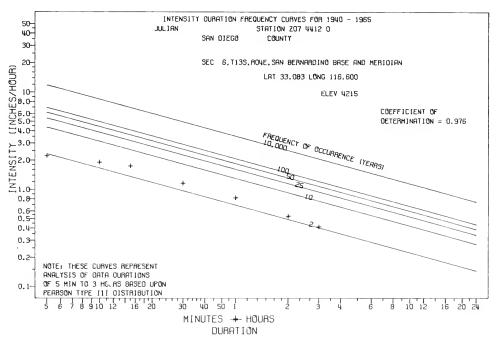


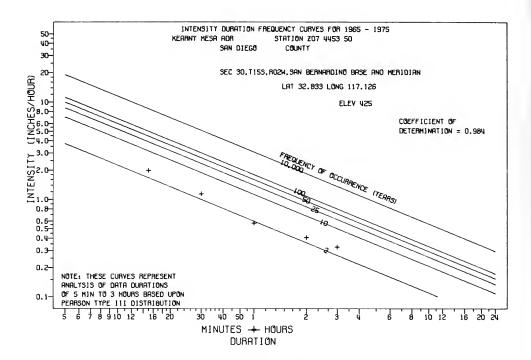


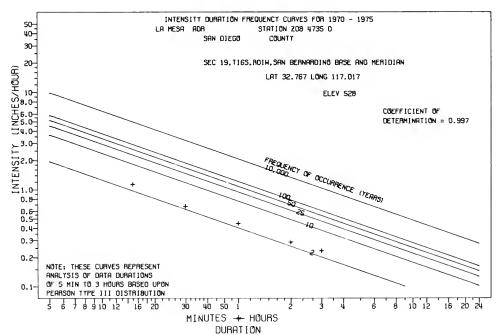


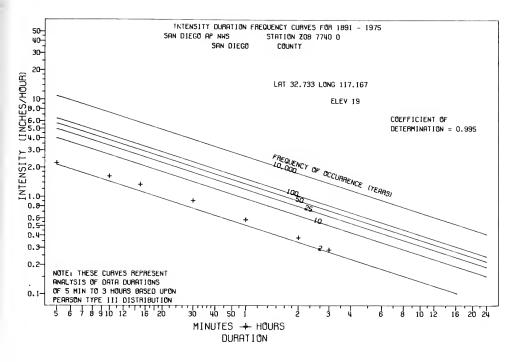


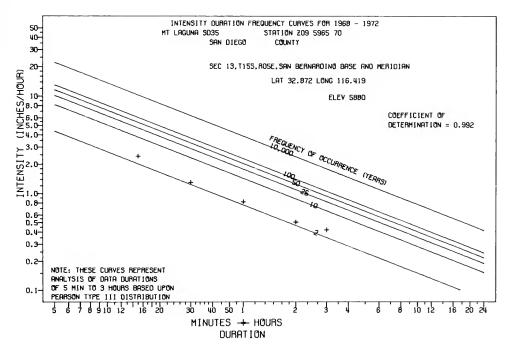


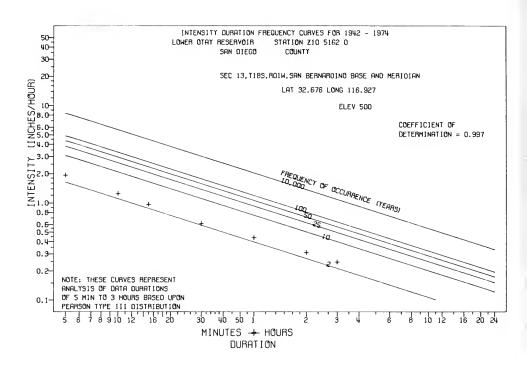


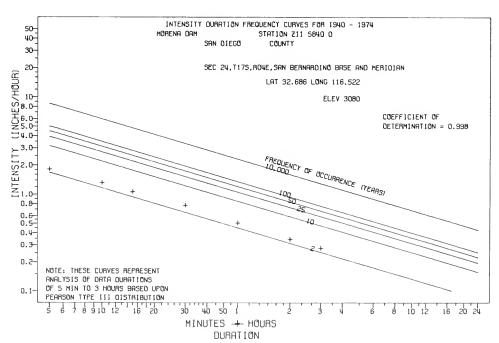


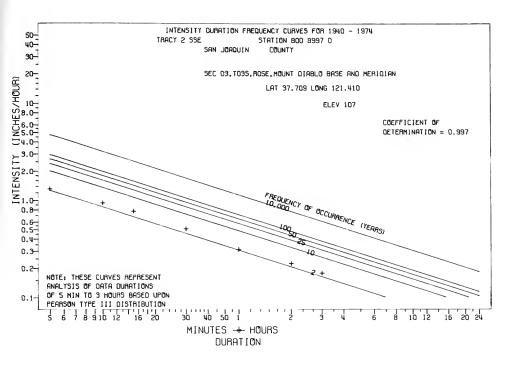


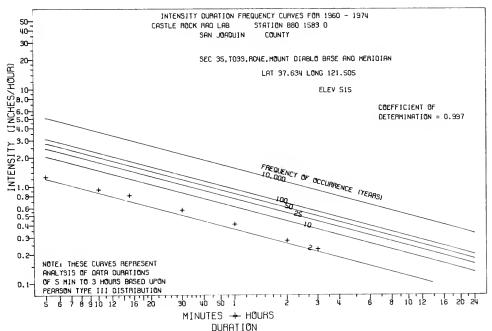


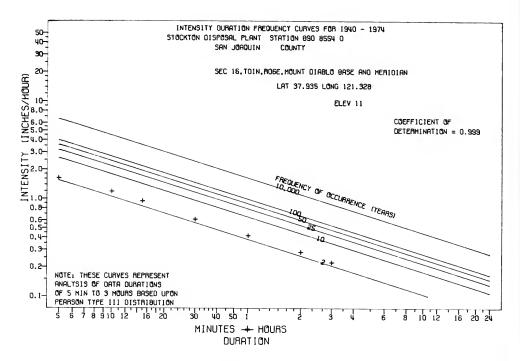


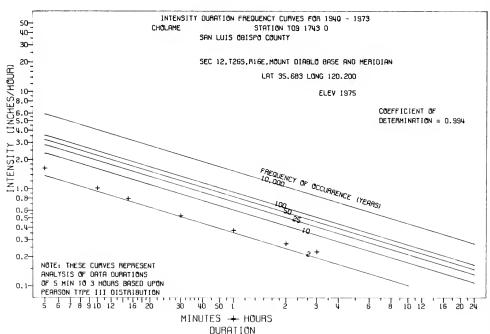


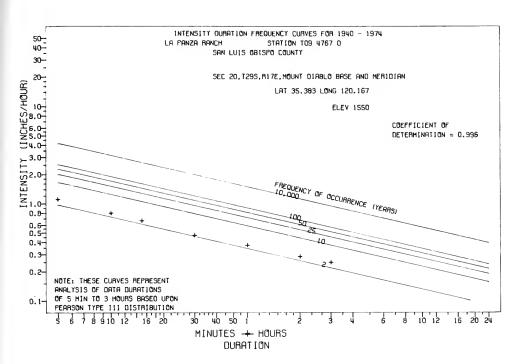


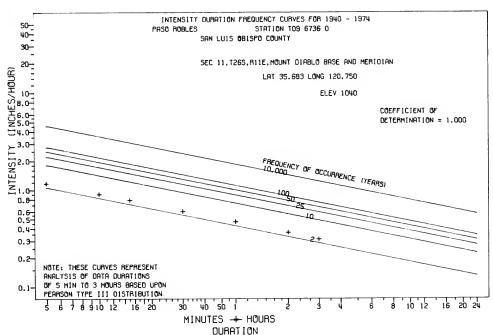


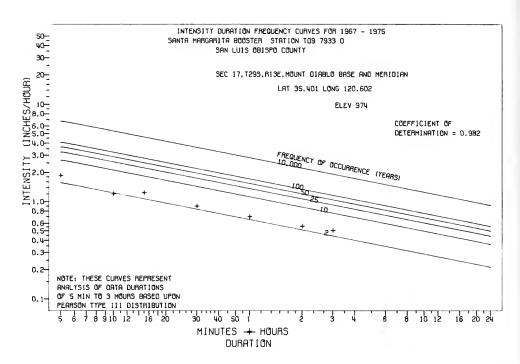


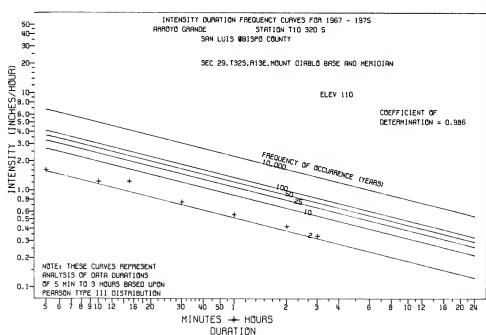


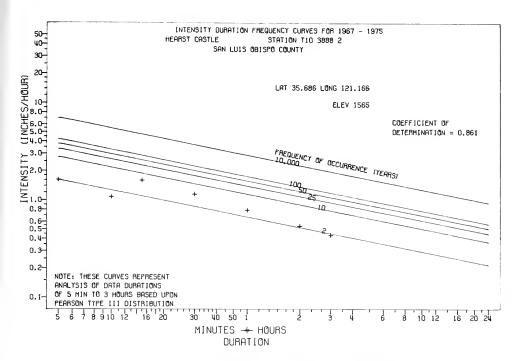


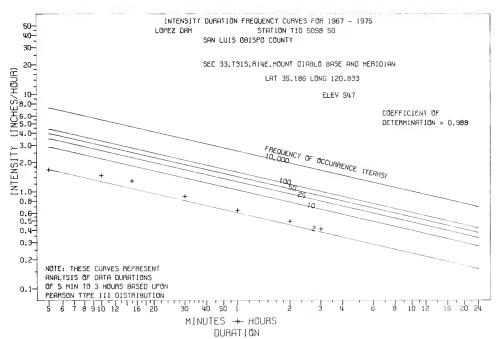


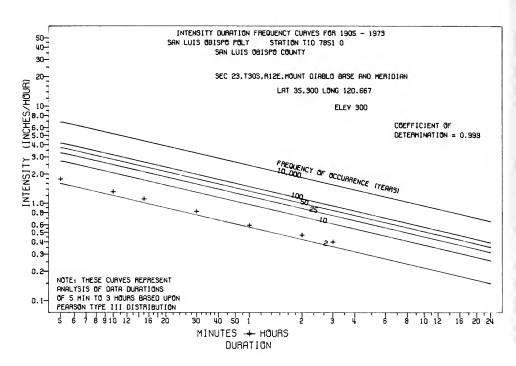


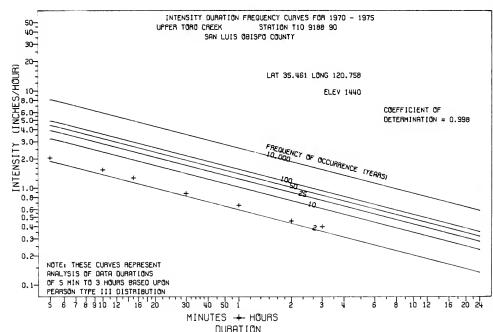


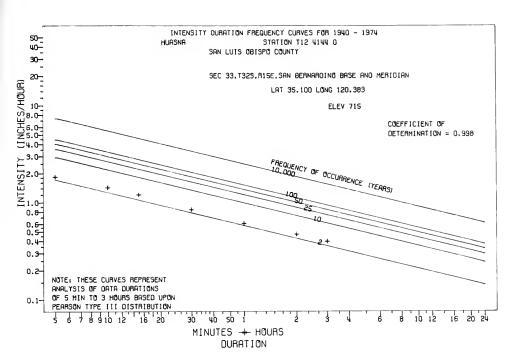


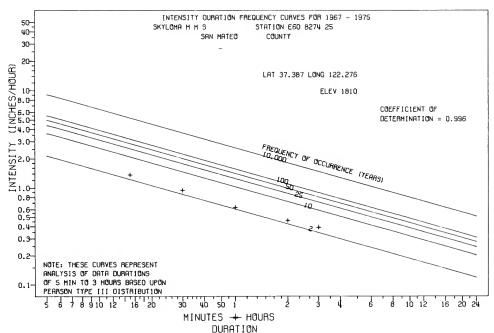


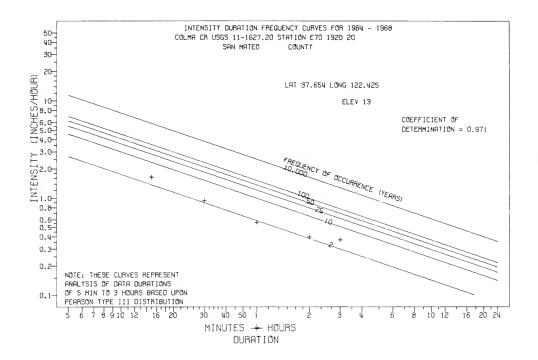


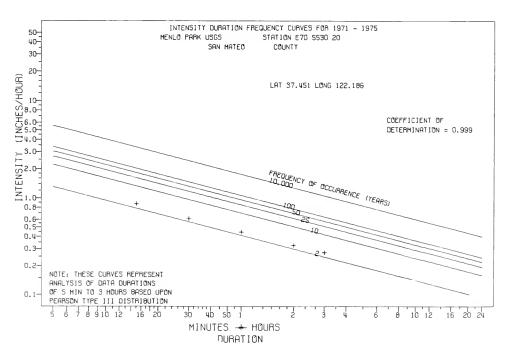


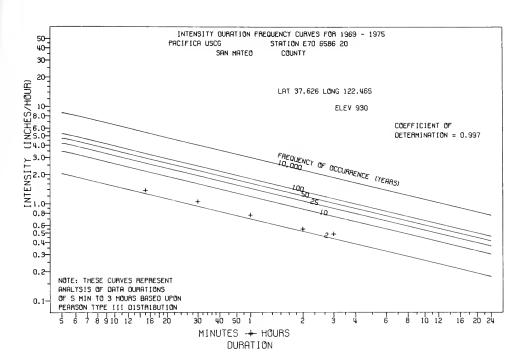


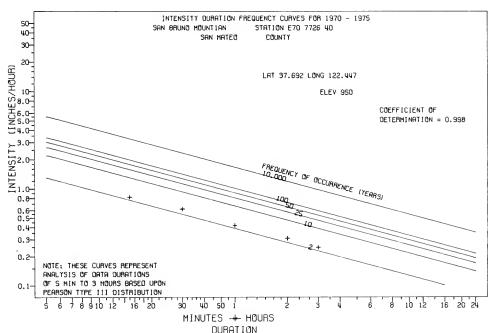


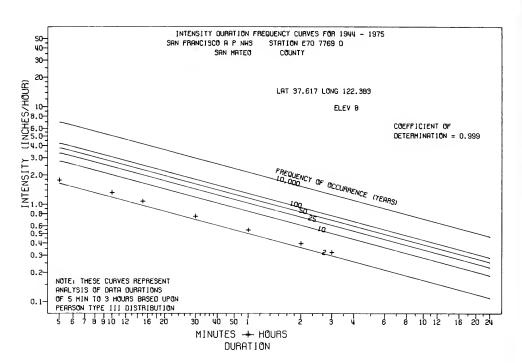


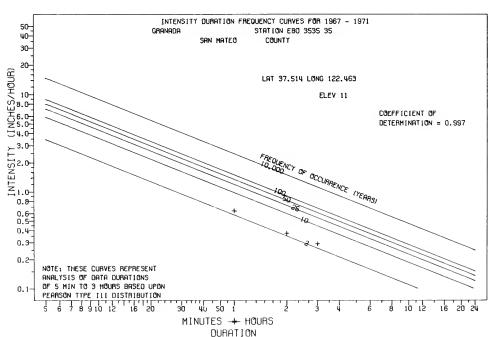


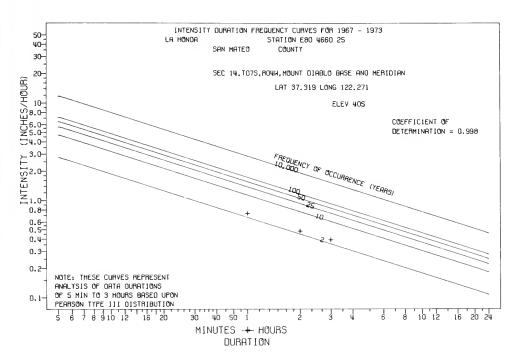


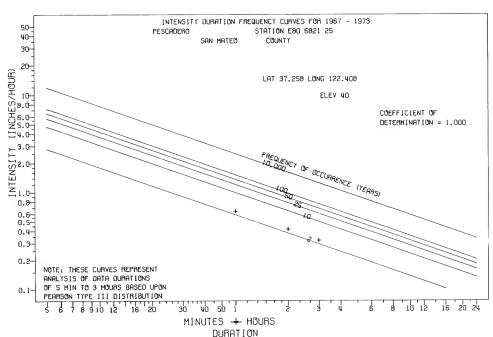


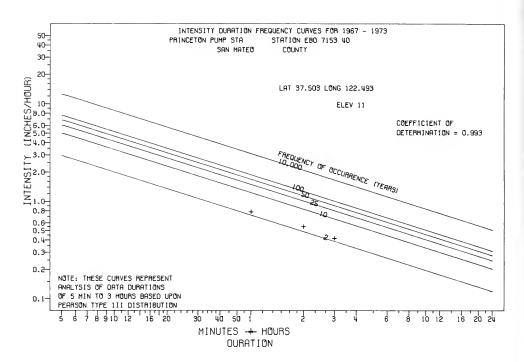


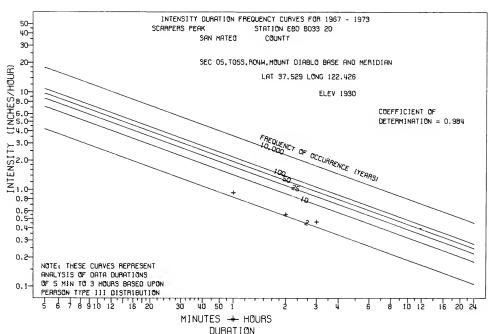


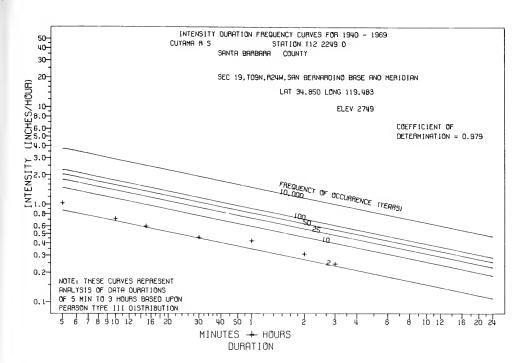


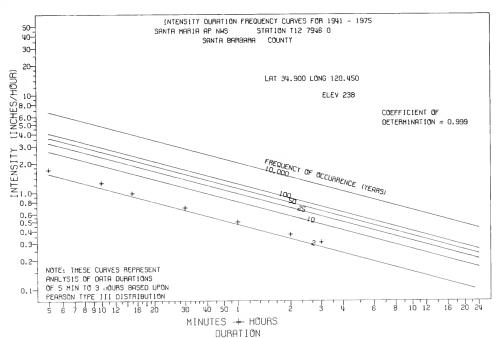


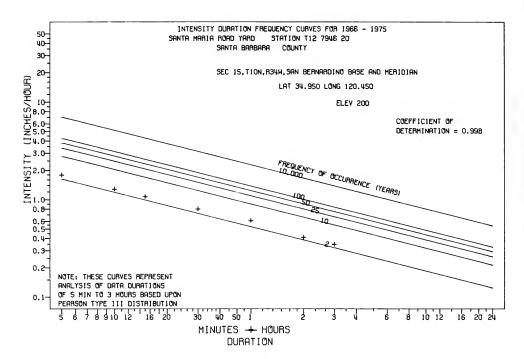


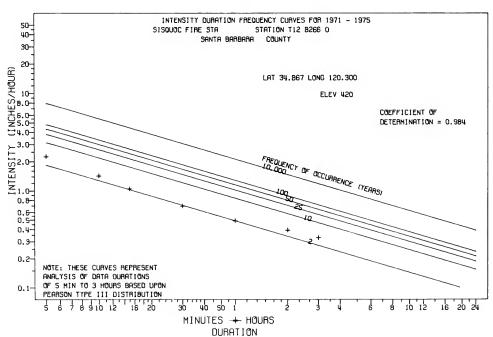


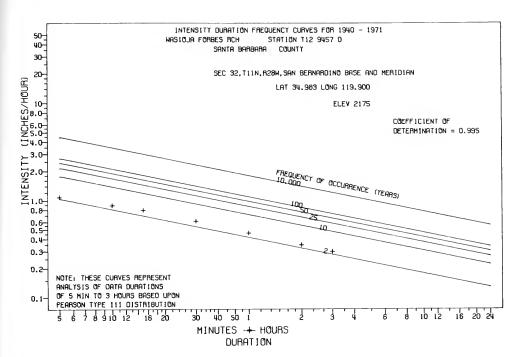


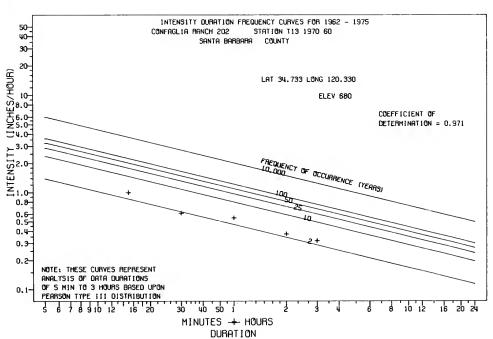


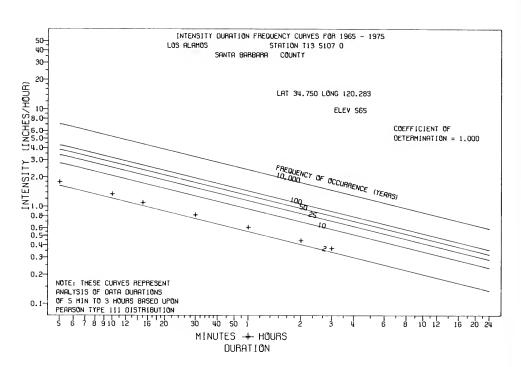


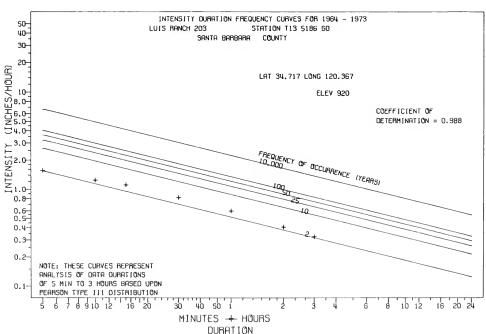


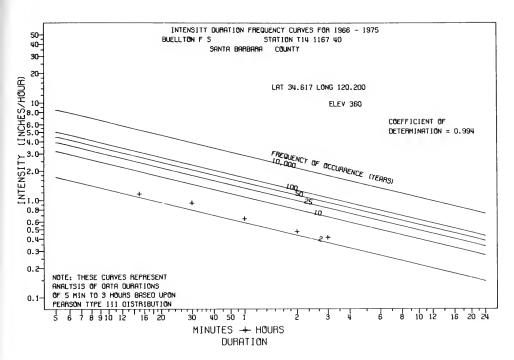


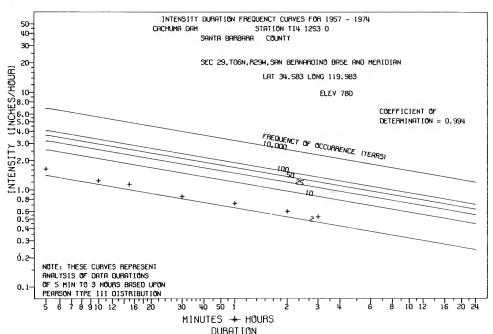


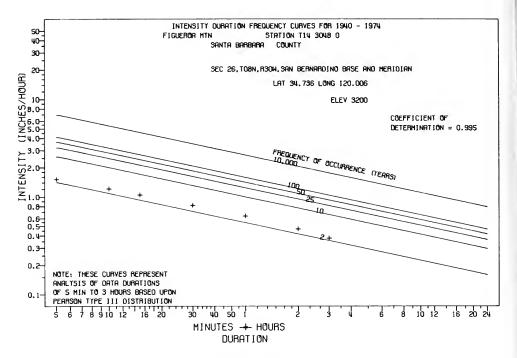


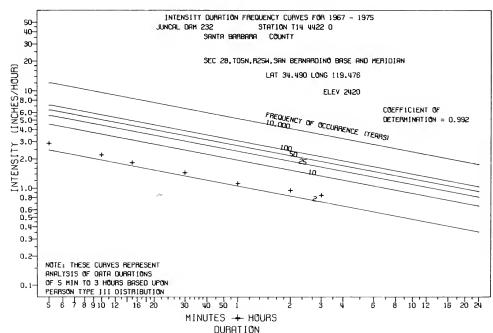


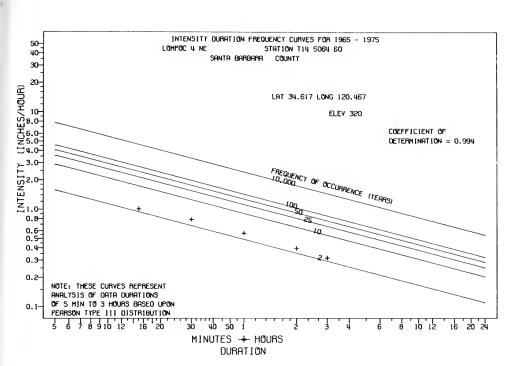


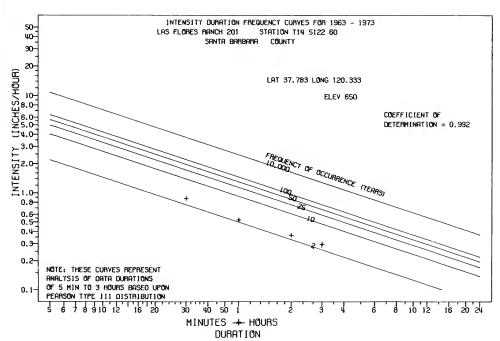


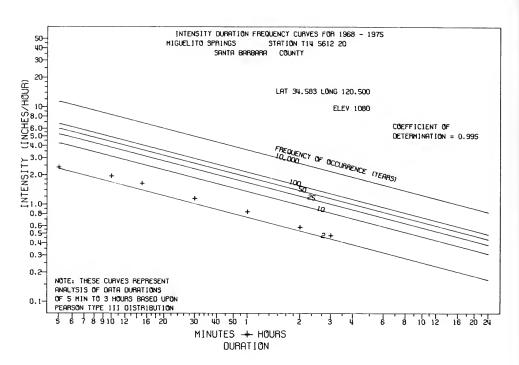


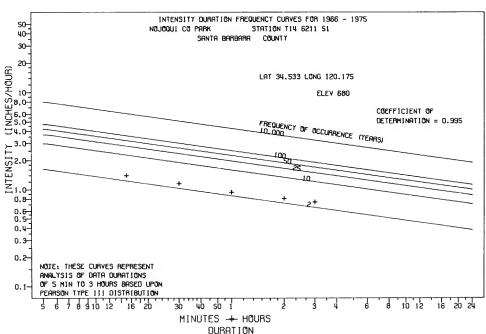


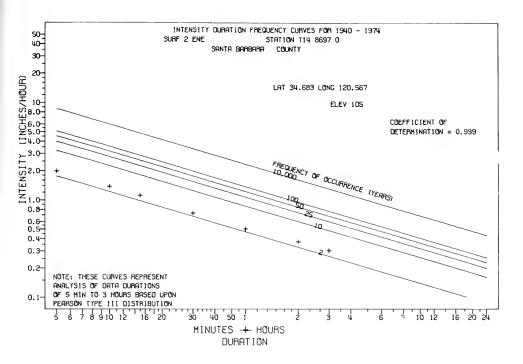


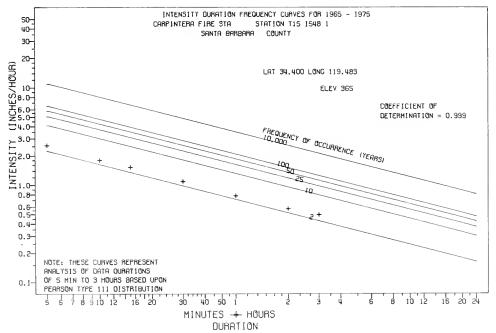


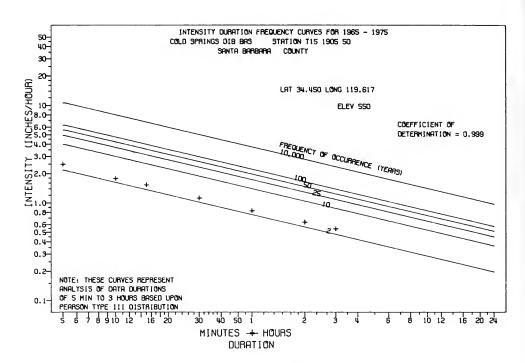


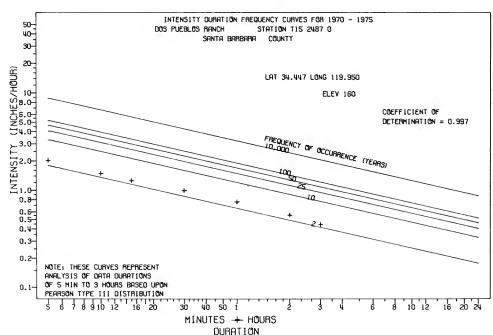


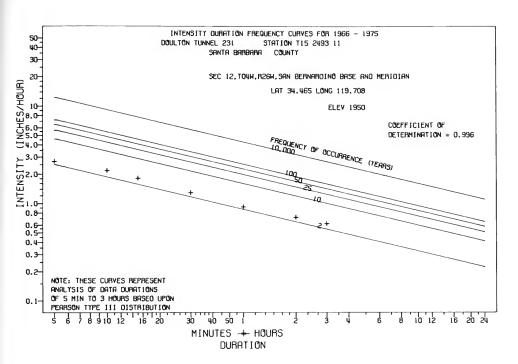


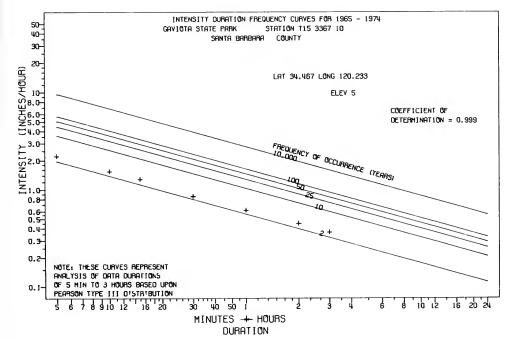


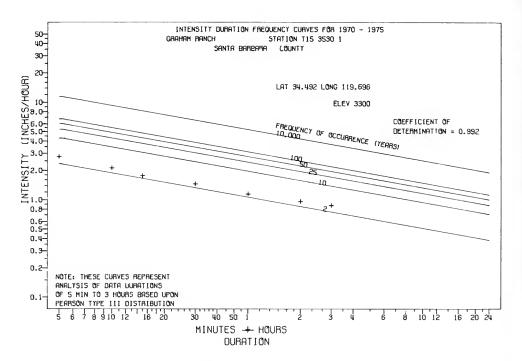


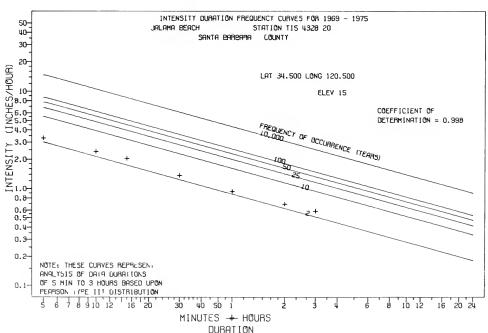


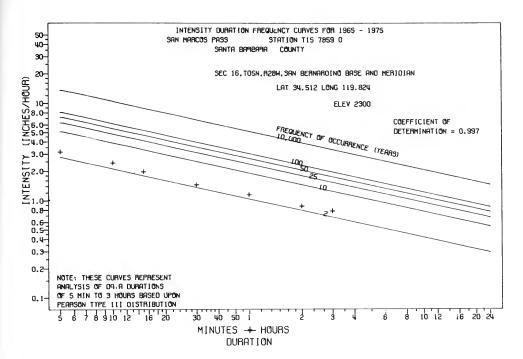


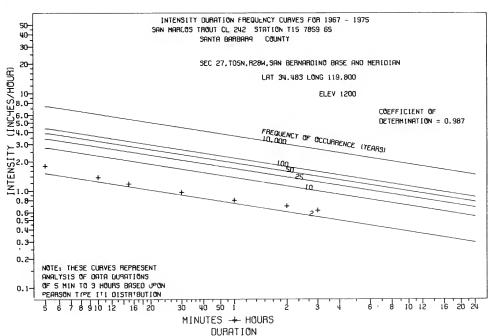


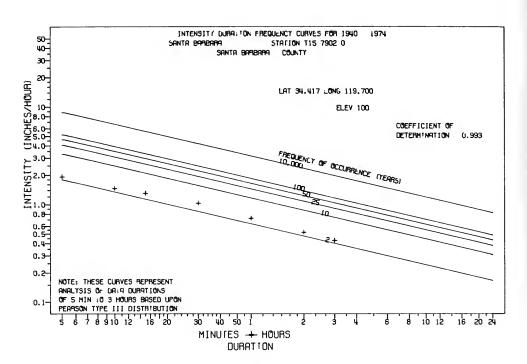


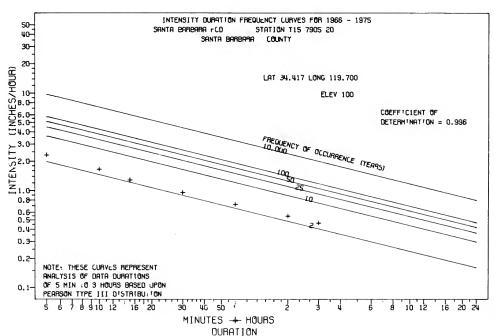


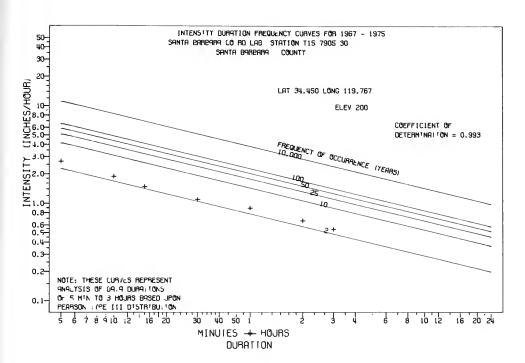


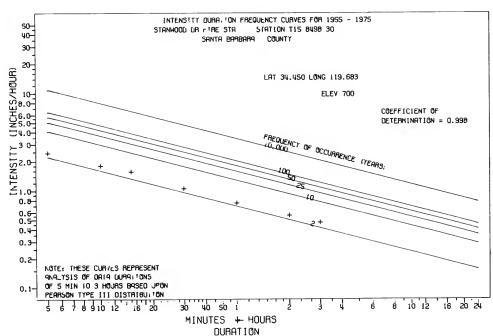


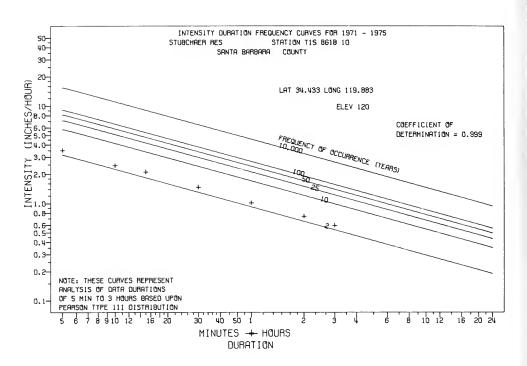


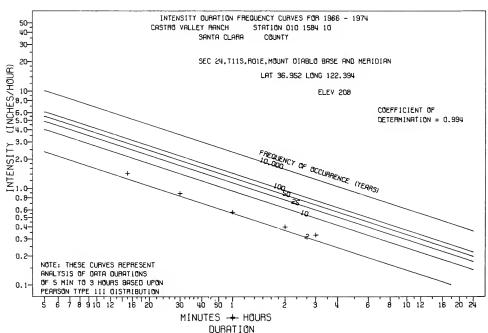


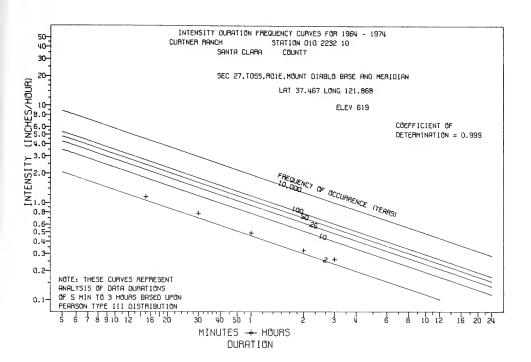


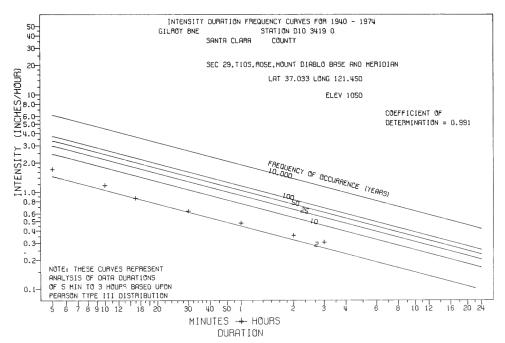


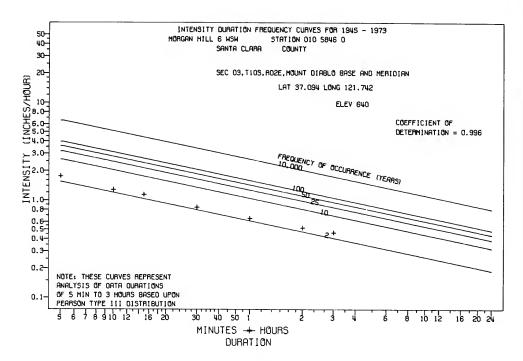


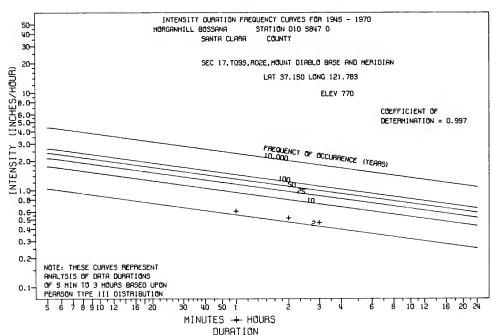


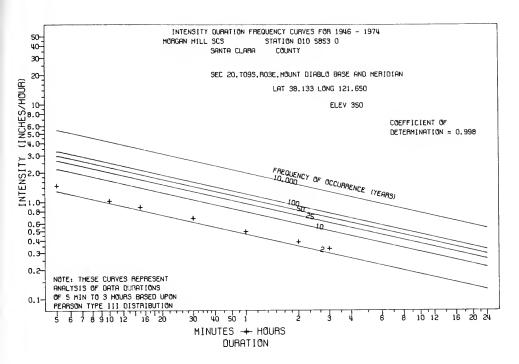


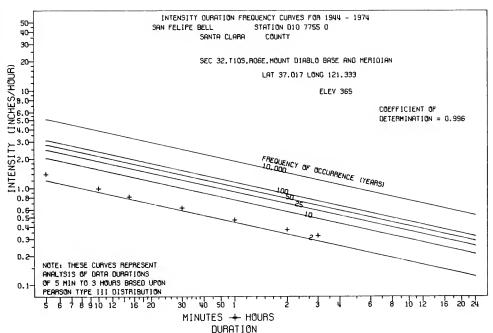


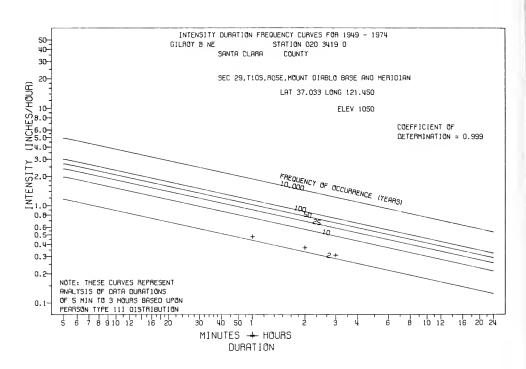


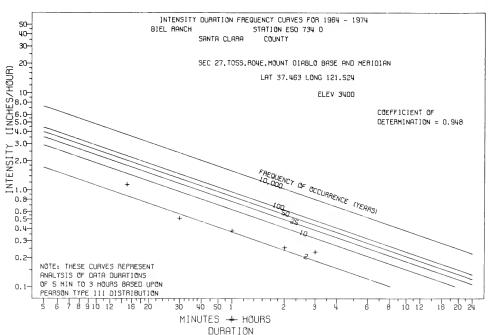


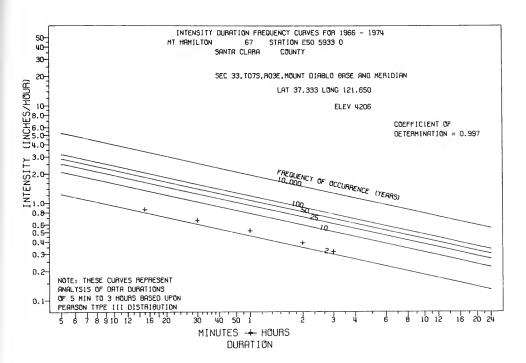


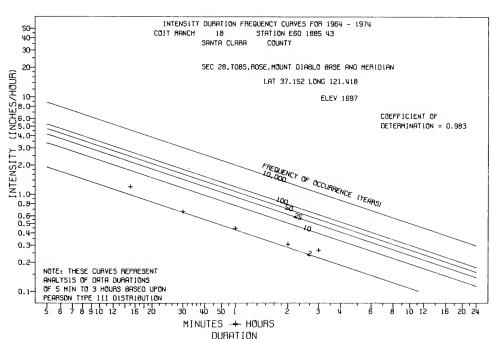


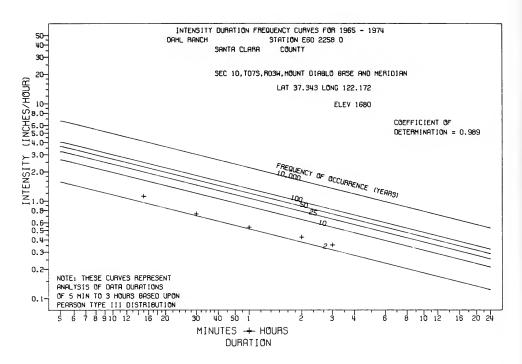


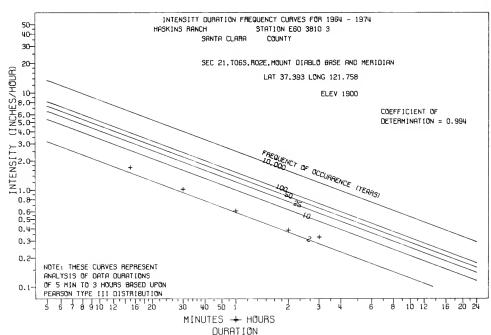


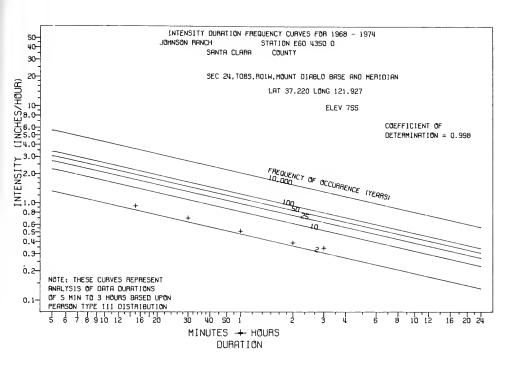


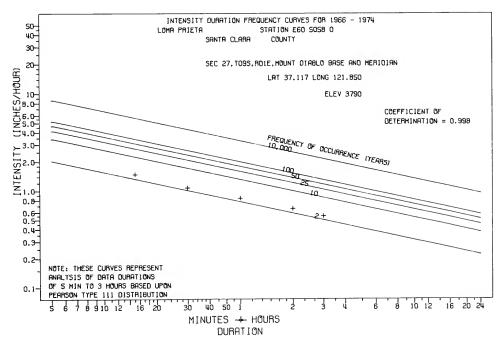


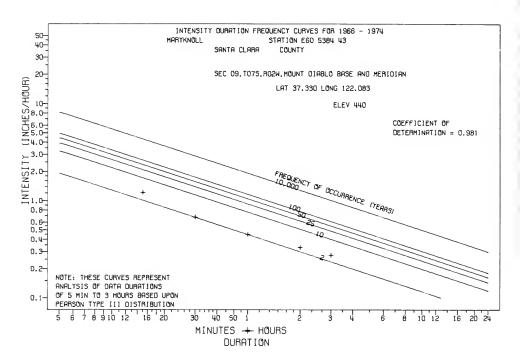


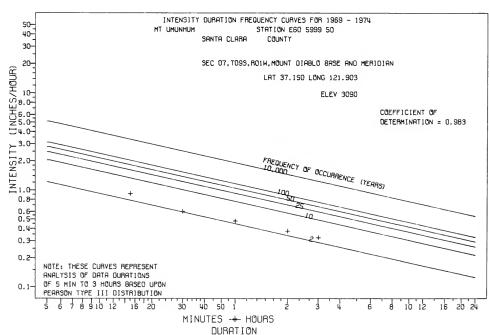


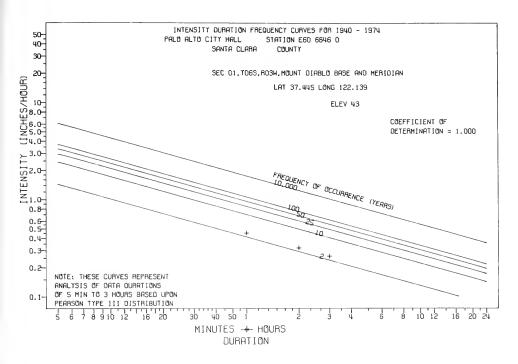


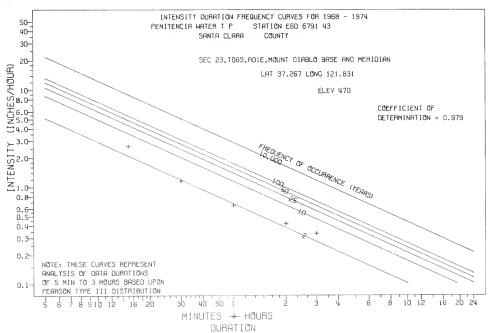


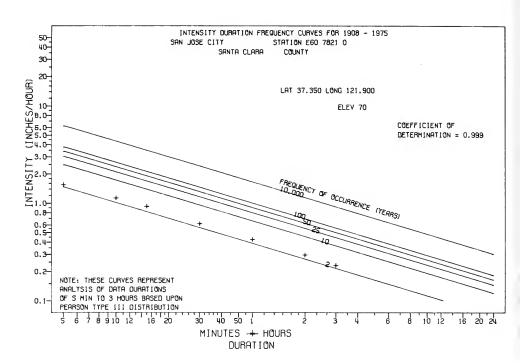


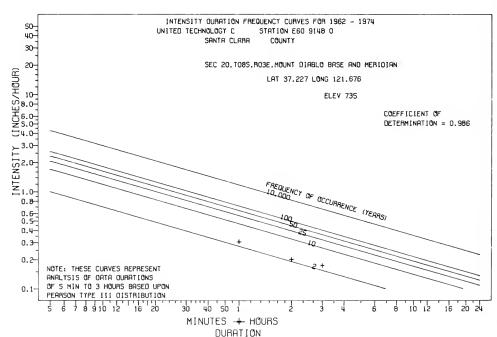


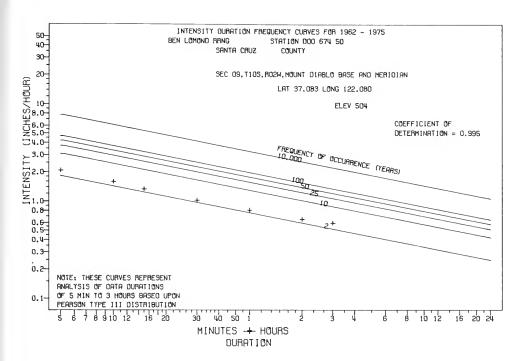


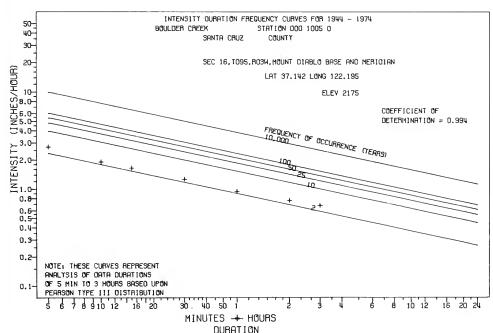


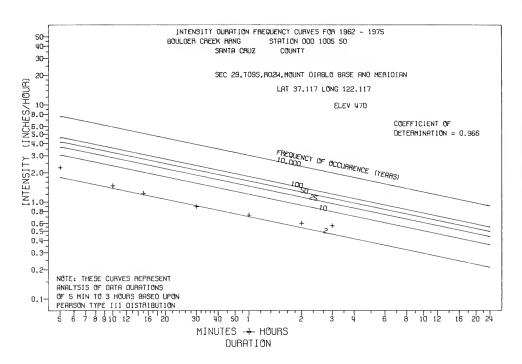


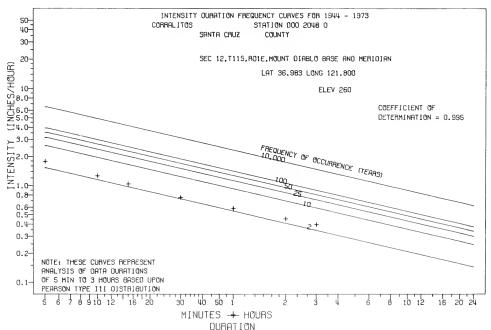


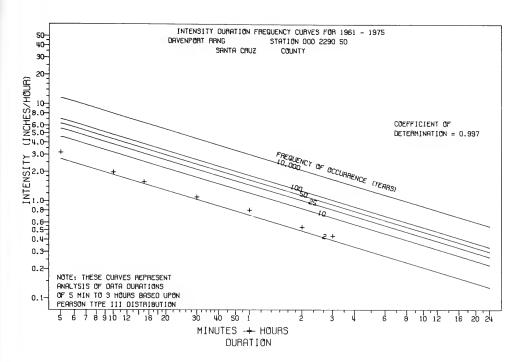


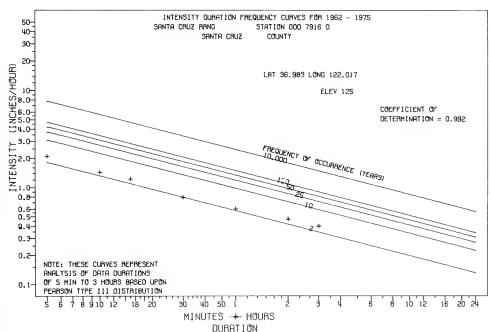


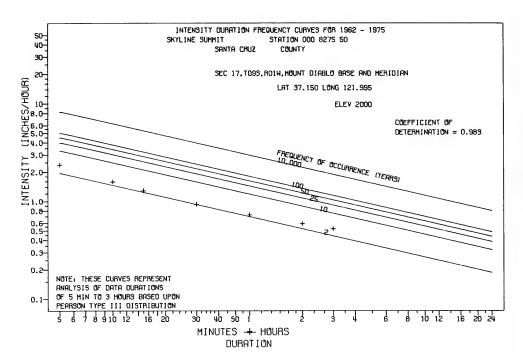


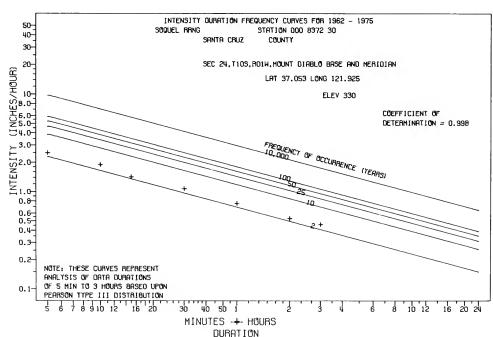


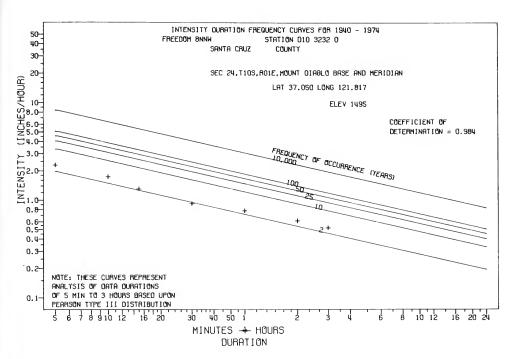


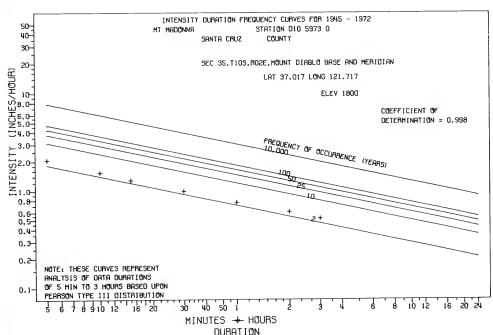


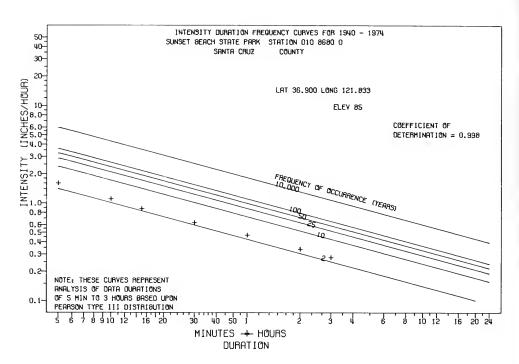


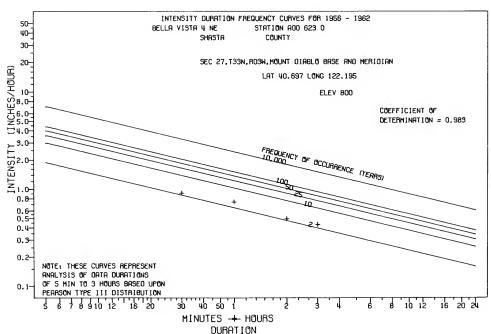


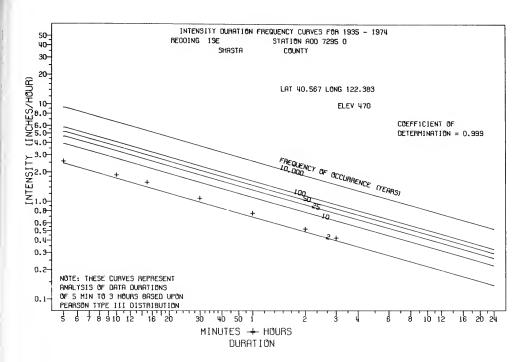


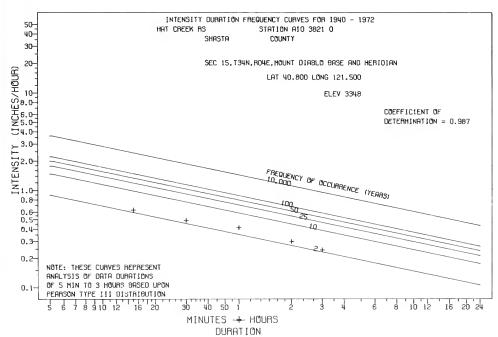


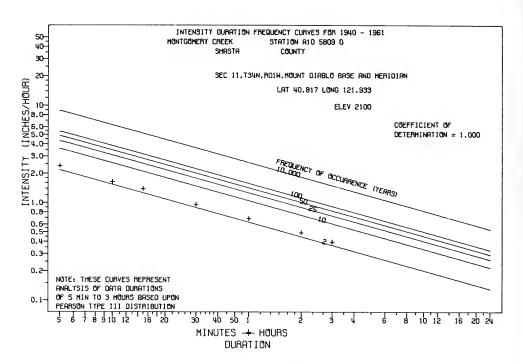


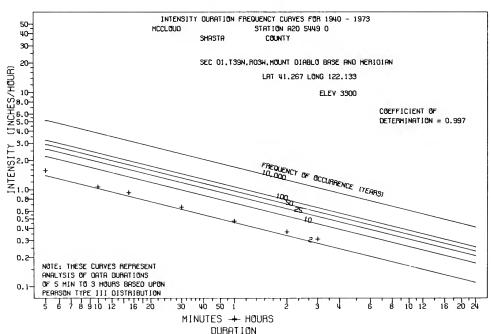


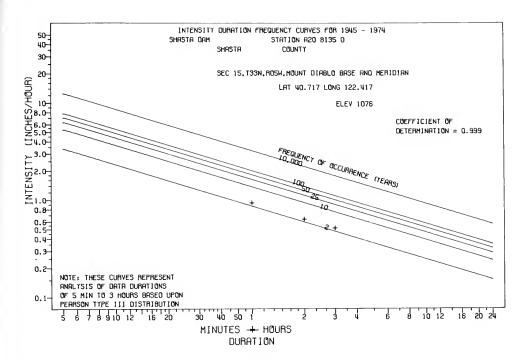


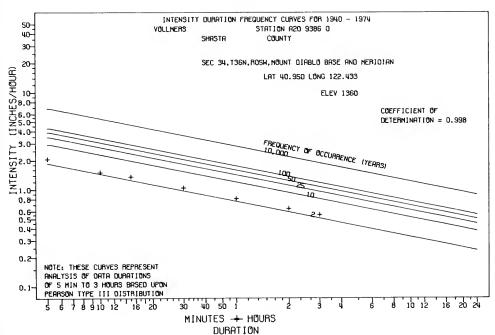


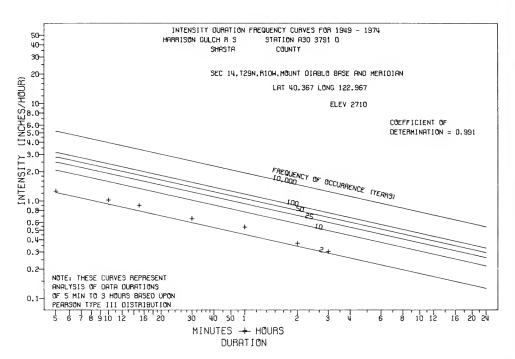


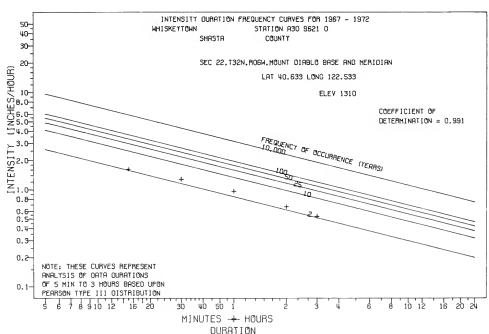


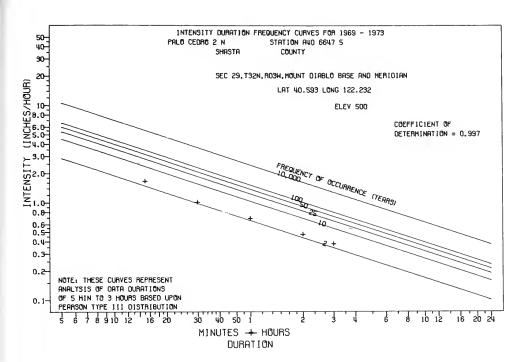


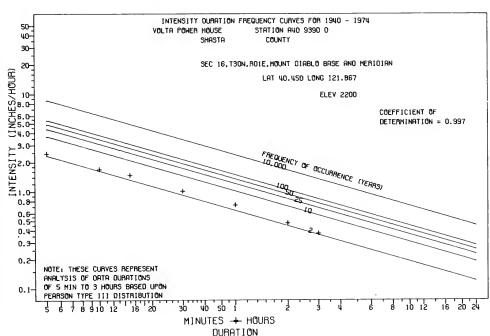


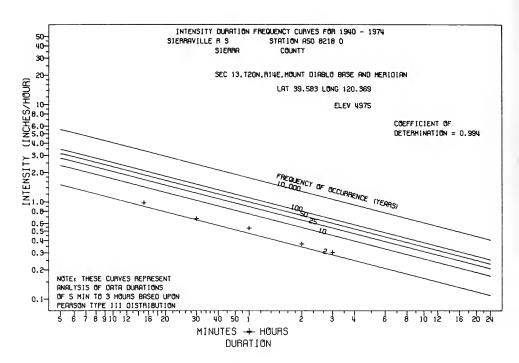


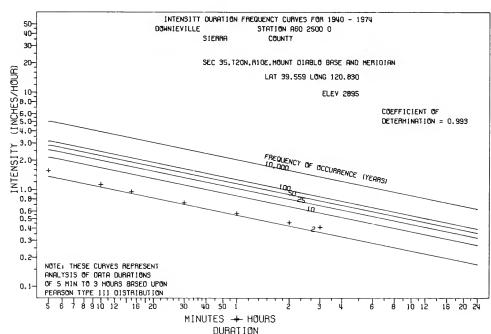


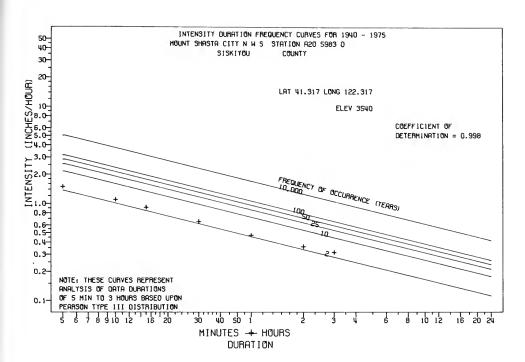


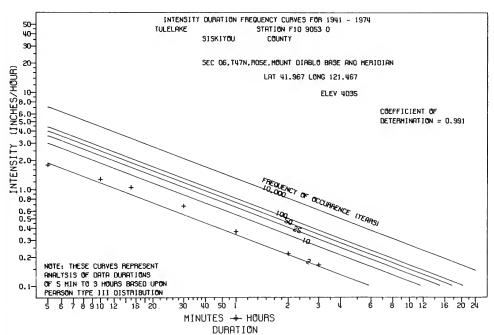


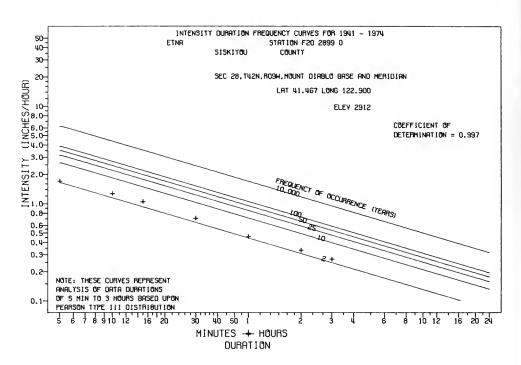


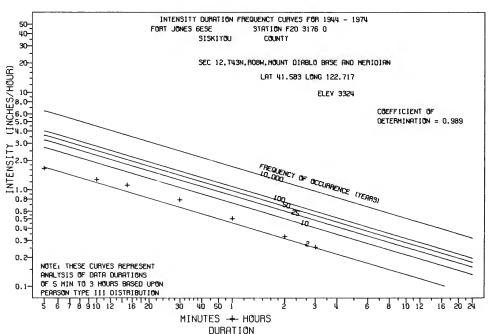


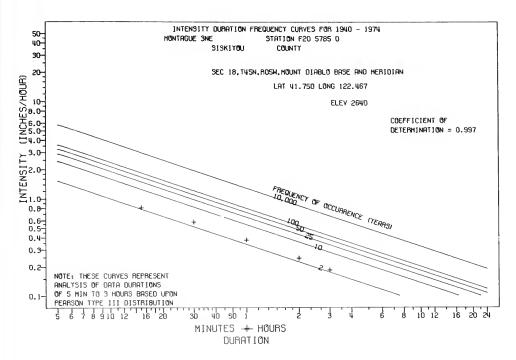


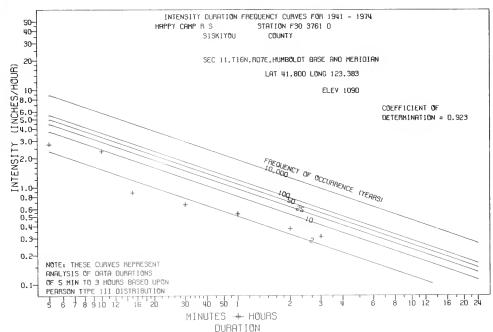


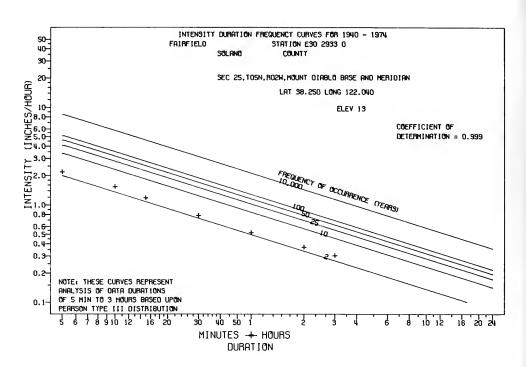


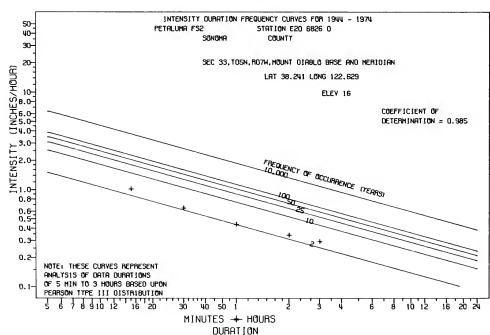


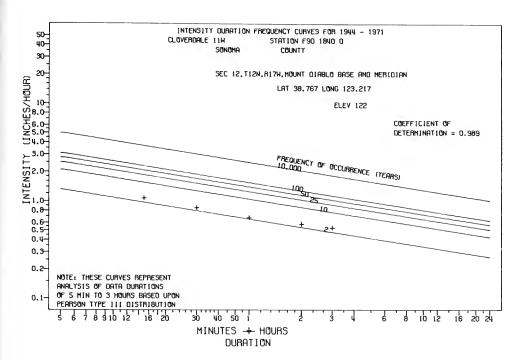


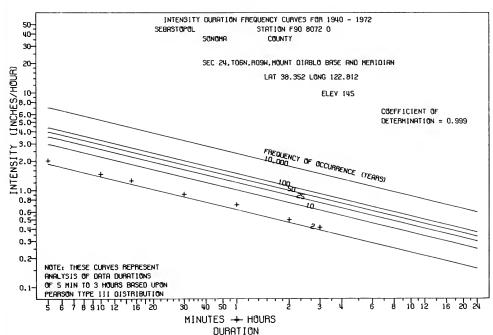


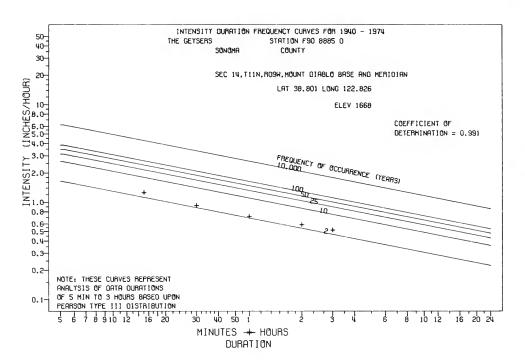


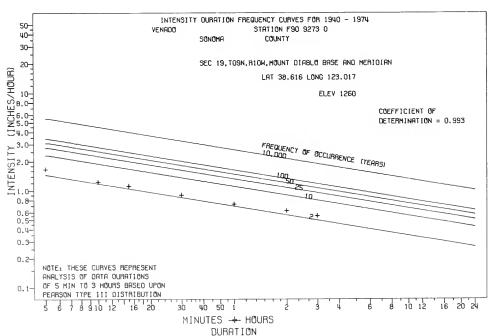


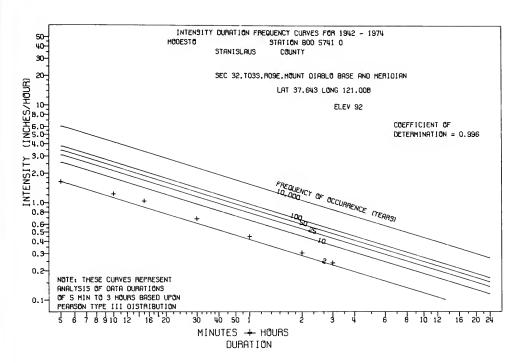


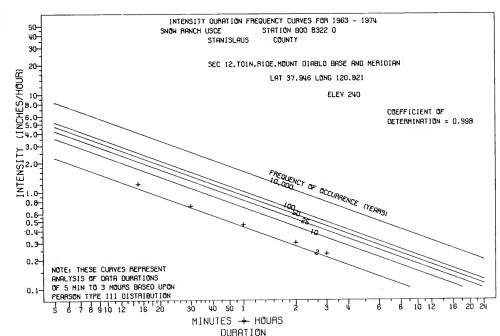


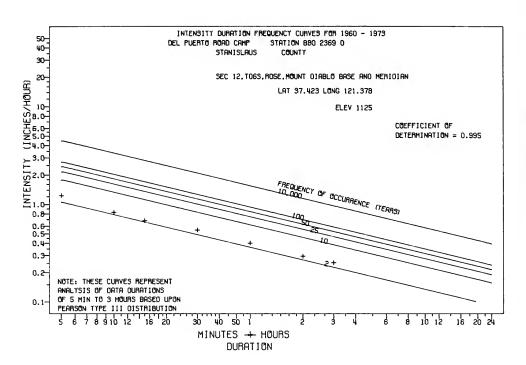


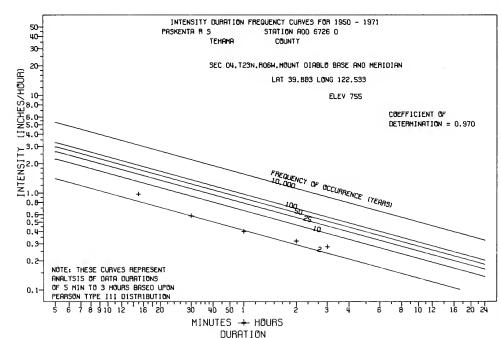


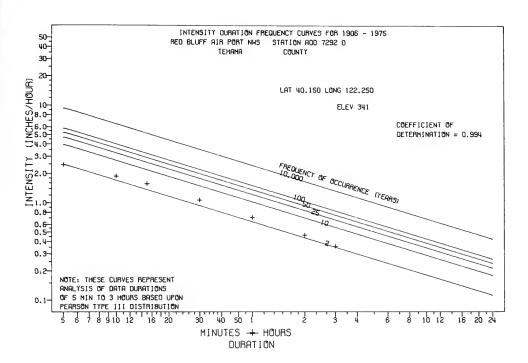


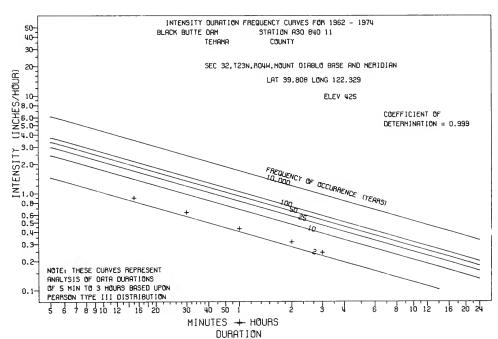


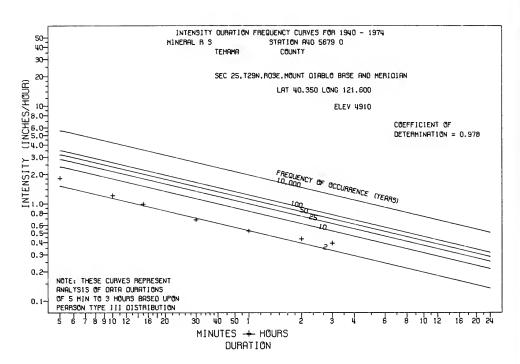


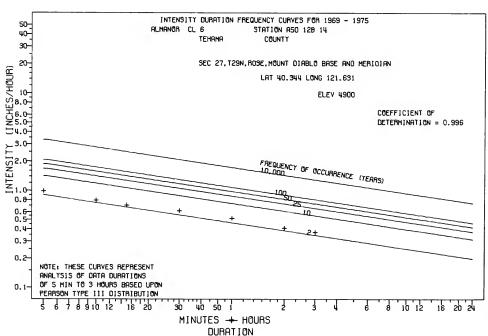


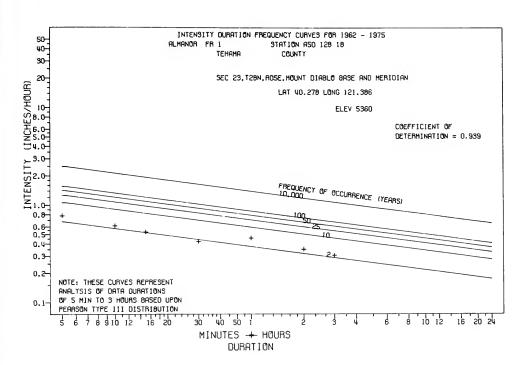


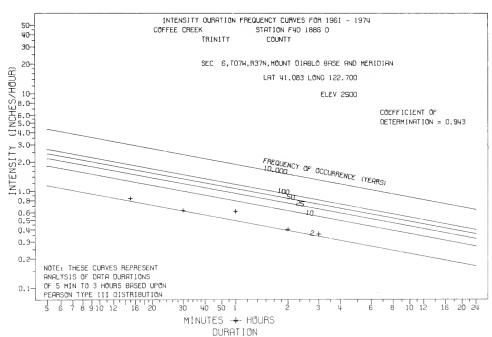


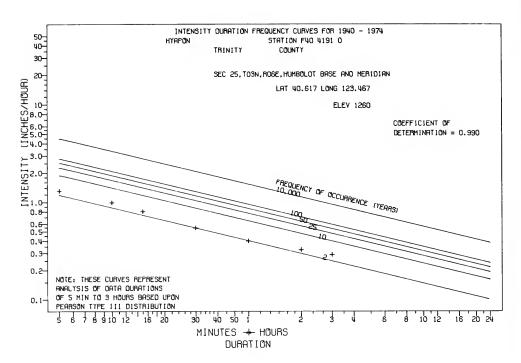


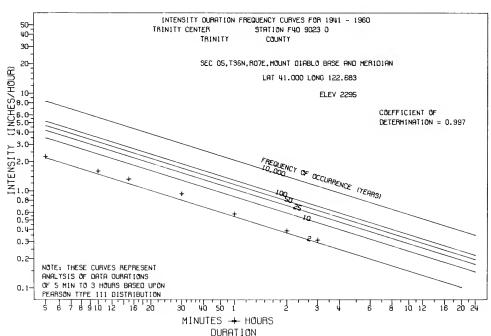


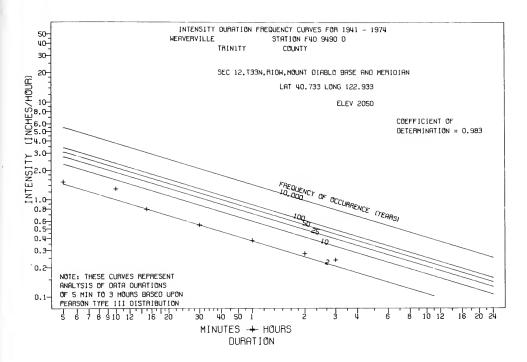


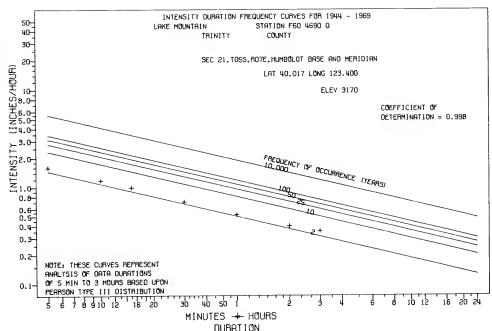


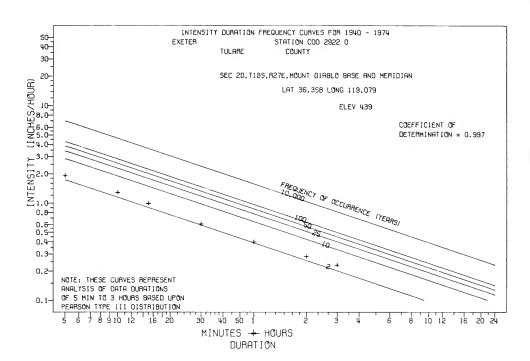


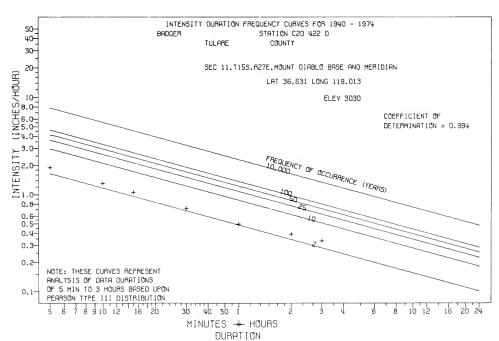


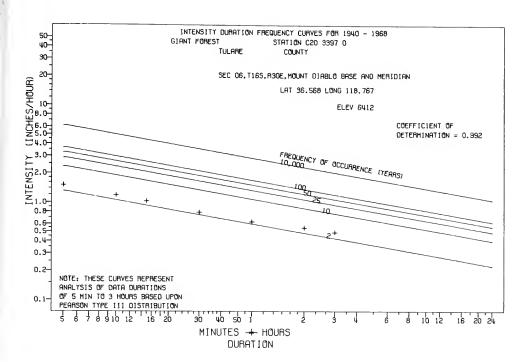


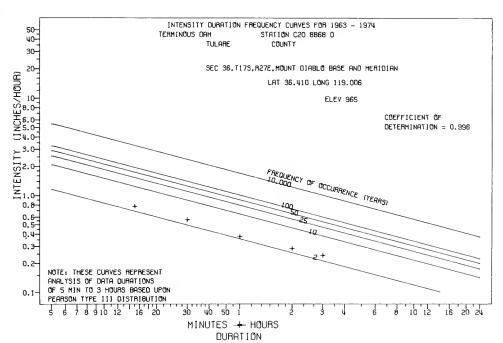


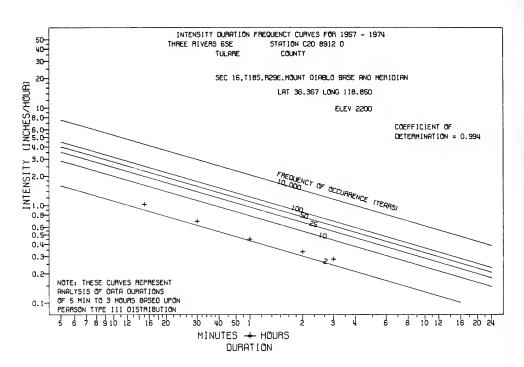


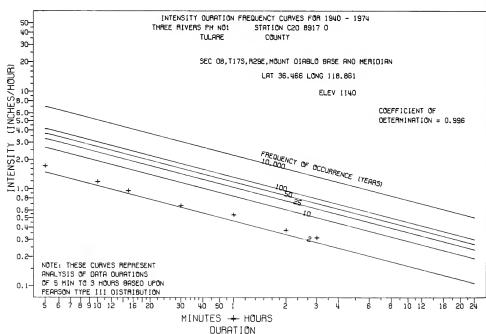


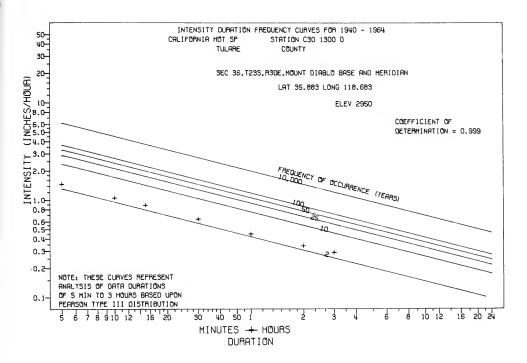


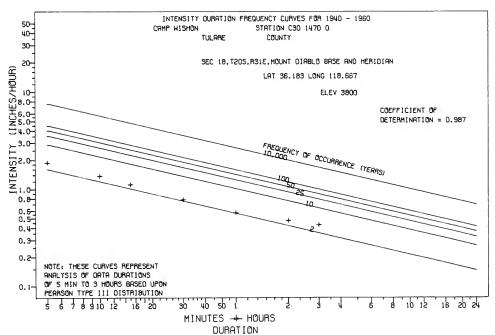


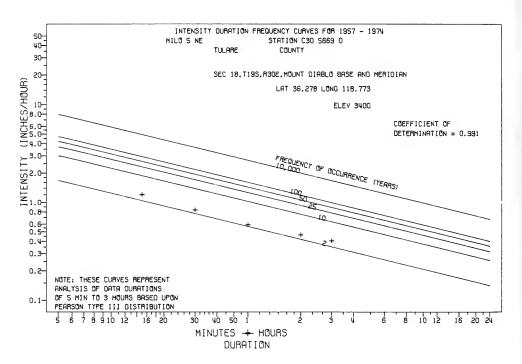


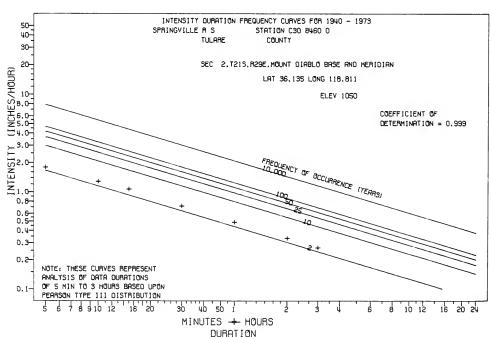


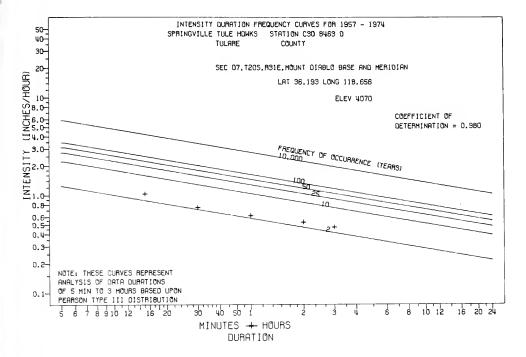


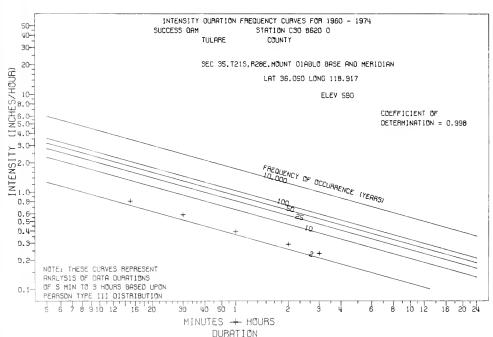


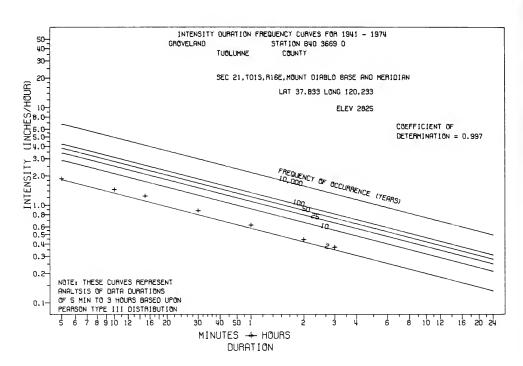


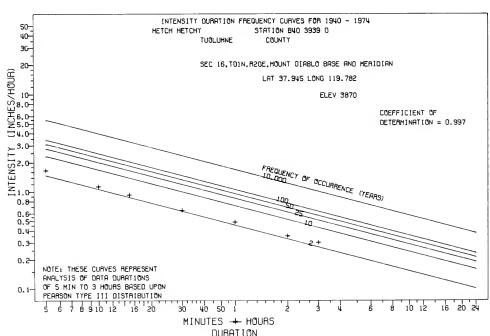


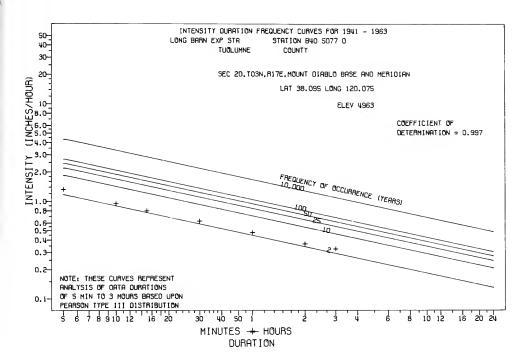


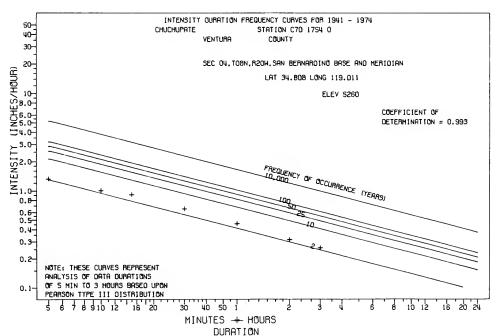


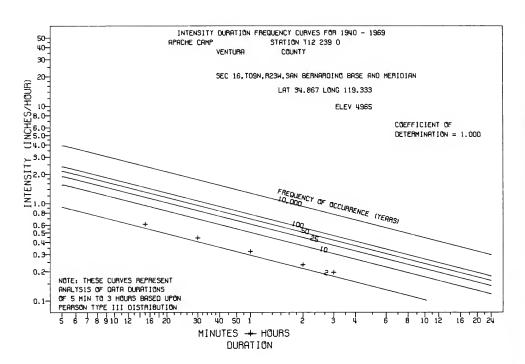


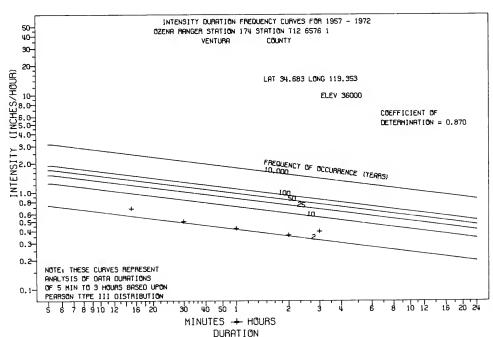


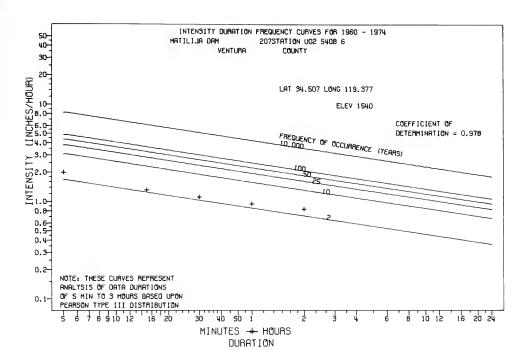


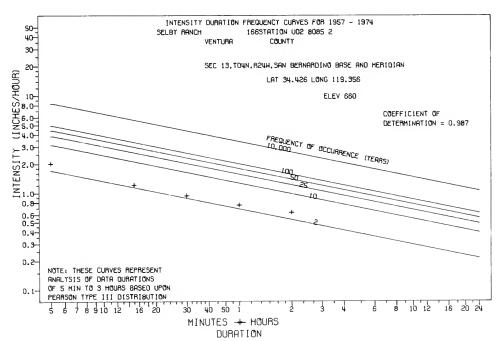


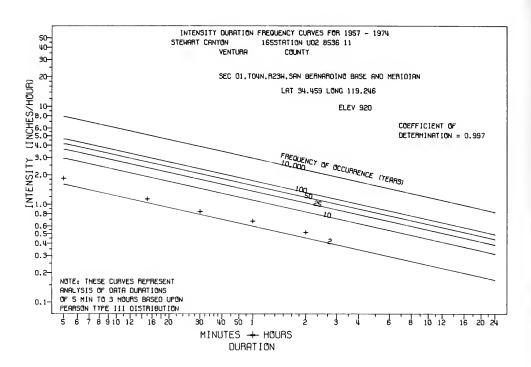


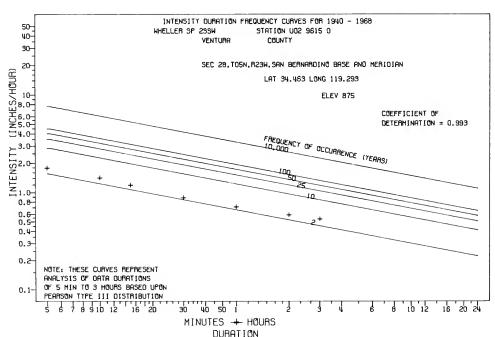


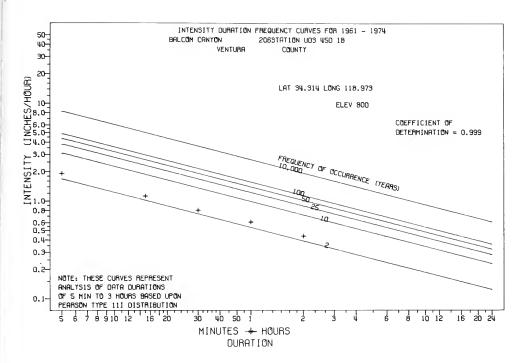


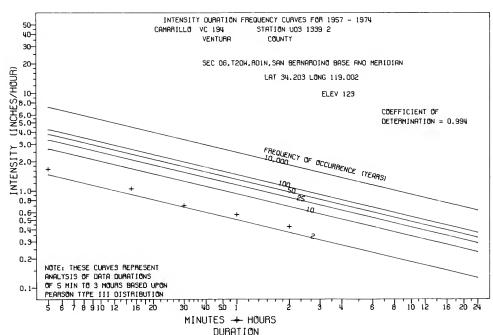


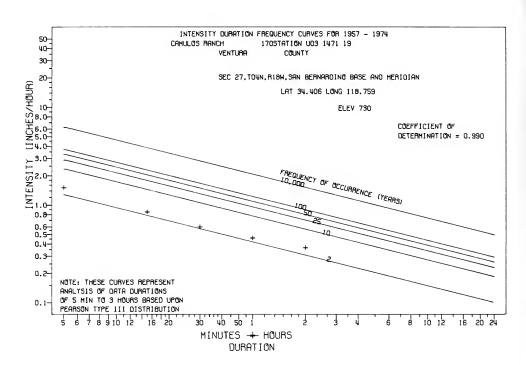


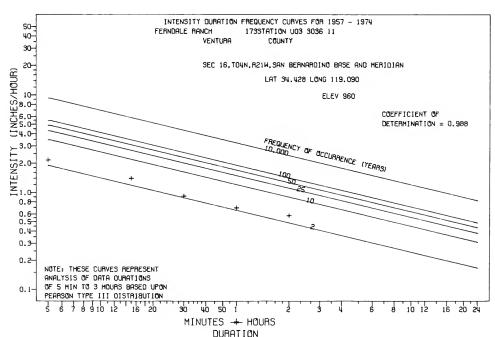


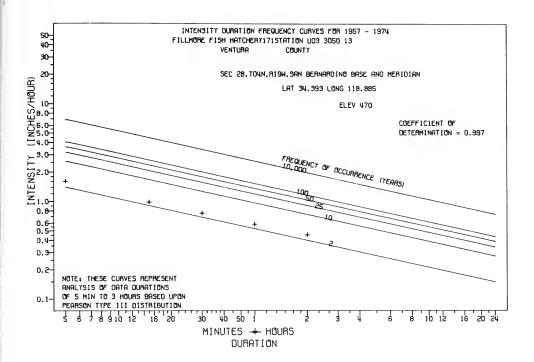


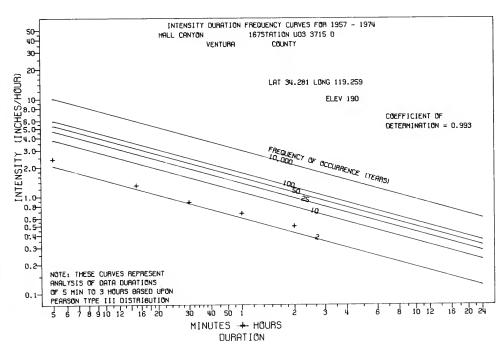


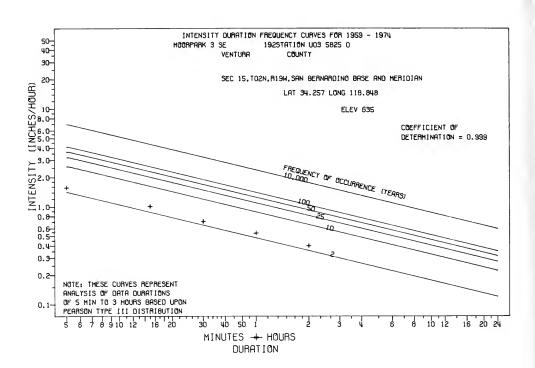


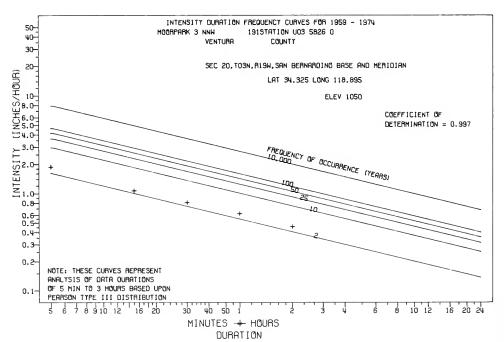


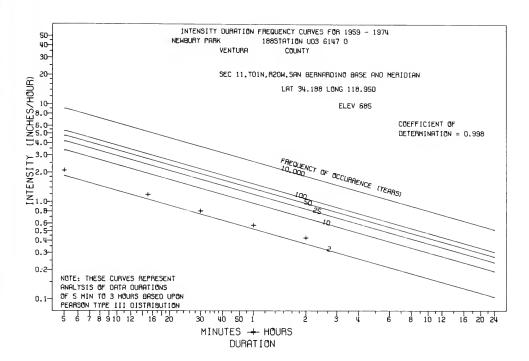


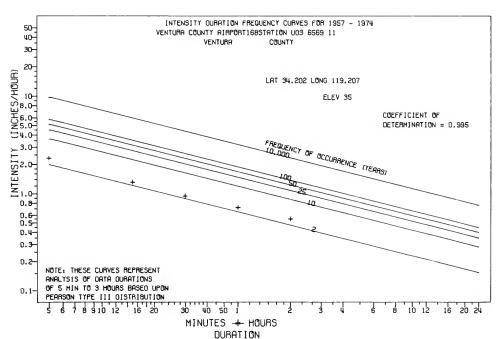


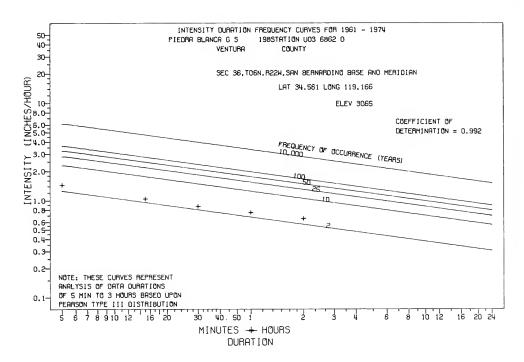


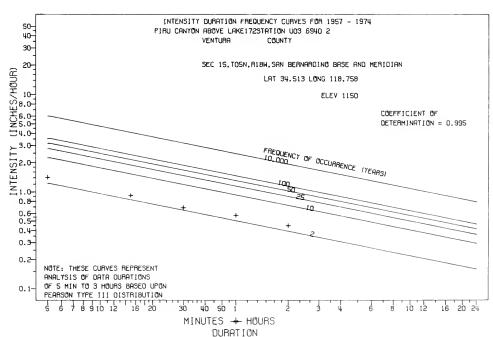


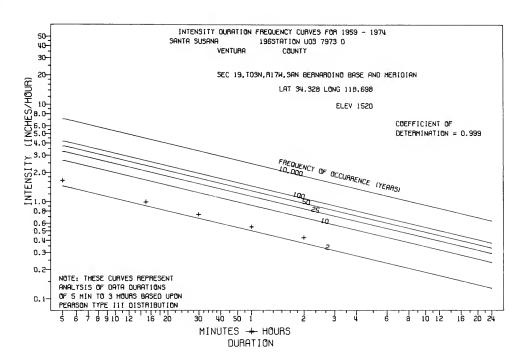


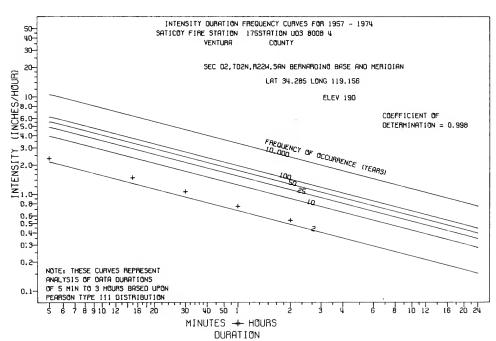


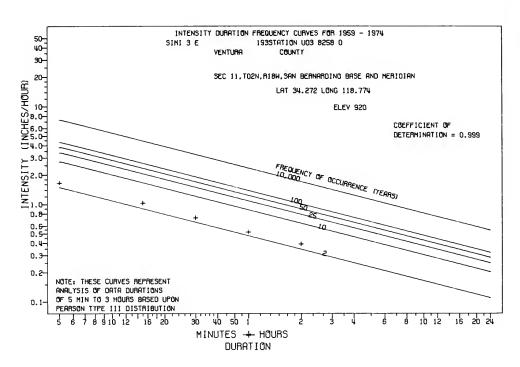


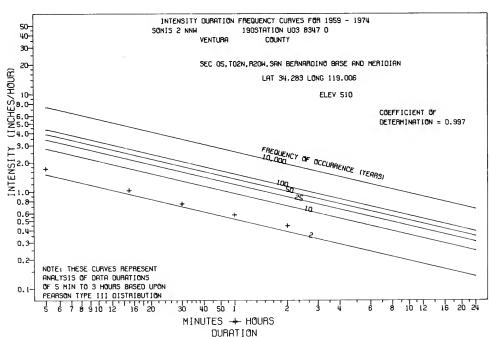


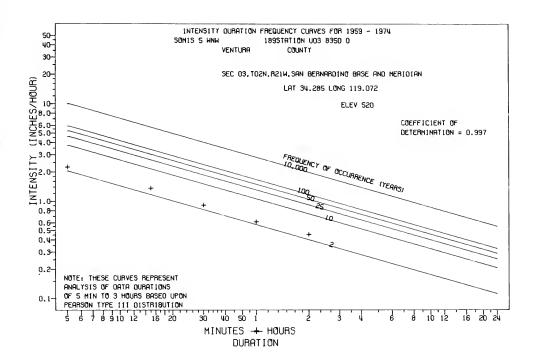


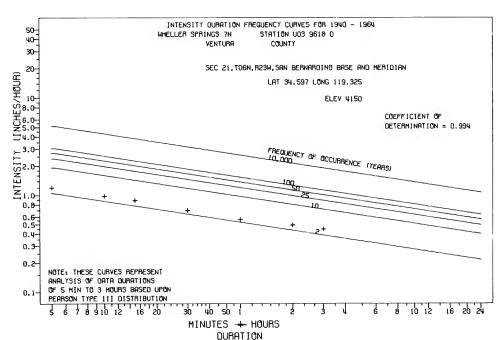


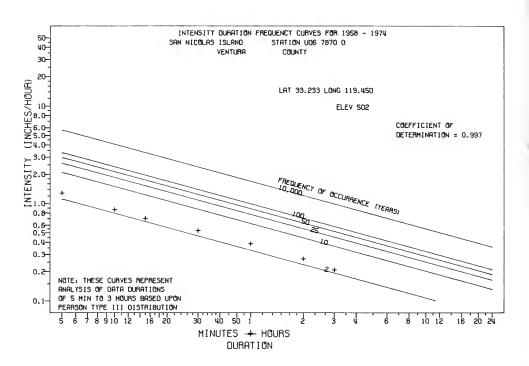


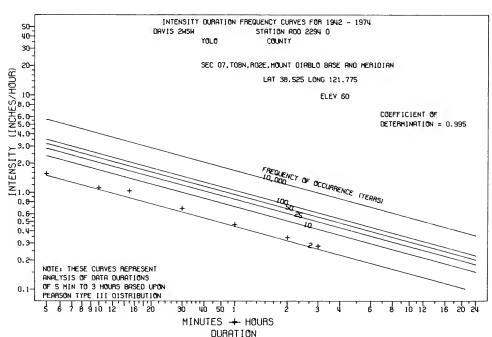


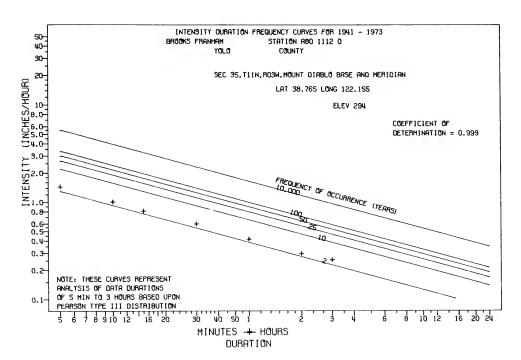


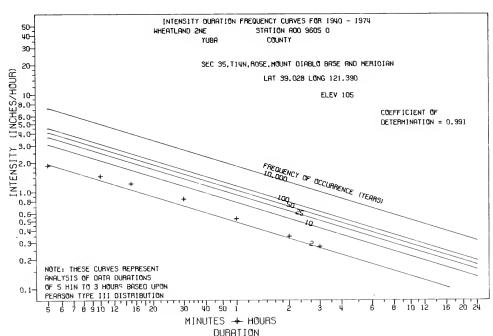


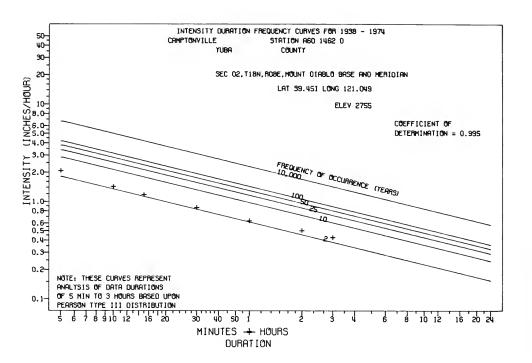


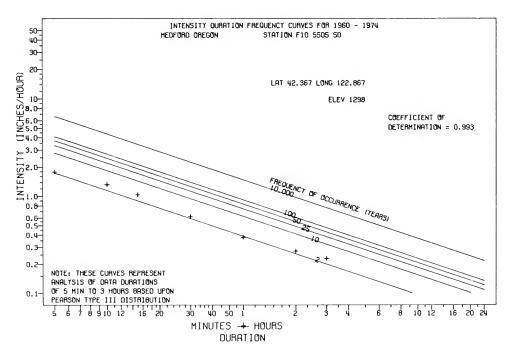


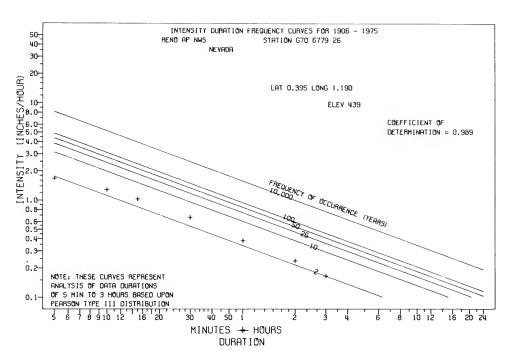


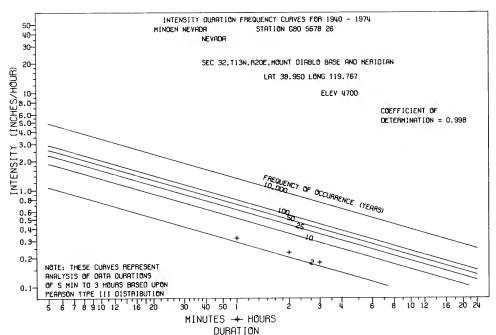


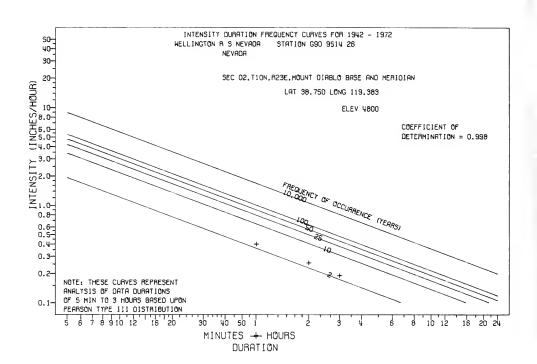


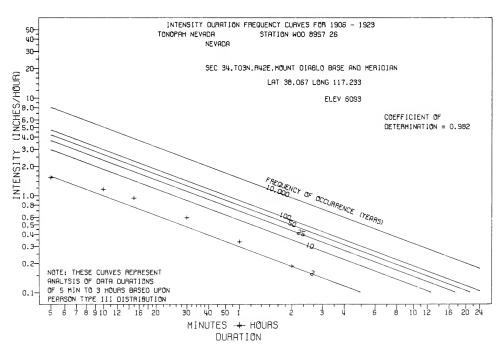


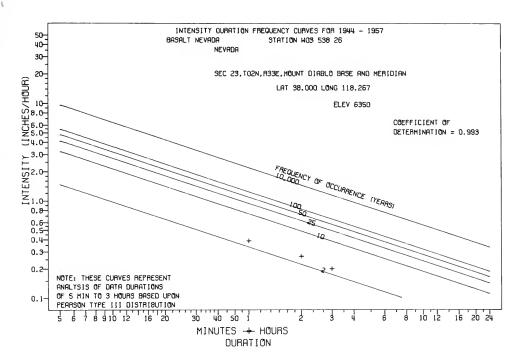


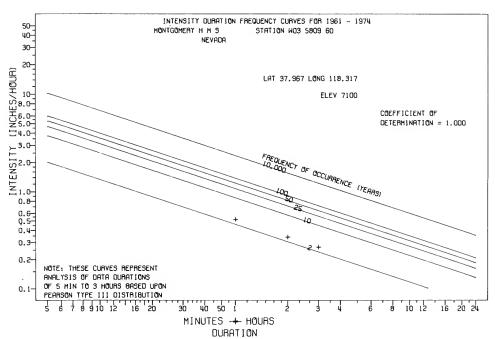


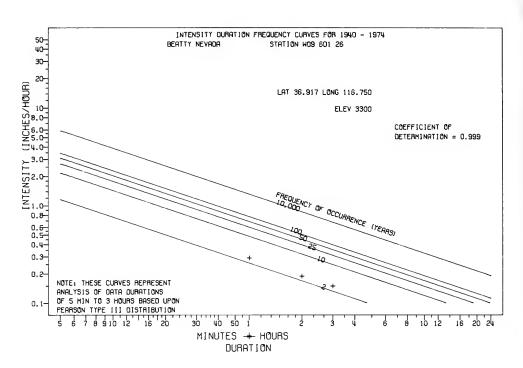


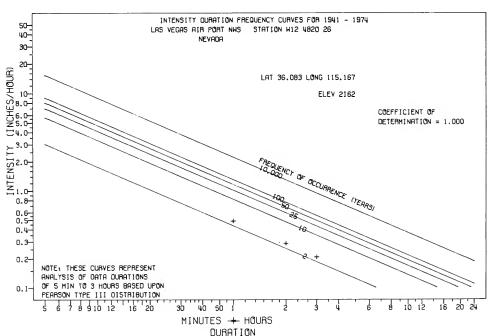


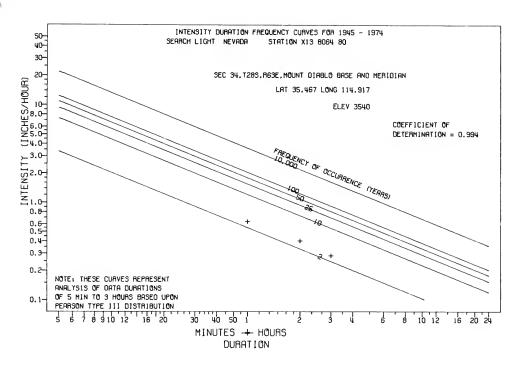


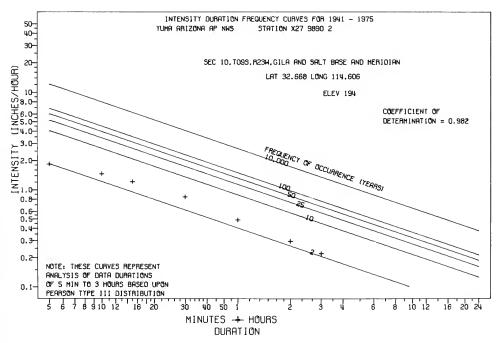












## **CONVERSION FACTORS**

## English to Metric System of Measurement

Quantity	English unit	Multiply by	To get metric equivalent
Length	inches (in)	25.4	millimetres (mm)
		.0254	metres (m)
	feet (ft)	.3048	metres (m)
	miles (mi)	1.6093	kilometres (km)
Area	square inches (in <sup>2</sup> )	$6.4516 \times 10^{-4}$	square metres (m <sup>2</sup> )
	square feet (ft <sup>2</sup> )	.092903	square metres (m²)
	acres	4046.9	square metres (m²)
		.40469	hectares (ha)
		.40469	square hectometres (hm²)
		.0040469	square kilometres (km²)
	square miles (mi <sup>2</sup> )	2.590	square kilometres (km²)
Volume	gallons (gal)	3.7854	litres (I)
		.0037854	cubic metres (m <sup>3</sup> )
	million gallons (10 <sup>6</sup> gal)	3785.4	cubic metres (m <sup>3</sup> )
	cubic feet (ft <sup>3</sup> )	.028317	cubic metres (m <sup>3</sup> )
	cubic yards (yd <sup>3</sup> )	.76455	cubic metres (m <sup>3</sup> )
	acre-feet (ac-ft)	1233.5	cubic metres (m <sup>3</sup> )
		.00 12335	cubic hectometres (hm³)
		$1.233 \times 10^{-6}$	cubic kilometres (km³)
Volume/Time			
(Flow)	cubic feet per second (ft <sup>3</sup> /s)	28.317	litres per second (1/s)
		.028317	cubic metres per second (m <sup>3</sup> /s)
	gallons per minute (gal/min)	.06309	litres per second (I/s)
		$6.309 \times 10^{-5}$	cubic metres per second (m <sup>3</sup> /s)
	million gallons per day (mgd)	.043813	cubic metres per second (m <sup>3</sup> /s)
Mass	pounds (lb)	.45359	kilograms (kg)
	tons (short, 2,000 lb)	.90718	tonne (t)
		907.18	kilograms (kg)
Power	horsepower (hp)	0.7460	kilowatts (kW)
Pressure	pounds per square inch (psi)	6894.8	pascal (Pa)
Temperature	Degrees Fahrenheit (°F)	$\frac{t F - 32}{1.8} = t C$	Degrees Celsius (°C)

14.1	



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